

### Civil Engineers & Surveyors

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# POST-CONSTRUCTION/E&SPC STORMWATER MANAGEMENT REPORT

**FOR** 

FRANKLIN HILL MANOR
PARCEL #16.7F.1.11
FRANKLIN HILL ROAD & ALBERT LANE
SMITHFIELD TOWNSHIP, MONROE COUNTY, PA

**SUBMITTED FOR:** 

D E & S PROPERTIES LLC 2621 ROUTE 940 POCONO SUMMIT, PA 18346

**SUBMITTED TO:** 

SMITHFIELD TOWNSHIP MONROE COUNTY, PA

REVISED MARCH 28, 2024 REVISED FEBRUARY 14, 2024 DECEMBER 1, 2023

CN-23-041

#### STORMWATER MANAGEMENT AND EROSION & SEDIMENT POLLUTION CONTROL NARRATIVE

This narrative has been prepared as part of the Stormwater Management and Erosion Control Plans for Franklin Hill Manor, a proposed subdivision on Albert Lane, owned by D E & S Properties. It has been prepared in accordance with the requirements of the Smithfield Township Ordinances, the Pennsylvania Code Title 25, Chapter 102 and the procedures outlined in the *Pennsylvania Stormwater Best Management Practices Manual*. The proposed project includes the construction of 3 single-family dwellings, on-lot wells and septic systems, and stormwater management berms. The project will be constructed on a wooded lot. The approximate area of earth disturbance is 2.37 acres. A NPDES Permit Application is being submitted concurrently to the Monroe County Conservation District. The project area discharges to a pond and an unnamed tributary to Marshalls Creek from two separate discharge points. In accordance with Pennsylvania Code Chapter 93, Marshalls Creek is a designated use: High Quality (HQ) Cold Water Fishery (CWF), Migratory Fishes (MF). The increase in stormwater runoff rate will be managed through the design of stormwater infiltration berms. Construction will take place immediately upon approval of the necessary permits. A project location map has been included on the plan.

#### I. SOIL FEATURES AND LIMITATIONS

According to the US Department of Agriculture (USDA), Natural Resources Conservation Service (NRCS), the soils on the site are listed below. Information can be found on the Plan Sheets and in the Appendix of this Report. There are no wetlands in the area of the project.

BaB - BATH CHANNERY LOAM, 3-8% SLOPES, HYDROLOGIC SOIL GROUP C, DEPTH TO WATER TABLE 24-36 INCHES, DEPTH TO BEDROCK 26-38 INCHES

BeB – BENSON-ROCK OUTCROP COMPLEX, 0-8% SLOPES, HYDROLOGIC SOIL GROUP D, DEPTH TO WATER TABLE >80 INCHES, DEPTH TO BEDROCK 12-20 INCHES

BeC – BENSON-ROCK OUTCROP COMPLEX, 8-25% SLOPES, HYDROLOGIC SOIL GROUP D, DEPTH TO WATER TABLE >80 INCHES, DEPTH TO BEDROCK 12-20 INCHES

MaB - MARDIN CHANNERY SILT LOAM, 3-8% SLOPES, HYDROLOGIC SOIL GROUP D, DEPTH TO WATER TABLE 13-24 INCHES, DEPTH TO BEDROCK 14-26 INCHES

A soil map, soil descriptions, and the soil use limitations and their resolutions are presented in the Appendix of this report.

### **II. STORMWATER RUNOFF**

The project is governed by the Smithfield Township Ordinances and district C of the Brodhead/McMichaels Watershed. If runoff cannot be discharged directly to a watercourse, for the disturbed area the post-development runoff rate is to be reduced from the 2- year post to 1-year pre, the 5-year post to the 5-year pre, the 10-year post to the 10-year pre, the 25-year post to the 25-year pre, the 50-year post to the 50-year pre, and the 100-year post to the 100-year pre. Two points of interest were analyzed, both of which are part of the Marshalls Creek watershed. Point of Interest #1 is a cross-pipe under Franklin Hill Road at the western limit of the project that discharges to a pond and Point of Interest #2 is a cross-pipe under Albert Lane at the eastern end of the project that discharges to a UNT to Marshalls Creek. All proposed earth disturbance discharges to one of these points of interest shown on the plans.

### **Stormwater Design Methodology:**

Stormwater runoff was modeled utilizing the Soil Conservation Service (SCS) methodology and the Hydraflow Hydrographs Extension software for AutoCAD Civil 3D. The design storm rainfall amounts and runoff curve numbers (CN) were taken from the Smithfield Township Ordinances. The Time of Concentration (Tc) was calculated utilizing the methodology set forth in Urban Hydrology for Small Watersheds (TR-55) SCS Segmental Approach/SCS Lag Equation. A summary of discharge rates for the points of interest have been included in the appendix below:

Point of Interest #1 includes an infiltration berm on lot 1 and lot 2. Point of Interest #2 includes an infiltration berm on lot 3. Calculations for these items have been provided in the Appendix.

#### III. BEST MANAGEMENT PRACTICES

The following E&S BMPs will be utilized for this project:

**Rock Construction Entrance:** A rock construction entrance will be installed where construction traffic will exit the project site onto a roadway in order to prevent excessive tracking of mud onto exiting roadways. The rock construction entrance will remain until completion of construction and a minimum of 70 percent perennial vegetative cover has been established for the project site.

**Compost Filter Sock:** Compost Filter Sock will be installed below the disturbed areas to filter sediment from stormwater runoff sheet flow and prevent off site transport of sediment. Compost Filter Sock will remain until completion of construction and a minimum of 70 percent perennial vegetative cover has been established for the project site. Compost Filter Sock will be re-installed if stabilized areas are disturbed after the completion of construction activities.

**Temporary Seeding and Mulching:** Upon temporary cessation of earth disturbance activity for more than four days the project site will be immediately stabilized with temporary seeding and mulching. Areas will receive topsoil, lime, fertilizer and seed conforming to PennDOT Publication 408, Formula E depending on slope and water content of soil. Temporary stabilization should continue until completion of construction and a minimum of 70 percent perennial vegetative cover has been established for the project site. Temporary seeding will occur in disturbed areas throughout the project site.

**Permanent Seeding and Mulching:** As soon as slopes, channels, and other disturbed areas reach final grade they will be stabilized. Areas will receive topsoil, lime, fertilizer and seed conforming to the *Erosion and Sediment Pollution Control Program Manual* depending on slope and water content of soil. Permanent seeding and mulching will occur in all disturbed areas throughout the project site.

Stormwater BMPs will include the installation of the stormwater infiltration berms and meadow resotration. This will provide rate reduction, water quality and groundwater recharge.

#### IV. SEQUENCE OF CONSTRUCTION ACTIVITIES

See the plans for the Sequence of Construction Activities.

#### V. SUPPORTING CALCULATIONS

Refer to the Appendix for the supporting calculations.

#### VI. PLAN DRAWINGS

Stormwater and erosion and sediment pollution control plans are attached.

#### VII. OPERATION AND MAINTENANCE PROGRAM

The operation and maintenance associated with the Erosion and Sediment Pollution Control BMP's were developed in accordance with the *Erosion and Sediment Pollution Control Program Manual*. The BMPs will be maintained as follows:

**Rock Construction Entrance:** The rock construction entrance thickness will be constantly maintained to the specified dimension. The rock construction entrance will be kept free of sediment and debris. Sediment will be removed from the rock construction entrance by mechanical means and returned to the construction site or sediment laden rock will be removed and replaced with clean rock. A stockpile of clean rock will be maintained on site for this purpose.

**Compost Filter Sock:** Compost filter sock will be inspected weekly and after each runoff event to ensure that they are intact and functioning properly. Sediment will be removed when accumulations reach 1/2 the height of the sock. Damaged compost filter sock will be repaired immediately. Any section of compost filter sock that has been undermined or over-topped will be replaced with a rock filter outlet.

**Temporary Seeding and Mulching:** Mulch is to be used as necessary for protection until vegetation is established. Seeded areas will be inspected for failure and reseeded and repaired immediately, as necessary. If inadequate cover is attained, the choice of seed will be reevaluated along with the quantities of lime and fertilizer.

Permanent E&S Control Measures will be maintained as follows:

**Permanent Seeding and Mulching:** Seeded areas will be inspected for failure and reseeded and repaired immediately, as necessary. If inadequate cover is attained, the choice of seed will be reevaluated along with the quantities of lime and fertilizer.

The operation and maintenance procedures associated with the stormwater features were developed in accordance with the *Pennsylvania Stormwater Best Management Practices Manual* to provide for inspection of the PCSM BMPs, including the repair, replacement, or other routine maintenance of the PCSM BMPs to ensure proper function and operation. The property owner is responsible for the operation and maintenance associated with the proposed stormwater management features. These procedures have been provided on the plan drawings.

### VIII. WASTE RECYCLING AND DISPOSAL

All suitable accumulated sediment will be incorporated into the fill and reused on-site. Unsuitable material will be removed from the site and disposed of in a lawful manner according to the Pennsylvania Department of Environmental Protection's Solid Waste Management Regulations (Pennsylvania Code Title 25, Chapter 260.1 et. seq., 271.1 et. seq., and 287.1 et. seq). The disposal site must have a separate erosion control plan and must be approved by either PA DEP or the County Conservation District.

### **APPENDIX**

#### FRANKLIN HILL MANOR SUBDIVISION - STORMWATER CALCULATIONS:

HYDROGRAPHS AND DRAINAGE AREA MAPS FOLLOW THE SUMMARIZED CALCULATIONS BELOW. SCS METHOD USED IN ACCORDANCE WITH THE NPDES PERMIT APPLICATION REQUIREMENT.

### **DISCHARGE POINT #1 TO POND**

- PRE-DEVELOPMENT POI 1:
  - o DRAINAGE AREA = 2.33 ACRES
  - o CURVE NUMBER
    - 0.15 LAWN D SOILS = 80
    - 1.74 ACRES WOODS C SOILS = 70
    - 0.29 ACRES WOODS D SOILS = 77
    - 0.15 ACRES IMPERVIOUS = 98
    - WEIGHTED CN = 73
  - o TC = 28.2 MINS
    - SHEET FLOW = 200' @ 5.4% SLOPE, N=0.4
    - SHALLOW CONC = 240' @ 10.8%, UNPAVED
    - SHALLOW CONC = 250' @ 6.9%, UNPAVED
  - o POI 1 PRE-DEVELOPMENT RUNOFF RATE
    - Q1 = 0.885 CFS
    - Q2 = 1.484 CFS
    - Q5 = 2.507 CFS
    - Q10 = 4.023 CFS
    - Q25 = 6.077 CFS
    - Q50 = 7.371 CFS
    - Q100 = 9.137 CFS
- PRE-DEVELOPMENT POI 1 (DISTURBED AREA ONLY):
  - o DRAINAGE AREA = 1.28 ACRES
  - o CURVE NUMBER
    - 0.07 ACRES WOODS D SOILS = 77
    - 1.21 ACRES WOODS C SOILS = 70
    - WEIGHTED CN = 70
  - o TC = 7.6 MINS
    - SHEET FLOW = 50' @ 11.91% SLOPE, N=0.4
    - SHALLOW CONC = 60' @ 11.82%, UNPAVED
    - SHALLOW CONC = 272' @ 3.9%, UNPAVED
  - o POI 1 PRE-DEVELOPMENT RUNOFF RATE
    - Q1 = 0.704 CFS
    - Q2 = 1.229 CFS
    - Q5 = 2.130 CFS
    - Q10 = 3.477 CFS
    - Q25 = 5.307 CFS
    - Q50 = 6.480 CFS
    - Q100 = 8.093 CFS

- POST-DEVELOPMENT POI 1:
- POST-DEVELOPMENT POI 1 BYPASS 1:
  - o TOTAL DRAINAGE AREA = 1.03 ACRES
  - o CURVE NUMBER
    - 0.30 ACRES MEADOW C SOILS = 71
    - 0.11 ACRES WOODS D SOILS = 77
    - 0.29 ACRES WOODS C SOILS = 70
    - 0.20 ACRES IMPERVIOUS = 98
    - 0.03 ACRES MEADOW D SOILS = 78
    - 0.10 ACRES LAWN C&D SOILS = 79 (AS SHOWN IN HYDROGRAPHS) COMBINATION OF 0.09 ACRES LAWN D = 80 & 0.01 LAWN C = 74
    - WEIGHTED CN = 78

#### o TC = 27.7 MINS

- SHEET FLOW = 200' @ 5.4% SLOPE, N=0.4
- SHALLOW CONC = 134' @ 10.8%, UNPAVED
- SHALLOW CONC = 96' @ 8.3%, PAVED
- CHANNEL = 318' @ 6.6%, N=0.025
- RUNOFF RATE
  - Q1 = 0.623 CFS
  - Q2 = 0.935 CFS
  - Q5 = 1.446 CFS
  - Q10 = 2.181 CFS
  - Q25 = 3.151 CFS
  - Q50 = 3.747 CFS
  - Q100 = 4.551 CFS

#### o AREA TO INFILTRATION BERM #1

- DRAINAGE AREA = 0.46 ACRES
- CURVE NUMBER
  - 0.08 ACRES IMPERVIOUS = 98
  - 0.18 ACRES LAWN (C SOILS) = 74
  - 0.07 ACRES MEADOW (C SOILS) = 71
  - 0.07 ACRES WOODS (C SOILS) = 70
  - 0.01 ACRES WOODS (D SOILS) = 77
  - 0.05 ACRES LAWN (D SOILS) = 80
  - WEIGHTED CN = 78
- TC = 9.0 MINS
  - SHEET FLOW = 56' @ 7.14% SLOPE, N=0.4
  - SHALLOW CONC = 40' @ 5.26%, PAVED
  - SHALLOW CONC = 87' @ 7.31%, UNPAVED
- RUNOFF RATE
  - Q1 = 0.519 CFS
  - Q2 = 0.759 CFS
  - Q5 = 1.148 CFS
  - Q10 = 1.710 CFS
  - Q25 = 2.448 CFS
  - Q50 = 2.899 CFS
  - Q100 = 3.505 CFS

#### ■ BERM #1

- RECHARGE VOLUME REQUIRED:
  - I = 0.6 INCHES
  - Rev = (I)(IMPERVIOUS AREA)
  - Rev = (0.6 IN)(0.29 AC)(43560 SF)(FT/12 IN)
  - Rev = 631.62 CF
  - VOLUME OF SYSTEM BELOW ORIFICE = 1736 CF
- RECHARGE VOLUME TIME TO DRAIN:
  - INFILTRATION RATE UTILIZED 1.0 IN/HR
  - TESTING PROVIDED A RATE OF 2.0 IN/HR WITH A SAFETY FACTOR OF 2 = 1.0 IN/HR
  - DRAIN TIME OF REV = (3 FT DEPTH OF INFILTRATION AREA)(HR/1.0 IN)(12 IN/FT) = 36 HOURS
- BOTTOM @ 680.00, TOP BERM @ 684.00, 5 FT LONG SPILLWAY @ 683.50, RISER @ 683.40, 12" HDPE DISCHARGE PIPE 15' LONG @ 1% INV. OUT @ 681.00, 3" X 36" ORIFICE @ 683.00
- OUTFLOW
  - o Q1 = 0.000 CFS, ELEV @ 682.06
  - o Q2 = 0.000 CFS, ELEV @ 682.36
  - o Q5 = 0.000 CFS, ELEV @ 682.88
  - o Q10 = 0.196 CFS, ELEV @ 683.06
  - o Q25 = 1.108 CFS, ELEV @ 683.23
  - o Q50 = 1.594 CFS, ELEV @ 683.32
  - o Q100 = 2.431 CFS, ELEV @ 683.43

#### o AREA TO INFILTRATION BERM #2

- DRAINAGE AREA = 0.89 ACRES
- CURVE NUMBER
  - 0.13 ACRES IMPERVIOUS = 98
  - 0.30 ACRES LAWN (C SOILS) = 74
  - 0.13 ACRES MEADOW (C SOILS) = 71
  - 0.17 ACRES WOODS (C SOILS) = 70
  - 0.10 ACRES WOODS (D SOILS) = 77
  - 0.06 ACRES LAWN (D SOILS) = 80
  - WEIGHTED CN = 77
- TC = 26.6 MINS
  - SHEET FLOW = 200' @ 5.92% SLOPE, N=0.4
  - SHALLOW CONC = 114' @ 8.43%, UNPAVED
  - SHALLOW CONC = 59' @ 8.7%, PAVED
  - SHALLOW CONC = 143' @ 8.1%, UNPAVED
- RUNOFF RATE
  - Q1 = 0.535 CFS
  - Q2 = 0.815 CFS
  - Q5 = 1.275 CFS
  - Q10 = 1.946 CFS
  - Q25 = 2.834 CFS
  - Q50 = 3.381 CFS

- Q100 = 4.120 CFS
- BERM #2
  - RECHARGE VOLUME REQUIRED:
    - I = 0.6 INCHES
    - Rev = (I)(IMPERVIOUS AREA)
    - Rev = (0.6 IN)(0.29 AC)(43560 SF)(FT/12 IN)
    - Rev = 631.62 CF
    - VOLUME OF SYSTEM BELOW ORIFICE = 1705 CF
  - RECHARGE VOLUME TIME TO DRAIN:
    - INFILTRATION RATE UTILIZED 1.75 IN/HR
    - TESTING PROVIDED A RATE OF 3.5 IN/HR WITH A SAFETY FACTOR OF 2 = 1.75 IN/HR
    - DRAIN TIME OF REV = (2 FT DEPTH OF INFILTRATION AREA)(HR/1.75 IN)(12 IN/FT) = 12 HOURS
  - BOTTOM @ 691.00, TOP BERM @ 694.00, 5 FT WIDE SPILLWAY @ 693.50, RISER @ 693.40, 12" HDPE DISCHARGE PIPE 25' LONG @ 1% INV. OUT @ 691.50, 3" X 38" ORIFICE @ 692.75
  - OUTFLOW
    - o Q1 = 0.000 CFS, ELEV @ 692.35
    - o Q2 = 0.014 CFS, ELEV @ 692.71
    - o Q5 = 0.605 CFS, ELEV @ 692.90
    - o Q10 = 1.455 CFS, ELEV @ 693.02
    - o Q25 = 2.146 CFS, ELEV @ 693.19
    - o Q50 = 2.515 CFS, ELEV @ 693.31
    - o Q100 = 3.307 CFS, ELEV @ 693.45
- POST-DEVELOPMENT RELEASE RATE CRITERIA DISTRICT C ON ACT 167 MAP:
  - o 2YR POST TO 1 YR PRE
    - 2YR POST=1.484(2YR PRE)-1.229(2YR CHANGED)+0.704(1YR CHANGED)= 0.959CFS
  - o 5YR POST TO 5 YR PRE
    - ■5YR POST=2.507(5YR PRE)CFS
  - o 10YR POST TO 10 YR PRE
    - ■10YR POST=4.023(10YR PRE)CFS
  - o 25YR POST TO 25 YR PRE
    - ■25YR POST=6.077(25YR PRE)CFS
  - o 50YR POST TO 50 YR PRE
    - ■50YR POST=7.371(50YR PRE)CFS
  - o 100YR POST TO 100 YR PRE
    - ■100YR POST= 9.137(100YR PRE)CFS

#### O TOTAL POI 1 POST-DEVELOPMENT RUNOFF RATE

- Q1 = 0.623 CFS
- Q2 = 0.935 CFS
- Q5 = 1.659 CFS
- Q10 = 3.726 CFS
- Q25 = 6.052 CFS
- Q50 = 7.364 CFS

#### • Q100 = 9.091 CFS

DESIGN STORM	PRE-DEV. FLOW/VOLUME-POI 1	POST-DEV. FLOW/VOLUME – POI 1
1-YEAR	0.885 CFS / 4351 CF	0.623 CFS / 2706 CF
2-YEAR	1.484 CFS / 6635 CF	0.935 CFS / 3939 CF
5-YEAR	2.507 CFS / 10550 CF	1.659 CFS / 7053 CF
10-YEAR	4.023 CFS / 16417 CF	3.726 CFS / 12642 CF
25-YEAR	6.077 CFS / 24449 CF	6.052 CFS / 20657 CF
50-YEAR	7.371 CFS / 29526 CF	7.364 CFS / 25750 CF
100-YEAR	9.137 CFS / 36514 CF	9.091 CFS / 32803 CF

### • SWALE 1

- o FLOW = 7.364 CFS (50-YEAR STORM) SAME AS TOTAL POST TO POI 1
- o SLOPE @ 6.6%, DEPTH IS 2 FT. AND BOTTOM WIDTH IS 2 FT. SIDE SLOPES 3:1
- o S150BN MATTING, STAPLE PATTERN D.

### • SWALE 2

- DRAINAGE AREA = 0.08 ACRES
- CURVE NUMBER
  - 0.01 ACRES LAWN (C SOILS) = 74
  - 0.01 ACRES WOODS (C SOILS) = 70
  - 0.01 ACRES WOODS (D SOILS) = 77
  - 0.05 ACRES LAWN (D SOILS) = 80
  - WEIGHTED CN = 78
- TC = 5 MINS
- o FLOW = 0.533 CFS (50-YEAR STORM)
- o SLOPE @ 5.71%, DEPTH IS 1 FT. AND BOTTOM WIDTH IS 4 FT. SIDE SLOPES 3:1
- o S75BN MATTING, STAPLE PATTERN D.

### • SWALE 3

- DRAINAGE AREA = 0.08 ACRES
- CURVE NUMBER
  - 0.07 ACRES LAWN (C SOILS) = 74
  - 0.01 ACRES WOODS (C SOILS) = 70
  - WEIGHTED CN = 74
- TC = 5 MINS
- o FLOW = 0.482 CFS (50-YEAR STORM)
- o SLOPE @ 7.1%, DEPTH IS 1 FT. AND BOTTOM WIDTH IS 3 FT. SIDE SLOPES 8:1
- o S75BN MATTING, STAPLE PATTERN D.

#### • RIPRAP APRON 1

- o FLOW = 7.364 CFS (50-YEAR STORM) SAME AS TOTAL POST TO POI 1
- o VELOCITY = 4.60 FPS
- o PROPOSED: R-5 STONE, 5' INITIAL WIDTH, 13' TERMINAL WIDTH, 9' LENGTH, 27" THICK

### • RIPRAP APRON 2

o FLOW = 1.594 CFS (50-YEAR STORM) <u>SAME AS OUTFLOW OF BERM 1</u>

- o VELOCITY = 4.60 FPS
- o PROPOSED: R-3 STONE, 3' INITIAL WIDTH, 9' TERMINAL WIDTH, 6' LENGTH, 12" THICK
- RIPRAP APRON 3
  - o FLOW = 2.515 CFS (50-YEAR STORM) SAME AS OUTFLOW OF BERM 2
  - o VELOCITY = 5.20 FPS
  - o PROPOSED: R-3 STONE, 3' INITIAL WIDTH, 9' TERMINAL WIDTH, 6' LENGTH, 12" THICK

### **DISCHARGE POINT #2 TO UNTO TO MARSHALLS CREEK**

- PRE-DEVELOPMENT POI 2:
  - o DRAINAGE AREA = 10.36 ACRES
  - o CURVE NUMBER
    - 0.48 ACRES LAWN D SOILS = 80
    - 5.4 ACRES WOODS C SOILS = 70
    - 3.51 ACRES WOODS D SOILS = 77
    - 0.70 ACRES IMPERVIOUS = 98
    - 0.27 ACRES LAWN C SOILS = 74
    - WEIGHTED CN = 75
  - o TC = 23.0 MINS
    - SHEET FLOW = 175' @ 7.49% SLOPE, N=0.4
    - SHALLOW CONC = 200' @ 6.7%, UNPAVED
    - SHALLOW CONC = 425' @ 10.57%, UNPAVED
  - o POI 1 PRE-DEVELOPMENT RUNOFF RATE
    - Q1 = 5.768 CFS
    - Q2 = 9.134 CFS
    - Q5 = 14.76 CFS
    - Q10 = 22.98 CFS
    - Q25 = 34.08 CFS
    - Q50 = 40.96 CFS
    - **Q100 = 50.30 CFS**
- PRE-DEVELOPMENT POI 2 (DISTURBED AREA ONLY):
  - o DRAINAGE AREA = 1.09 ACRES
  - o CURVE NUMBER
    - 0.93 ACRES WOODS C SOILS = 70
    - 0.16 ACRES WOODS D SOILS = 77
    - WEIGHTED CN = 71
  - o TC = 21.3 MINS
    - SHEET FLOW = 100' @ 9.75% SLOPE, N=0.4
    - SHALLOW CONC = 75' @ 9.75%, UNPAVED
  - o POI 1 PRE-DEVELOPMENT RUNOFF RATE
    - Q1 = 0.396 CFS
    - Q2 = 0.702 CFS
    - Q5 = 1.233 CFS
    - Q10 = 2.031 CFS
    - Q25 = 3.126 CFS
    - Q50 = 3.822 CFS
    - Q100 = 4.776 CFS

- POST-DEVELOPMENT POI 2:
- POST-DEVELOPMENT POI 2 BYPASS 1:
  - o TOTAL DRAINAGE AREA = 6.97 ACRES

#### o CURVE NUMBER

- 0.11 ACRES MEADOW D SOILS = 78
- 0.70 ACRES IMPERVIOUS = 98
- 1.71 ACRES WOODS D SOILS = 77
- 3.61 ACRES WOODS C SOILS = 70
- 0.22 ACRES MEADOW (C SOILS) = 71
- 0.62 ACRES LAWN C & D SOILS = 77 (AS SHOWN IN HYDROGRAPHS) COMBINATION OF 0.35 ACRES LAWN D = 80 & 0.27 LAWN C = 74
- WEIGHTED CN = 75

#### o TC = 23.0 MINS

- SHEET FLOW = 175' @ 7.49% SLOPE, N=0.4
- SHALLOW CONC = 200' @ 6.7%, UNPAVED
- SHALLOW CONC = 425' @ 10.57%, UNPAVED
- RUNOFF RATE
  - Q1 = 3.881 CFS
  - Q2 = 6.145 CFS
  - Q5 = 9.927 CFS
  - Q10 = 15.46 CFS
  - Q25 = 22.93 CFS
  - Q50 = 27.56 CFS
  - Q100 = 33.84 CFS

#### o AREA TO INFILTRATION BERM #3

- DRAINAGE AREA = 3.34 ACRES
- CURVE NUMBER
  - 0.16 ACRES IMPERVIOUS = 98
  - 0.32 ACRES LAWN (C SOILS) = 74
  - 0.86 ACRES WOODS (C SOILS) = 70
  - 1.64 ACRES WOODS (D SOILS) = 77
  - 0.21 ACRES MEADOW (C SOILS) = 71
  - 0.15 ACRES LAWN (D SOILS) = 80
  - WEIGHTED CN = 76

#### o TC = 21.8 MINS

- SHEET FLOW = 150' @ 5.97% SLOPE, N=0.4
- SHALLOW CONC = 110' @ 4.76%, UNPAVED
- SHALLOW CONC = 31' @ 5%, PAVED
- SHALLOW CONC = 323' @ 11.36%, UNPAVED (AVERAGE FOR ENTIRE LENGTH)
- RUNOFF RATE
  - Q1 = 2.036 CFS
  - Q2 = 3.156 CFS
  - Q5 = 5.011 CFS
  - Q10 = 7.718 CFS
  - Q25 = 11.34 CFS
  - Q50 = 13.58 CFS
  - Q100 = 16.60 CFS

#### ■ BERM #3

- RECHARGE VOLUME REQUIRED:
  - I = 0.6 INCHES
  - Rev = (I)(IMPERVIOUS AREA)
  - Rev = (0.6 IN)(0.29 AC)(43560 SF)(FT/12 IN)
  - Rev = 631.32 CF
  - VOLUME OF SYSTEM BELOW ORIFICE = 8928 CF
- RECHARGE VOLUME TIME TO DRAIN:
  - INFILTRATION RATE UTILIZED 2.5 IN/HR
  - TESTING PROVIDED A RATE OF 5.0 IN/HR WITH A SAFETY FACTOR OF 2 = 2.5 IN/HR
  - DRAIN TIME OF REV = (2.4 FT DEPTH OF INFILTRATION AREA)(HR/2.5 IN)(12 IN/FT) = 11.52 HOURS
- BOTTOM @ 686.00, TOP BERM @ 690.00, 5 FT WIDE SPILLWAY @ 689.50, RISER @ 689.40, 18" HDPE DISCHARGE PIPE 27' LONG @ 13.89% INV. OUT @ 686.00, 5" X 36" ORIFICE @ 688.40, (2) 5" X 24" ORIFICES @ 688.40
- OUTFLOW
  - o Q1 = 0.000 CFS, ELEV @ 687.81
  - o Q2 = 0.000 CFS, ELEV @ 688.30
  - o Q5 = 1.859 CFS, ELEV @ 688.58
  - o Q10 = 5.592 CFS, ELEV @ 688.78
  - o Q25 = 9.083 CFS, ELEV @ 689.03
  - o Q50 = 10.60 CFS, ELEV @ 689.18
  - o Q100 = 12.00 CFS, ELEV @ 689.43
- POST-DEVELOPMENT RELEASE RATE CRITERIA DISTRICT C ON ACT 167 MAP:
  - o 2YR POST TO 1 YR PRE
    - •2YR POST=9.134(2YR PRE)-0.702(2YR CHANGED)+0.396(1YR CHANGED)= 8.828 CFS
  - o 5YR POST TO 5 YR PRE
    - ■5YR POST=14.76(5YR PRE)CFS
  - o 10YR POST TO 10 YR PRE
    - ■10YR POST=22.98(10YR PRE)CFS
  - o 25YR POST TO 25 YR PRE
    - ■25YR POST=34.08(25YR PRE)CFS
  - o 50YR POST TO 50 YR PRE
    - ■50YR POST=40.96(50YR PRE)CFS
  - o 100YR POST TO 100 YR PRE
    - ■100YR POST= 50.30(100YR PRE)CFS

#### O TOTAL POI 1 POST-DEVELOPMENT RUNOFF RATE

- Q1 = 3.881 CFS
- Q2 = 6.145 CFS
- Q5 = 9.927 CFS
- Q10 = 18.91 CFS
- Q25 = 31.23 CFS
- Q50 = 37.26 CFS
- Q100 = 45.11 CFS

DESIGN STORM	PRE-DEV. FLOW/VOLUME- POI 2	POST-DEV. FLOW/VOLUME – POI 2
1-YEAR	5.768 CFS / 22698 CF	3.881 CFS / 15271 CF
2-YEAR	9.134 CFS / 33808 CF	6.145 CFS / 22745 CF
5-YEAR	14.76 CFS / 52558 CF	9.927 CFS / 39037 CF
10-YEAR	22.98 CFS / 80289 CF	18.91 CFS / 64716 CF
25-YEAR	34.08 CFS / 117842 CF	31.23 CFS / 100235 CF
50-YEAR	40.96 CFS / 141430 CF	37.26 CFS / 122814 CF
100-YEAR	50.30 CFS / 173760 CF	45.11 CFS / 1537933 CF

#### SWALE 4

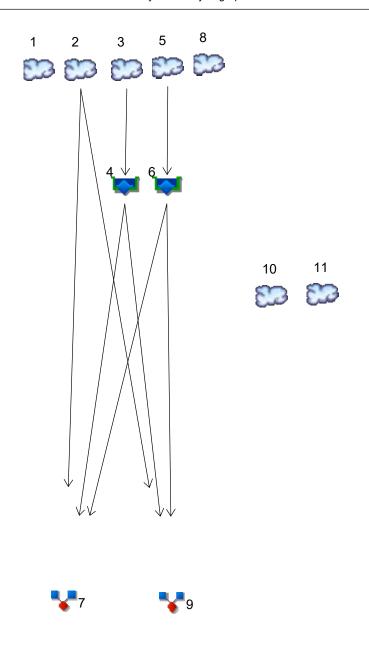
- DRAINAGE AREA = 0.81 ACRES
- CURVE NUMBER
  - 0.07 ACRES LAWN (C SOILS) = 74
  - 0.27 ACRES WOODS (C SOILS) = 70
  - 0.47 ACRES WOODS (D SOILS) = 77
  - WEIGHTED CN = 74

### o TC = 22.8 MINS

- SHEET FLOW = 175' @ 6.90% SLOPE, N=0.4
- SHALLOW CONC = 155' @ 7.82%, UNPAVED
- SHALLOW CONC = 61' @ 3.22%, PAVED
- SHALLOW CONC = 106' @ 14.57%, UNPAVED
- o FLOW = 3.113 CFS (50-YEAR STORM)
- o SLOPE @ 2.8%, DEPTH IS 0.5 FT. AND BOTTOM WIDTH IS 4 FT. SIDE SLOPES 3:1 LEFT, 32:1 RIGHT
- o S75BN MATTING, STAPLE PATTERN D.

### • LEVEL SPREADER 1:

- · 100-YEAR MAX DISCHARGE = 12.00 CFS
- · LENGTH = 13 FOOT PER CFS = 156 FT
- · PROPOSED LEVEL SPREADER TO BE 2 FT DEEP, 1 FT WIDE, AND 156 FT LONG· 6" PERFORATED PIPE RUNNING THROUGH LENGTH OF SPREADER
- · VELOCITY REQUIREMENT FOR DOWNGRADIENT VEGETATION = 4 FT/S
- $\cdot$  Q = CLH<sup>2</sup>/3 5.603 12 = 3(156)H<sup>3</sup>/2 H = 0.026 FT
- $\cdot$  A = 0.026 X 156 = 4.056 FT^2 V = 12/4.056 = 2.96 FT/S ACCEPTABLE



### <u>Legend</u>

<u>Hyd.</u>	<u>Origin</u>	<u>Description</u>
1	SCS Runoff	POI 1 PRE
2	SCS Runoff	POI 1 BYPASS
3	SCS Runoff	TO BERM #1
4	Reservoir	BERM #1
5	SCS Runoff	TO BERM #2
6	Reservoir	BERM #2
7	Combine	TOTAL POST POI 1
8	SCS Runoff	Pre Disturbed Area POI 1
9	Combine	Post to Swale #1
10	SCS Runoff	Post to Swale #2
11	SCS Runoff	Post to Swale #3

Project: 21-4-16 stormwater.gpw

Wednesday, 02 / 21 / 2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	0.885	2	732	4,351				POI 1 PRE
2	SCS Runoff	0.623	2	732	2,706				POI 1 BYPASS
3	SCS Runoff	0.519	2	720	1,209				TO BERM #1
4	Reservoir	0.000	2	1548	0	3	682.06	666	BERM #1
5	SCS Runoff	0.535	2	730	2,158				TO BERM #2
6	Reservoir	0.000	2	1050	0	5	692.35	973	BERM #2
7	Combine	0.623	2	732	2,706	2, 4, 6			TOTAL POST POI 1
8	SCS Runoff	0.704	2	720	1,898				Pre Disturbed Area POI 1
9	Combine	0.623	2	732	2,706	2, 4, 6,			Post to Swale #1
10	SCS Runoff	0.098	2	718	197				Post to Swale #2
11	SCS Runoff	0.073	2	718	151				Post to Swale #3
21-	4-16 stormwa	ater.gpw			Return F	Period: 1 Ye	ear	Wednesda	y, 02 / 21 / 2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	1.484	2	732	6,635				POI 1 PRE
2	SCS Runoff	0.935	2	732	3,904				POI 1 BYPASS
3	SCS Runoff	0.759	2	720	1,744				TO BERM #1
4	Reservoir	0.000	2	1498	0	3	682.36	1,015	BERM #1
5	SCS Runoff	0.815	2	730	3,144				TO BERM #2
6	Reservoir	0.014	2	806	35	5	692.71	1,516	BERM #2
7	Combine	0.935	2	732	3,939	2, 4, 6			TOTAL POST POI 1
8	SCS Runoff	1.229	2	720	3,014				Pre Disturbed Area POI 1
9	Combine	0.935	2	732	3,939	2, 4, 6,			Post to Swale #1
10	SCS Runoff	0.142	2	718	284				Post to Swale #2
11	SCS Runoff	0.112	2	718	227				Post to Swale #3
21-	4-16 stormwa	ater.gpw			Return F	Period: 2 Ye	ear	Wednesda	y, 02 / 21 / 2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	2.507	2	732	10,550				POI 1 PRE
2	SCS Runoff	1.446	2	732	5,884				POI 1 BYPASS
3	SCS Runoff	1.148	2	720	2,628				TO BERM #1
4	Reservoir	0.000	2	1834	0	3	682.88	1,599	BERM #1
5	SCS Runoff	1.275	2	730	4,787				TO BERM #2
6	Reservoir	0.605	2	744	1,169	5	692.90	1,792	BERM #2
7	Combine	1.659	2	742	7,053	2, 4, 6			TOTAL POST POI 1
8	SCS Runoff	2.130	2	720	4,973				Pre Disturbed Area POI 1
9	Combine	1.659	2	742	7,053	2, 4, 6,			Post to Swale #1
10	SCS Runoff	0.213	2	718	428				Post to Swale #2
11	SCS Runoff	0.178	2	718	356				Post to Swale #3
21-	4-16 stormwa	ater apw			Return F	Period: 5 Ye	ear	Wednesda	y, 02 / 21 / 2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	4.023	2	732	16,417				POI 1 PRE
2	SCS Runoff	2.181	2	730	8,758				POI 1 BYPASS
3	SCS Runoff	1.710	2	718	3,911				TO BERM #1
4	Reservoir	0.196	2	740	846	3	683.06	1,897	BERM #1
5	SCS Runoff	1.946	2	728	7,185				TO BERM #2
6	Reservoir	1.455	2	736	3,037	5	693.02	2,015	BERM #2
7	Combine	3.726	2	734	12,642	2, 4, 6			TOTAL POST POI 1
8	SCS Runoff	3.477	2	720	7,975				Pre Disturbed Area POI 1
9	Combine	3.726	2	734	12,642	2, 4, 6,			Post to Swale #1
10	SCS Runoff	0.316	2	716	638				Post to Swale #2
11	SCS Runoff	0.273	2	718	550				Post to Swale #3
21_	4-16 stormwa	ater anw			Return F	Period: 10 \	/ear	Wednesda	y, 02 / 21 / 2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	6.077	2	730	24,449				POI 1 PRE
2	SCS Runoff	3.151	2	730	12,592				POI 1 BYPASS
3	SCS Runoff	2.448	2	718	5,623				TO BERM #1
4	Reservoir	1.108	2	726	2,328	3	683.23	2,355	BERM #1
5	SCS Runoff	2.834	2	728	10,401				TO BERM #2
6	Reservoir	2.146	2	736	5,738	5	693.19	2,496	BERM #2
7	Combine	6.052	2	730	20,657	2, 4, 6			TOTAL POST POI 1
8	SCS Runoff	5.307	2	720	12,155				Pre Disturbed Area POI 1
9	Combine	6.052	2	730	20,657	2, 4, 6,			Post to Swale #1
10	SCS Runoff	0.450	2	716	917				Post to Swale #2
11	SCS Runoff	0.402	2	716	812				Post to Swale #3
21_	4-16 stormwa	ater anw			Return F	Period: 25	/ear	Wednesda	y, 02 / 21 / 2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	7.371	2	730	29,526				POI 1 PRE
2	SCS Runoff	3.747	2	730	14,978				POI 1 BYPASS
3	SCS Runoff	2.899	2	718	6,689				TO BERM #1
4	Reservoir	1.594	2	724	3,284	3	683.32	2,592	BERM #1
5	SCS Runoff	3.381	2	728	12,408				TO BERM #2
6	Reservoir	2.515	2	736	7,488	5	693.31	2,833	BERM #2
7	Combine	7.364	2	730	25,750	2, 4, 6			TOTAL POST POI 1
8	SCS Runoff	6.480	2	718	14,826				Pre Disturbed Area POI 1
9	Combine	7.364	2	730	25,750	2, 4, 6,			Post to Swale #1
10	SCS Runoff	0.533	2	716	1,091				Post to Swale #2
11	SCS Runoff	0.482	2	716	978				Post to Swale #3
21-	4-16 stormwa	ater apw			Return F	Period: 50 \	(ear	Wednesda	y, 02 / 21 / 2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	9.137	2	730	36,514				POI 1 PRE
2	SCS Runoff	4.551	2	730	18,230				POI 1 BYPASS
3	SCS Runoff	3.505	2	718	8,142				TO BERM #1
4	Reservoir	2.431	2	724	4,629	3	683.43	2,891	BERM #1
5	SCS Runoff	4.120	2	728	15,148				TO BERM #2
6	Reservoir	3.307	2	736	9,943	5	693.45	3,240	BERM #2
7	Combine	9.091	2	732	32,803	2, 4, 6			TOTAL POST POI 1
8	SCS Runoff	8.093	2	718	18,526				Pre Disturbed Area POI 1
9	Combine	9.091	2	732	32,803	2, 4, 6,			Post to Swale #1
10	SCS Runoff	0.643	2	716	1,327				Post to Swale #2
11	SCS Runoff	0.591	2	716	1,206				Post to Swale #3
21-	4-16 stormwa	ater.gpw			Return F	Period: 100	Year	Wednesda	y, 02 / 21 / 2024

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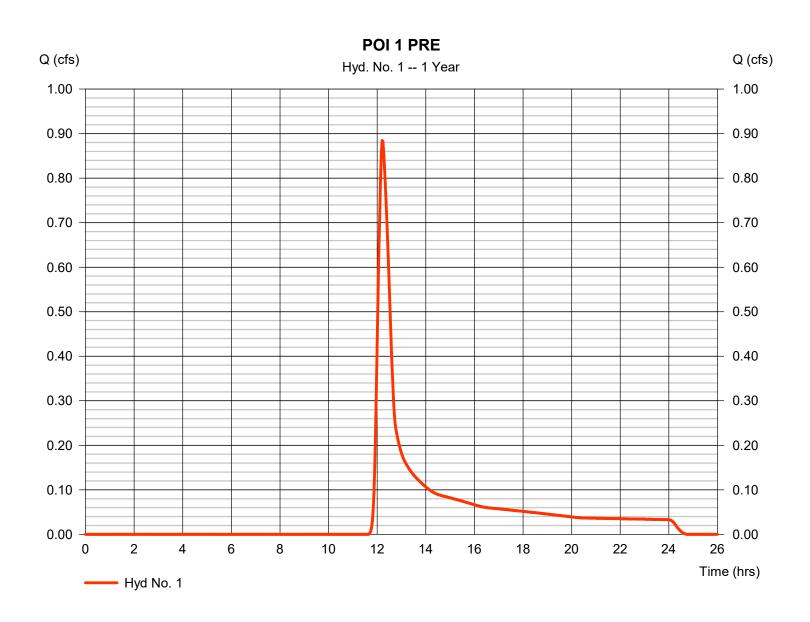
Wednesday, 02 / 21 / 2024

### Hyd. No. 1

POI 1 PRE

Hydrograph type = SCS Runoff Peak discharge = 0.885 cfsStorm frequency = 1 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 4.351 cuftCurve number = 73\* Drainage area = 2.330 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 28.20 min = TR55 Total precip. Distribution = Type II = 2.40 inStorm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.150 \times 98) + (0.290 \times 77) + (1.740 \times 70) + (0.150 \times 80)] / 2.330$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 24 hrs

Wednesday, 02 / 21 / 2024

= 484

### Hyd. No. 2

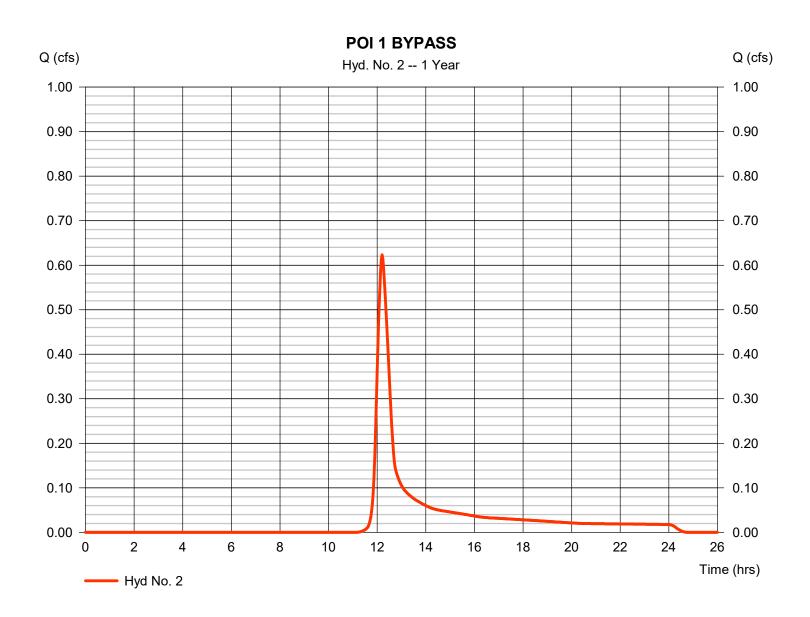
POI 1 BYPASS

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 0.623 cfsStorm frequency = 1 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 2.706 cuftCurve number = 78\* Drainage area = 1.030 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 27.70 min = TR55 Total precip. Distribution = Type II = 2.40 in

Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.110 \times 77) + (0.200 \times 98) + (0.100 \times 79) + (0.300 \times 71) + (0.290 \times 70) + (0.030 \times 78)] / 1.030$ 



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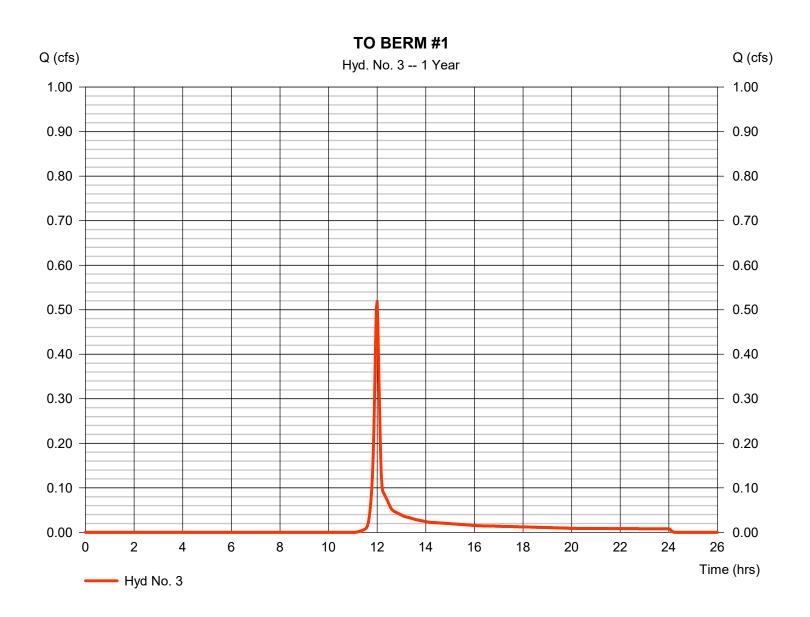
Wednesday, 02 / 21 / 2024

### Hyd. No. 3

TO BERM #1

Hydrograph type = SCS Runoff Peak discharge = 0.519 cfsStorm frequency = 1 yrsTime to peak  $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 1,209 cuftCurve number = 78\* Drainage area = 0.460 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = TR55  $= 9.00 \, \text{min}$ Total precip. Distribution = Type II = 2.40 inStorm duration Shape factor = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.080 \times 98) + (0.180 \times 74) + (0.070 \times 71) + (0.070 \times 70) + (0.010 \times 77) + (0.050 \times 80)] / 0.460$ 



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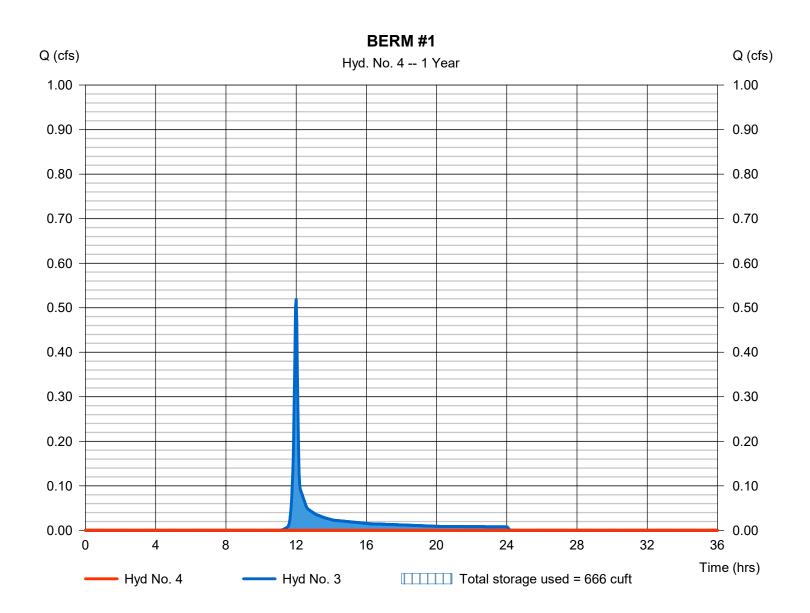
Wednesday, 02 / 21 / 2024

### Hyd. No. 4

BERM #1

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency Time to peak  $= 25.80 \, hrs$ = 1 yrsTime interval = 2 min Hyd. volume = 0 cuft Inflow hyd. No. Max. Elevation = 3 - TO BERM #1 = 682.06 ft= BERM #1 Reservoir name Max. Storage = 666 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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= 24 hrs

Wednesday, 02 / 21 / 2024

= 484

### Hyd. No. 5

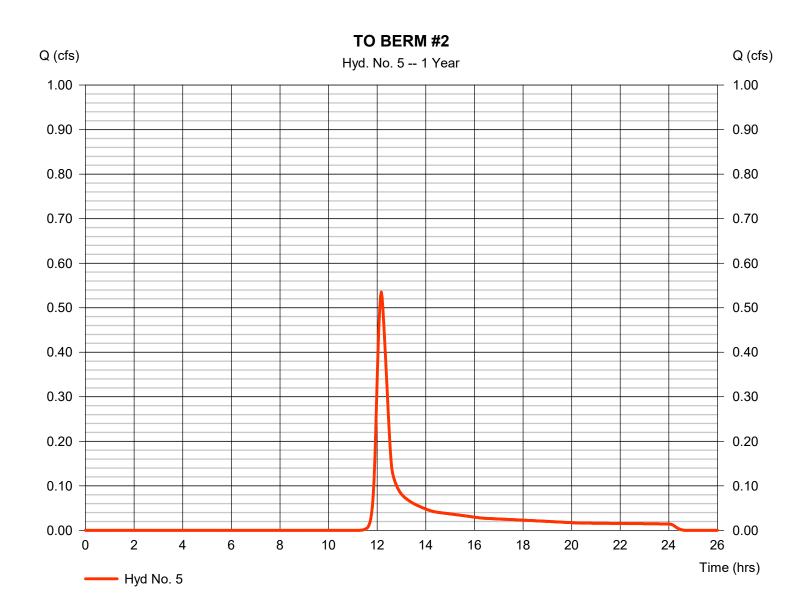
TO BERM #2

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 0.535 cfsStorm frequency = 1 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 2.158 cuft Curve number Drainage area = 0.890 ac= 77\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 26.60 min = TR55 Total precip. Distribution = Type II = 2.40 in

Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.130 \times 98) + (0.130 \times 71) + (0.170 \times 70) + (0.300 \times 74) + (0.100 \times 77) + (0.060 \times 80)] / 0.890$ 



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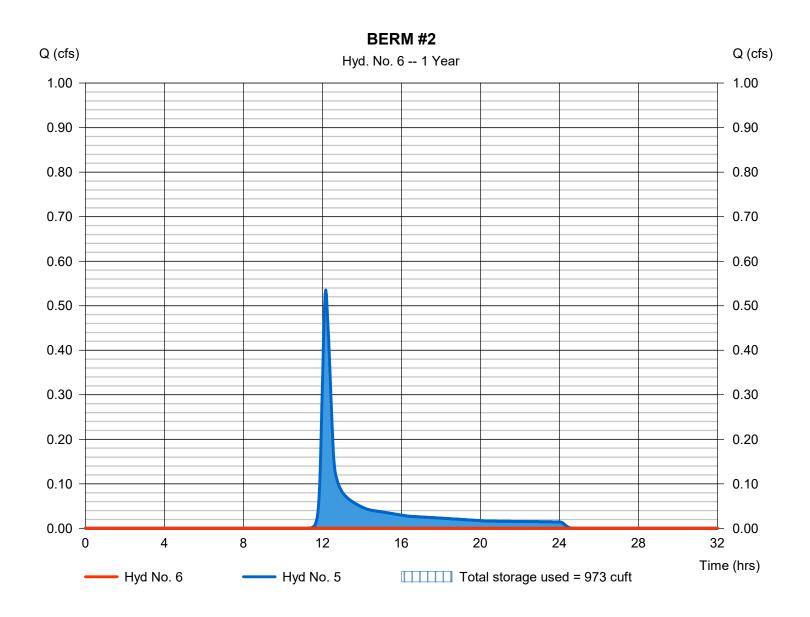
Wednesday, 02 / 21 / 2024

### Hyd. No. 6

BERM #2

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency Time to peak  $= 17.50 \, hrs$ = 1 yrsTime interval = 2 min Hyd. volume = 0 cuft = 5 - TO BERM #2 Max. Elevation  $= 692.35 \, ft$ Inflow hyd. No. = BERM #2 Reservoir name Max. Storage = 973 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



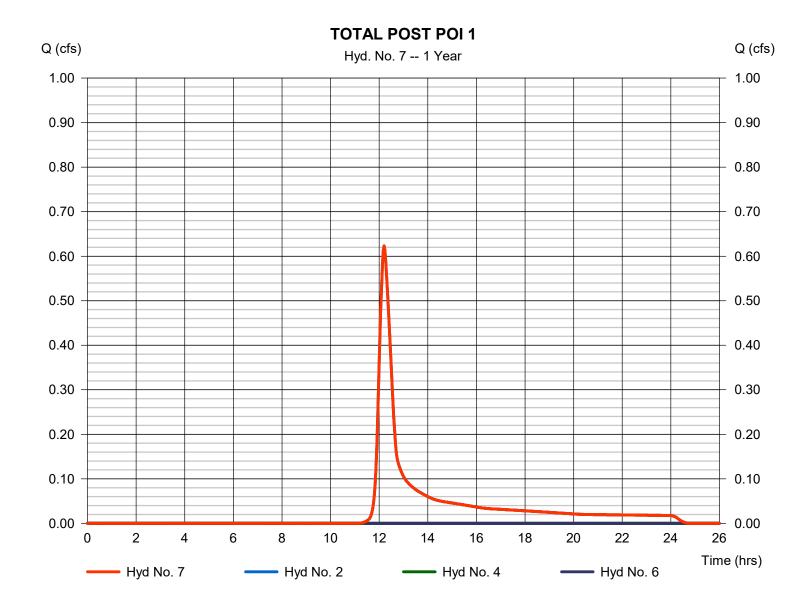
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Wednesday, 02 / 21 / 2024

### Hyd. No. 7

**TOTAL POST POI 1** 

Hydrograph type = Combine Peak discharge = 0.623 cfsTime to peak Storm frequency = 1 yrs $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 2,706 cuft Inflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac



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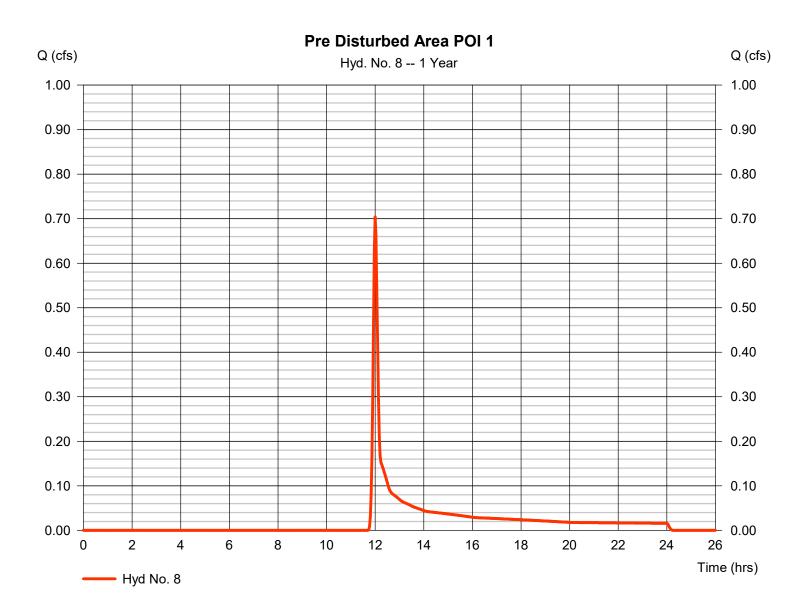
Wednesday, 02 / 21 / 2024

### Hyd. No. 8

Pre Disturbed Area POI 1

Hydrograph type = SCS Runoff Peak discharge = 0.704 cfsStorm frequency Time to peak  $= 12.00 \, hrs$ = 1 yrsTime interval = 2 min Hyd. volume = 1,898 cuft Drainage area = 1.280 acCurve number = 70\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 7.60 \, \text{min}$ = TR55 Total precip. = 2.40 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 77) + (1.210 x 70)] / 1.280



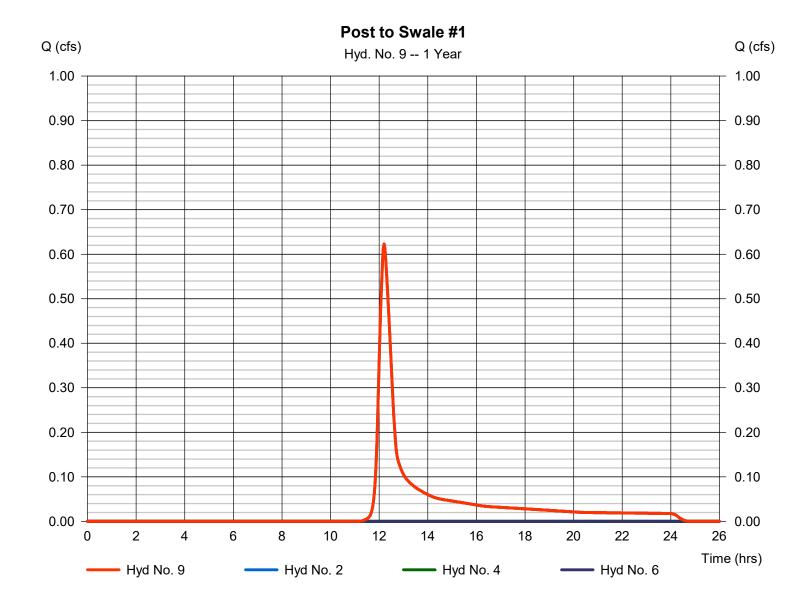
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Wednesday, 02 / 21 / 2024

### Hyd. No. 9

Post to Swale #1

Hydrograph type = Combine Peak discharge = 0.623 cfsTime to peak Storm frequency = 1 yrs $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 2,706 cuftInflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac



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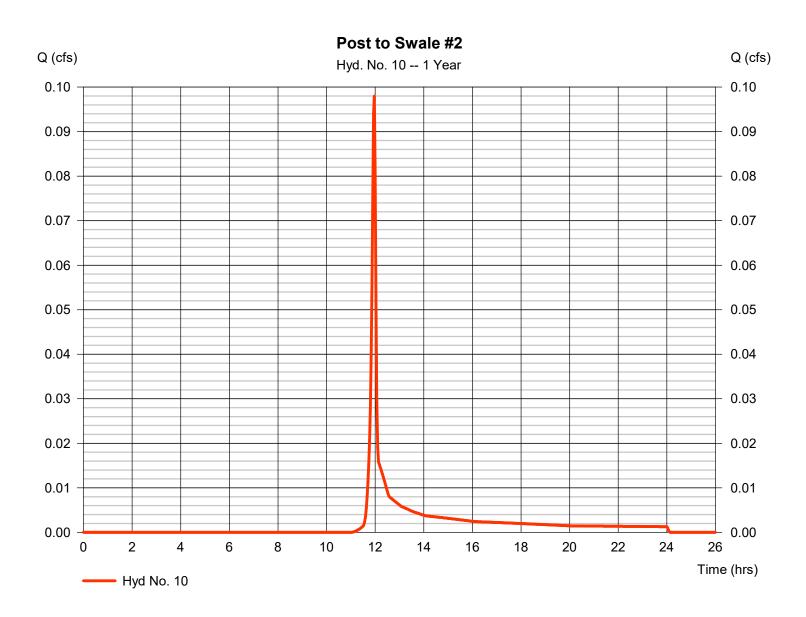
Wednesday, 02 / 21 / 2024

### Hyd. No. 10

Post to Swale #2

Hydrograph type = SCS Runoff Peak discharge = 0.098 cfsStorm frequency = 1 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 197 cuft Curve number Drainage area = 0.080 ac= 78\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 5.00 min = User Total precip. = 2.40 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.050 \times 80) + (0.010 \times 74) + (0.010 \times 77) + (0.010 \times 70)] / 0.080$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

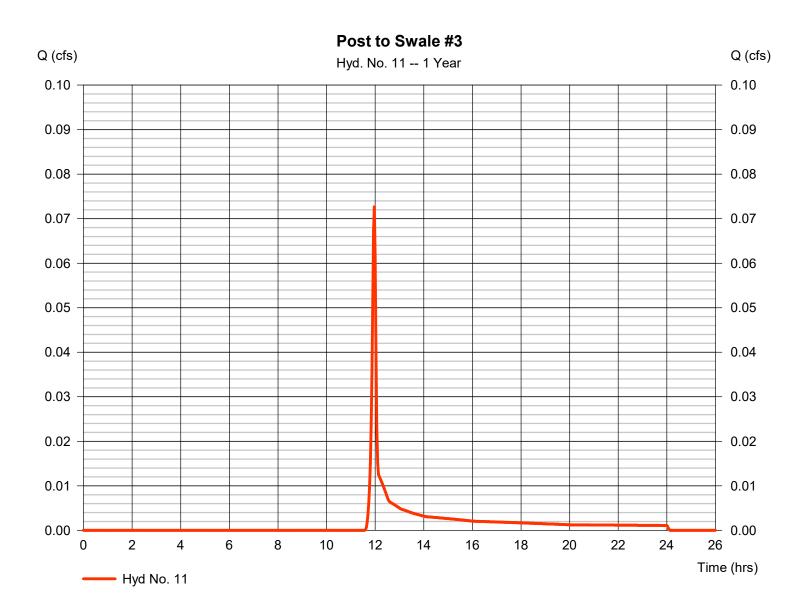
Wednesday, 02 / 21 / 2024

### Hyd. No. 11

Post to Swale #3

Hydrograph type = SCS Runoff Peak discharge = 0.073 cfsStorm frequency = 1 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 151 cuft Drainage area Curve number = 0.080 ac= 74\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 5.00 min = User Total precip. = 2.40 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.070 \times 74) + (0.010 \times 70)] / 0.080$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

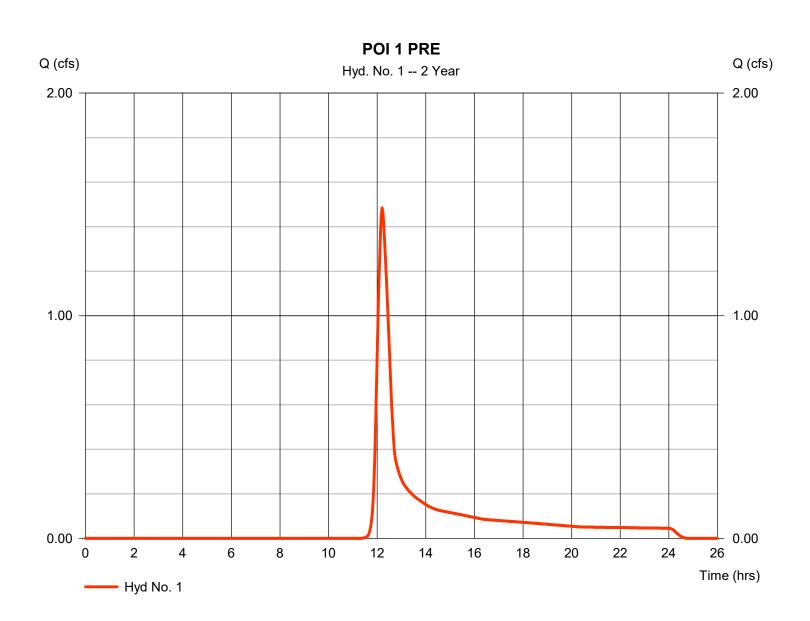
Wednesday, 02 / 21 / 2024

### Hyd. No. 1

POI 1 PRE

Hydrograph type = SCS Runoff Peak discharge = 1.484 cfsStorm frequency = 2 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 6,635 cuft= 73\* Drainage area = 2.330 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 28.20 min = TR55 Total precip. = 2.88 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.150 \times 98) + (0.290 \times 77) + (1.740 \times 70) + (0.150 \times 80)] / 2.330$ 



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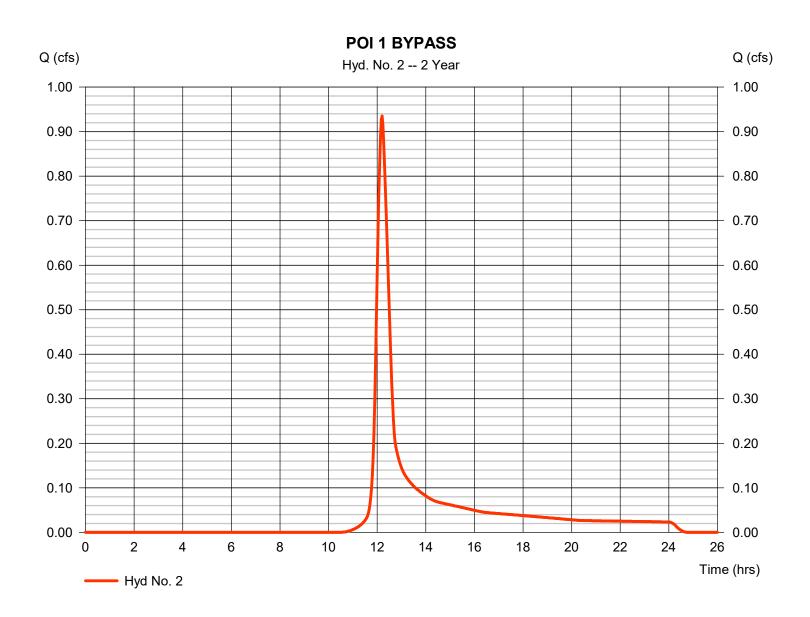
Wednesday, 02 / 21 / 2024

### Hyd. No. 2

POI 1 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 0.935 cfsStorm frequency = 2 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 3.904 cuft Curve number = 78\* Drainage area = 1.030 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 27.70 min = TR55 Total precip. = 2.88 inDistribution = Type II Storm duration Shape factor = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.110 \times 77) + (0.200 \times 98) + (0.100 \times 79) + (0.300 \times 71) + (0.290 \times 70) + (0.030 \times 78)] / 1.030$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

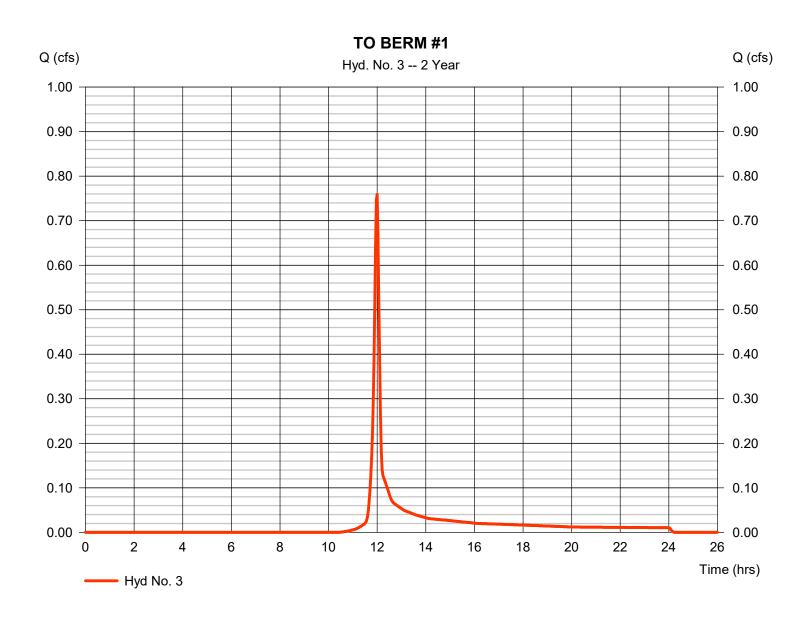
Wednesday, 02 / 21 / 2024

### Hyd. No. 3

TO BERM #1

Hydrograph type = SCS Runoff Peak discharge = 0.759 cfsStorm frequency = 2 yrsTime to peak  $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 1,744 cuft Curve number = 78\* Drainage area = 0.460 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = TR55  $= 9.00 \, \text{min}$ Total precip. = 2.88 inDistribution = Type II Storm duration Shape factor = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.080 \times 98) + (0.180 \times 74) + (0.070 \times 71) + (0.070 \times 70) + (0.010 \times 77) + (0.050 \times 80)] / 0.460$ 



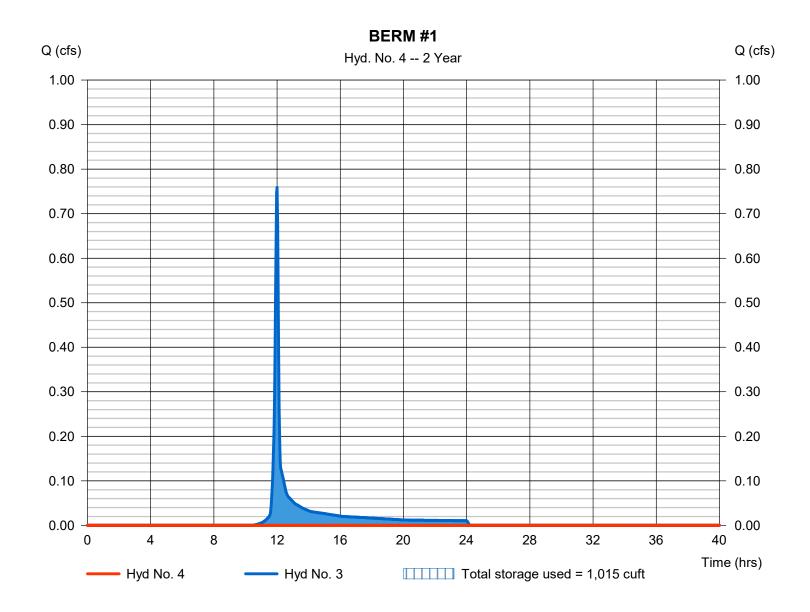
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#### Hyd. No. 4

BERM #1

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency = 2 yrsTime to peak  $= 24.97 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Inflow hyd. No. Max. Elevation = 3 - TO BERM #1 = 682.36 ft= BERM #1 Reservoir name Max. Storage = 1,015 cuft



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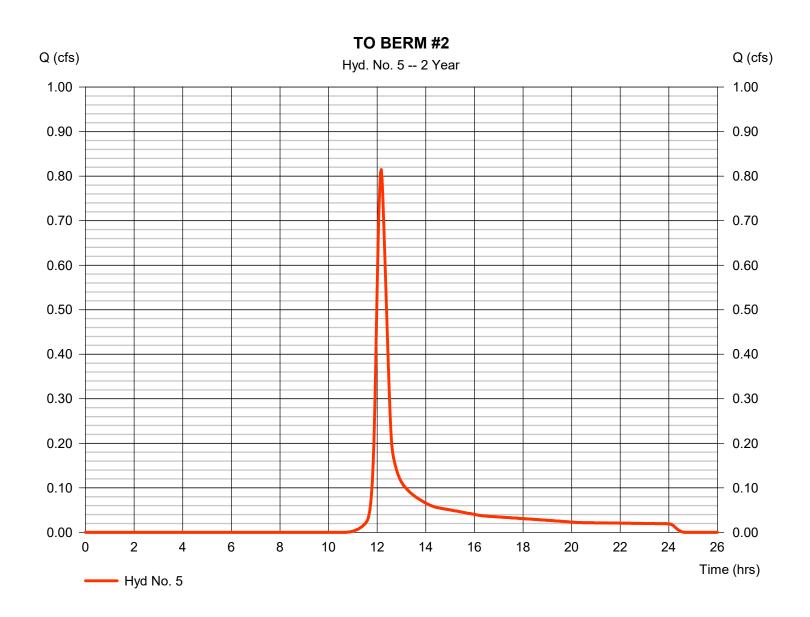
Wednesday, 02 / 21 / 2024

#### Hyd. No. 5

TO BERM #2

Hydrograph type = SCS Runoff Peak discharge = 0.815 cfsStorm frequency = 2 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 3,144 cuftCurve number Drainage area = 0.890 ac= 77\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 26.60 min = TR55 Total precip. = 2.88 inDistribution = Type II Storm duration Shape factor = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.130 \times 98) + (0.130 \times 71) + (0.170 \times 70) + (0.300 \times 74) + (0.100 \times 77) + (0.060 \times 80)] / 0.890$ 



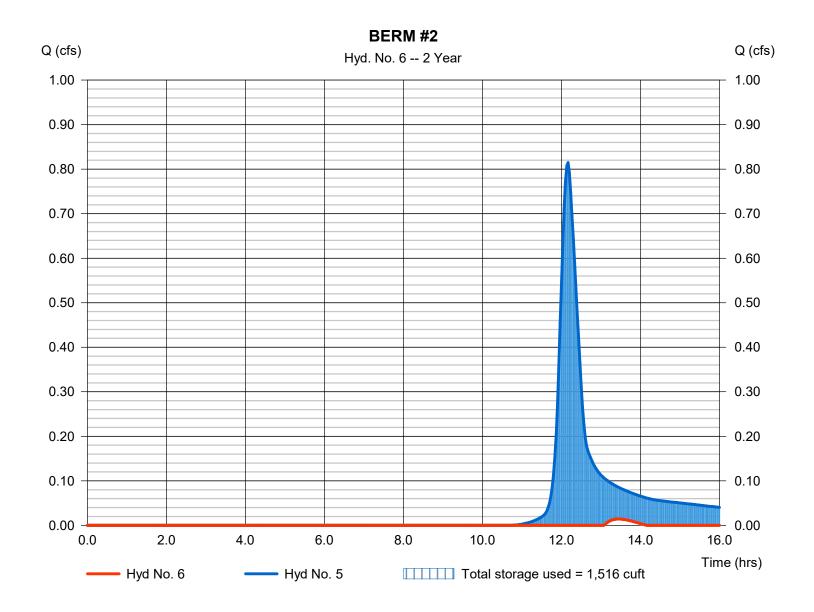
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#### Hyd. No. 6

BERM #2

Hydrograph type Peak discharge = 0.014 cfs= Reservoir Storm frequency = 2 yrsTime to peak  $= 13.43 \, hrs$ Time interval = 2 min Hyd. volume = 35 cuft = 5 - TO BERM #2 Max. Elevation Inflow hyd. No.  $= 692.71 \, \text{ft}$ = BERM #2 Reservoir name Max. Storage = 1,516 cuft



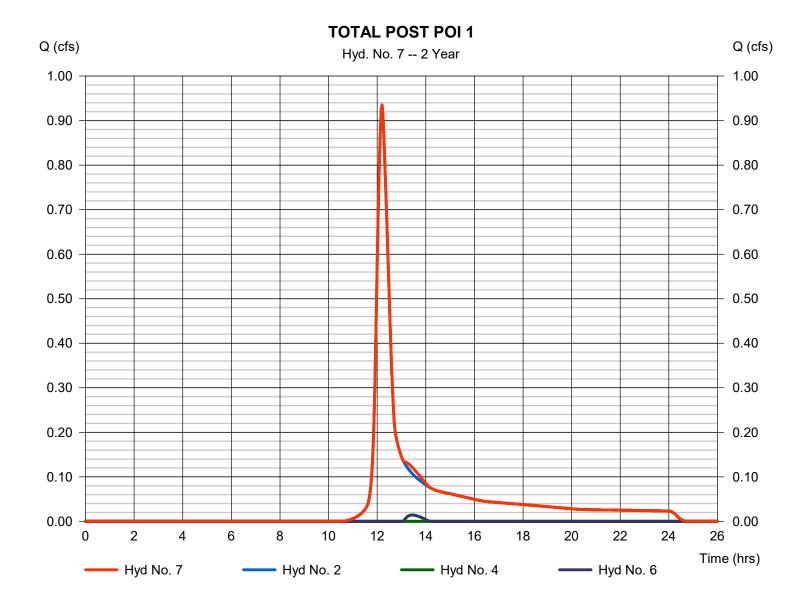
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#### Hyd. No. 7

**TOTAL POST POI 1** 

Hydrograph type = Combine Peak discharge = 0.935 cfsTime to peak Storm frequency = 2 yrs $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 3,939 cuftInflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac



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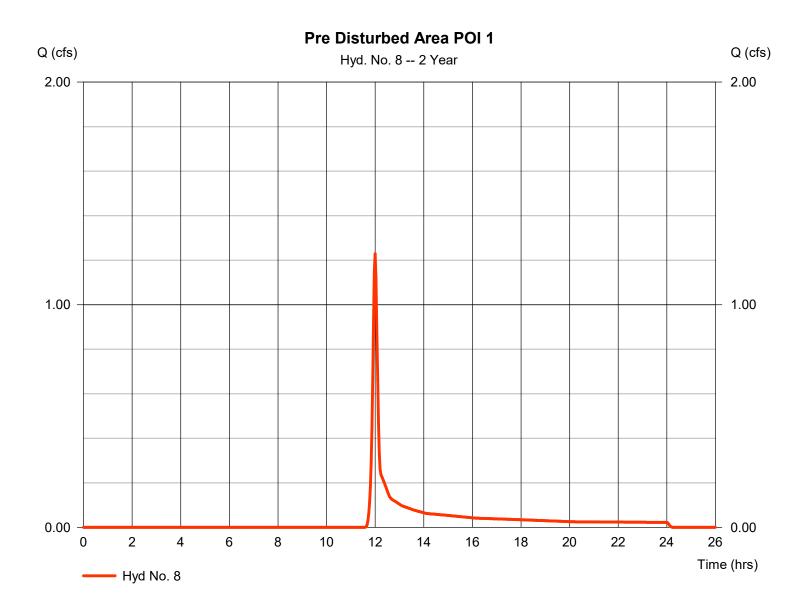
Wednesday, 02 / 21 / 2024

#### Hyd. No. 8

Pre Disturbed Area POI 1

Hydrograph type = SCS Runoff Peak discharge = 1.229 cfsStorm frequency = 2 yrsTime to peak  $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 3.014 cuft = 1.280 acCurve number = 70\* Drainage area Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 7.60 \, \text{min}$ = TR55 Total precip. = 2.88 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 77) + (1.210 x 70)] / 1.280



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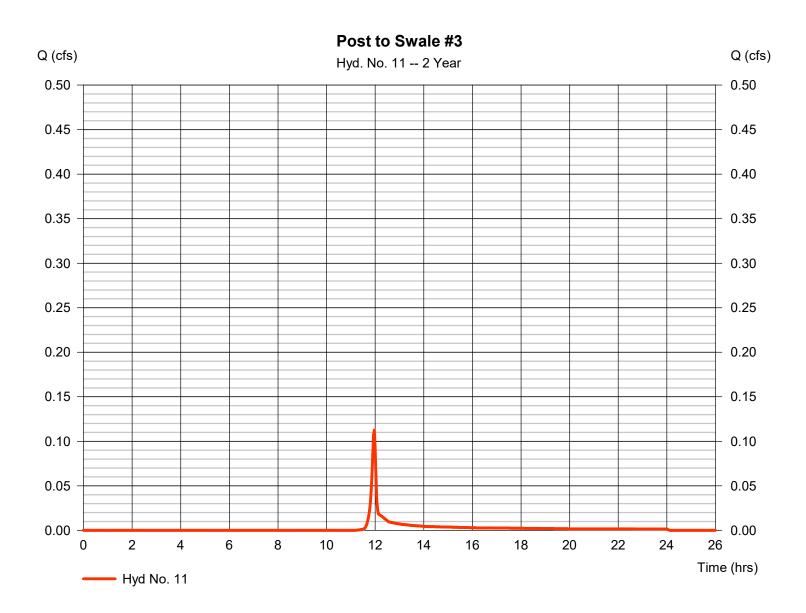
Wednesday, 02 / 21 / 2024

#### Hyd. No. 11

Post to Swale #3

Hydrograph type = SCS Runoff Peak discharge = 0.112 cfsStorm frequency = 2 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 227 cuft Drainage area Curve number = 0.080 ac= 74\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 5.00 min = User Total precip. = 2.88 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 74) + (0.010 x 70)] / 0.080



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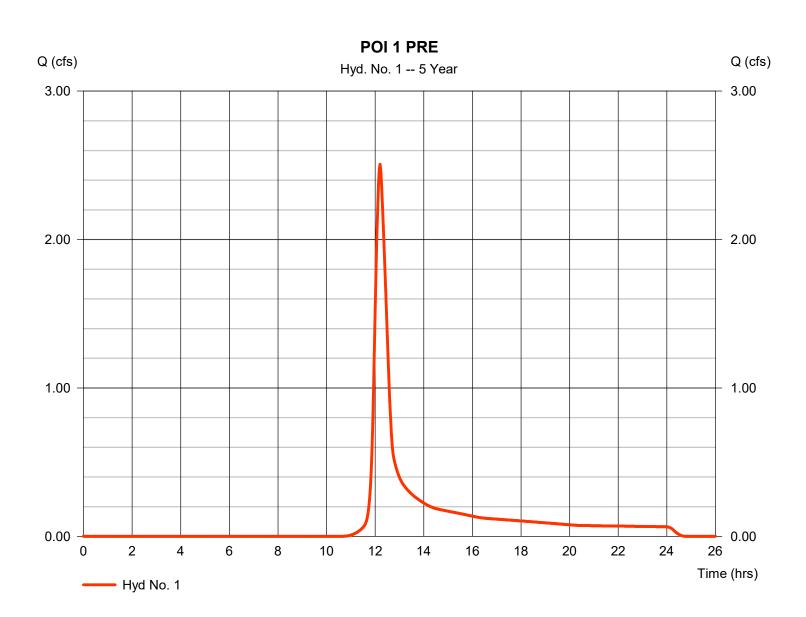
Wednesday, 02 / 21 / 2024

#### Hyd. No. 1

POI 1 PRE

Hydrograph type = SCS Runoff Peak discharge = 2.507 cfsStorm frequency = 5 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 10,550 cuftDrainage area = 2.330 acCurve number = 73\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 28.20 min = TR55 Total precip. Distribution = Type II = 3.60 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.150 \times 98) + (0.290 \times 77) + (1.740 \times 70) + (0.150 \times 80)] / 2.330$ 



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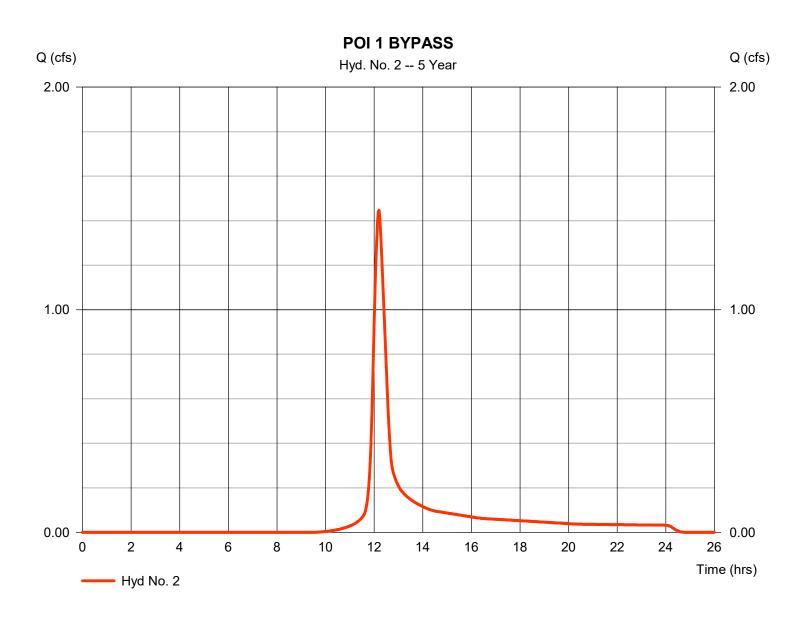
Wednesday, 02 / 21 / 2024

#### Hyd. No. 2

POI 1 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 1.446 cfsStorm frequency = 5 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 5.884 cuft = 78\* Drainage area = 1.030 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 27.70 min = TR55 Total precip. Distribution = Type II = 3.60 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.110 \times 77) + (0.200 \times 98) + (0.100 \times 79) + (0.300 \times 71) + (0.290 \times 70) + (0.030 \times 78)] / 1.030$ 



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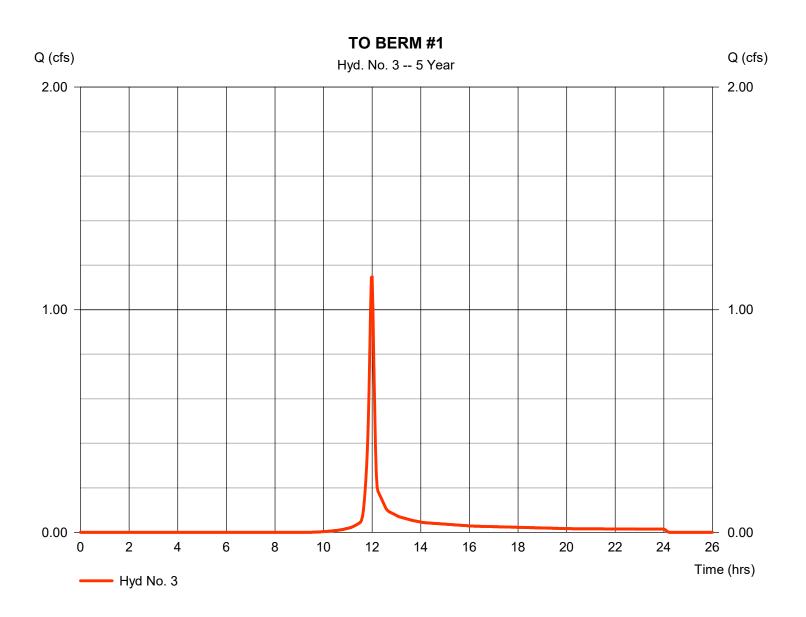
Wednesday, 02 / 21 / 2024

#### Hyd. No. 3

TO BERM #1

Hydrograph type = SCS Runoff Peak discharge = 1.148 cfsStorm frequency = 5 yrsTime to peak  $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 2,628 cuft = 78\* Drainage area = 0.460 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 9.00 min = TR55 Total precip. = 3.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.080 \times 98) + (0.180 \times 74) + (0.070 \times 71) + (0.070 \times 70) + (0.010 \times 77) + (0.050 \times 80)] / 0.460$ 



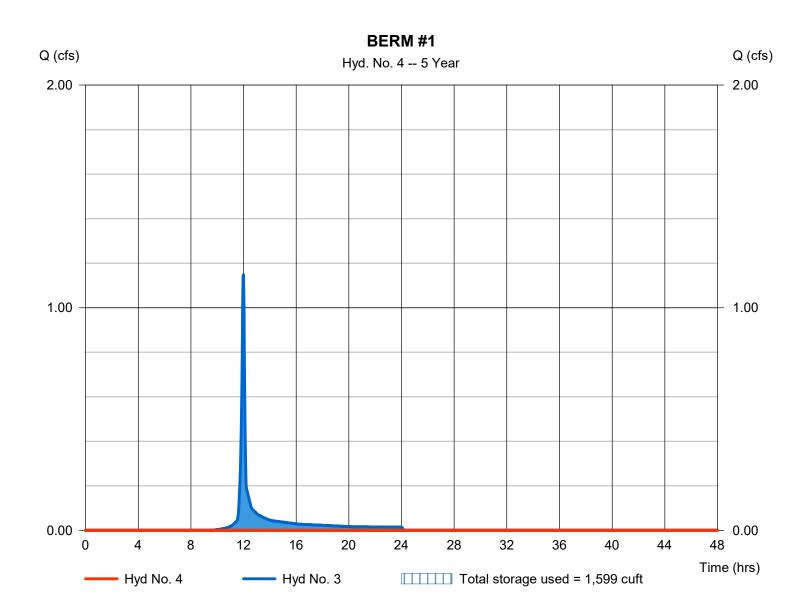
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### Hyd. No. 4

BERM #1

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency = 5 yrsTime to peak  $= 30.57 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft = 3 - TO BERM #1 Max. Elevation Inflow hyd. No. = 682.88 ft= BERM #1 Reservoir name Max. Storage = 1,599 cuft



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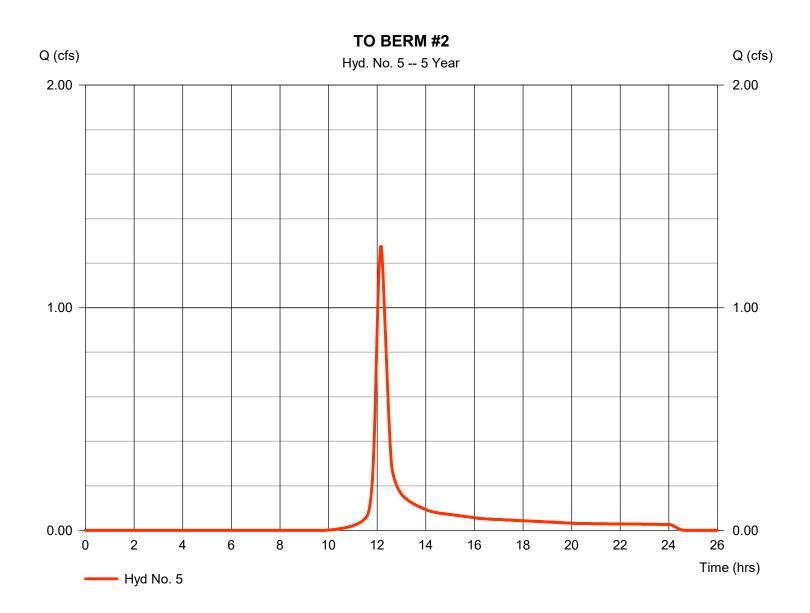
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#### Hyd. No. 5

TO BERM #2

Hydrograph type = SCS Runoff Peak discharge = 1.275 cfsStorm frequency = 5 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 4,787 cuft= 77\* Drainage area = 0.890 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 26.60 min = TR55 Total precip. Distribution = Type II = 3.60 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.130 \times 98) + (0.130 \times 71) + (0.170 \times 70) + (0.300 \times 74) + (0.100 \times 77) + (0.060 \times 80)] / 0.890$ 



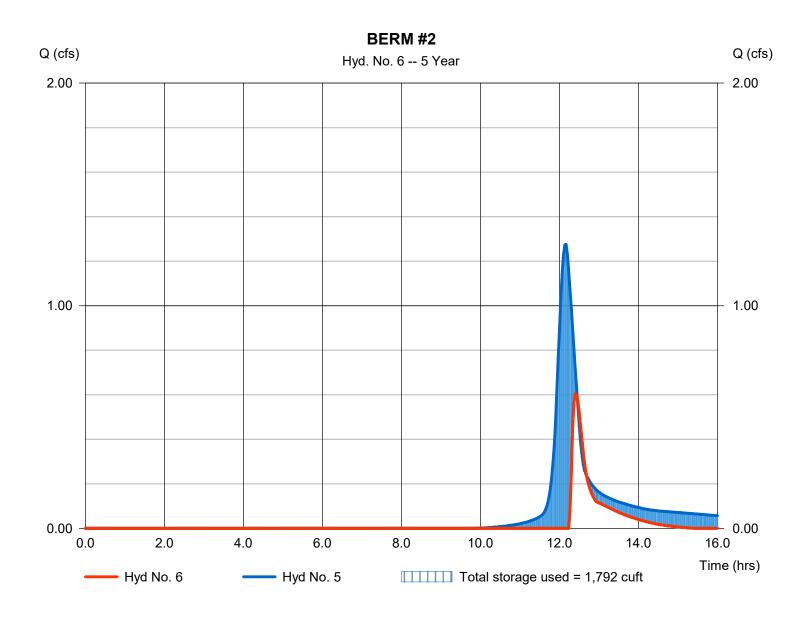
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#### Hyd. No. 6

BERM #2

Hydrograph type Peak discharge = 0.605 cfs= Reservoir Storm frequency = 5 yrsTime to peak  $= 12.40 \, hrs$ Time interval = 2 min Hyd. volume = 1,169 cuft= 5 - TO BERM #2 Max. Elevation Inflow hyd. No. = 692.90 ft= BERM #2 Reservoir name Max. Storage = 1,792 cuft



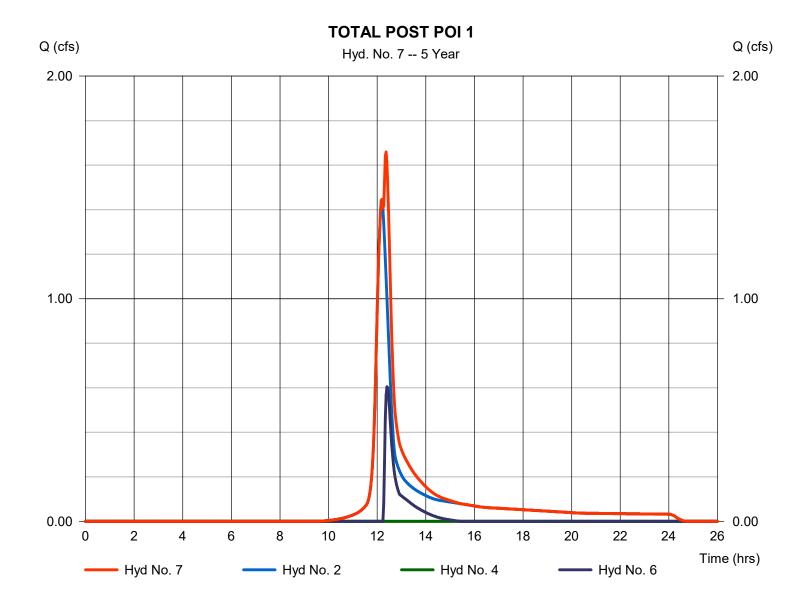
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#### Hyd. No. 7

**TOTAL POST POI 1** 

Hydrograph type = Combine Peak discharge = 1.659 cfsStorm frequency Time to peak = 5 yrs $= 12.37 \, hrs$ Time interval = 2 min Hyd. volume = 7,053 cuftInflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac



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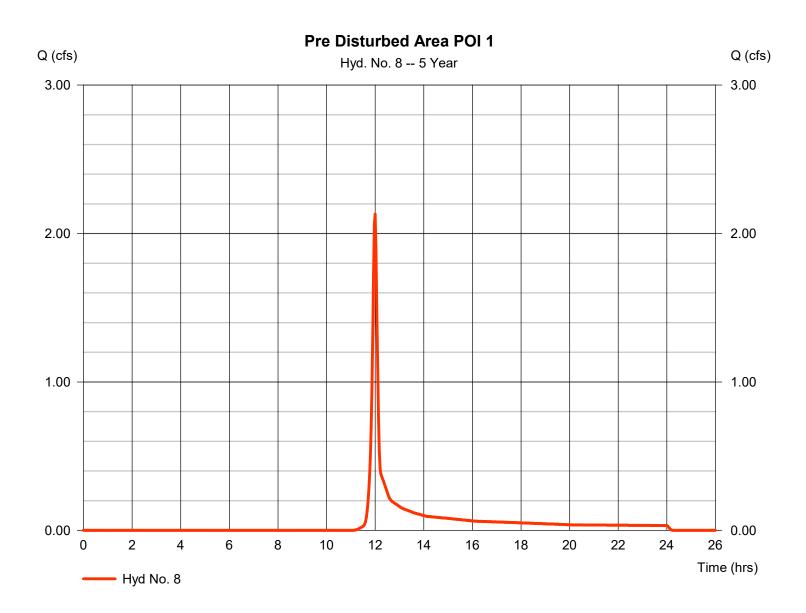
Wednesday, 02 / 21 / 2024

#### Hyd. No. 8

Pre Disturbed Area POI 1

Hydrograph type = SCS Runoff Peak discharge = 2.130 cfsStorm frequency = 5 yrsTime to peak  $= 12.00 \, hrs$ Time interval = 2 min Hyd. volume = 4,973 cuft= 1.280 acCurve number = 70\* Drainage area Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 7.60 \, \text{min}$ = TR55 Total precip. = 3.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 77) + (1.210 x 70)] / 1.280



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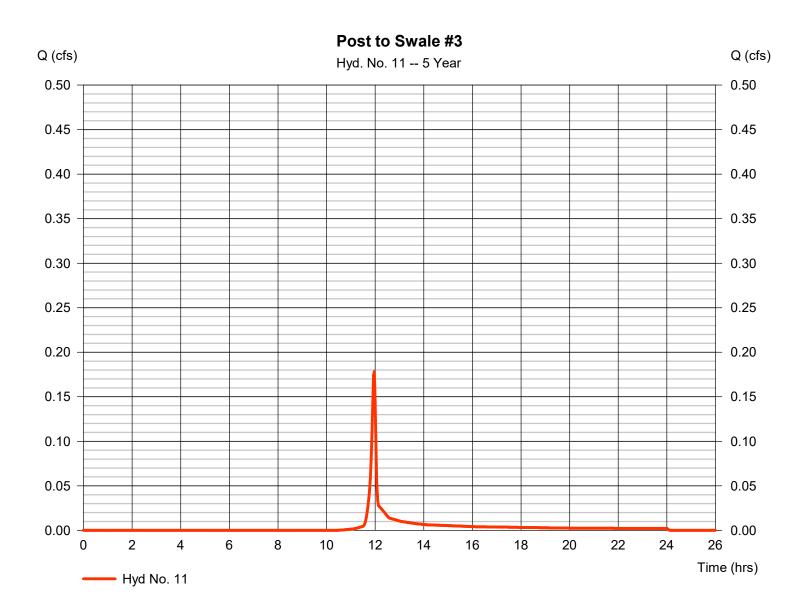
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#### Hyd. No. 11

Post to Swale #3

Hydrograph type = SCS Runoff Peak discharge = 0.178 cfsStorm frequency = 5 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 356 cuft Drainage area Curve number = 0.080 ac= 74\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 5.00 min = User Total precip. Distribution = Type II = 3.60 inStorm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 74) + (0.010 x 70)] / 0.080



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#### Hyd. No. 1

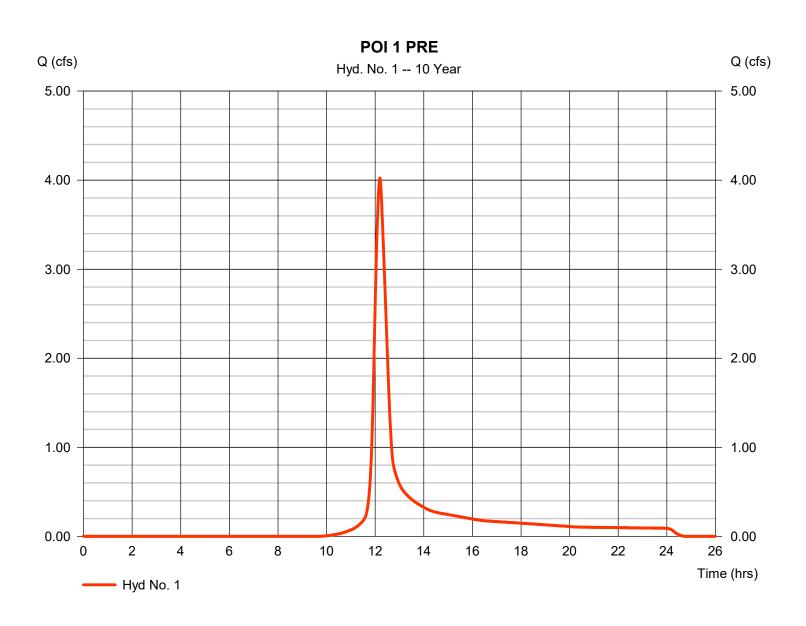
POI 1 PRE

Hydrograph type = SCS Runoff Peak discharge = 4.023 cfsStorm frequency = 10 yrsTime to peak  $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 16.417 cuft Drainage area = 2.330 acCurve number = 73\* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) = 28.20 min Tc method = TR55

Total precip. = 4.56 in Distribution = Type II

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.150 \times 98) + (0.290 \times 77) + (1.740 \times 70) + (0.150 \times 80)] / 2.330$ 



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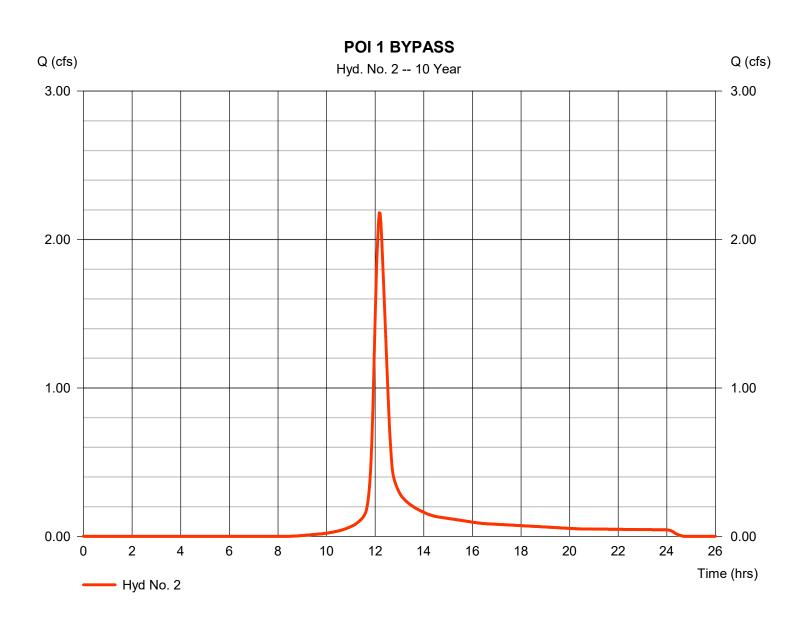
Wednesday, 02 / 21 / 2024

#### Hyd. No. 2

POI 1 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 2.181 cfsStorm frequency = 10 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 8,758 cuft = 78\* Drainage area = 1.030 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) = 27.70 min Tc method = TR55 Total precip. = 4.56 inDistribution = Type II Storm duration = 24 hrs = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.110 \times 77) + (0.200 \times 98) + (0.100 \times 79) + (0.300 \times 71) + (0.290 \times 70) + (0.030 \times 78)] / 1.030$ 



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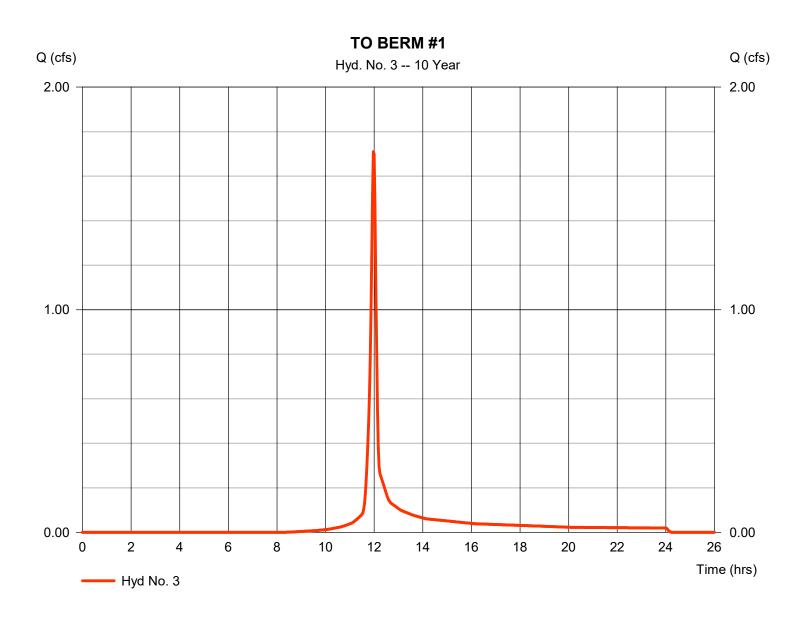
Wednesday, 02 / 21 / 2024

#### Hyd. No. 3

TO BERM #1

Hydrograph type = SCS Runoff Peak discharge = 1.710 cfsStorm frequency = 10 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 3,911 cuft= 78\* Drainage area = 0.460 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 9.00 min = TR55 Total precip. = 4.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.080 \times 98) + (0.180 \times 74) + (0.070 \times 71) + (0.070 \times 70) + (0.010 \times 77) + (0.050 \times 80)] / 0.460$ 



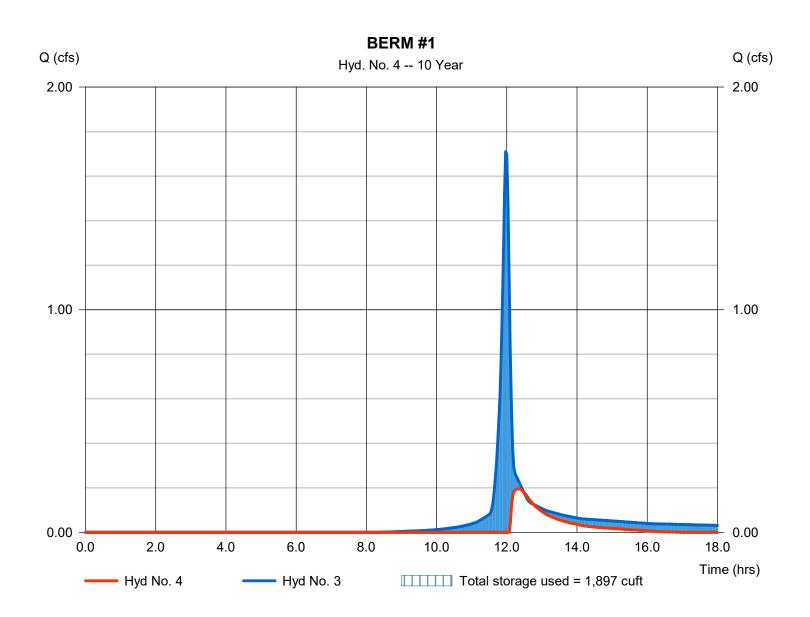
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### Hyd. No. 4

BERM #1

Hydrograph type = Reservoir Peak discharge = 0.196 cfsStorm frequency = 10 yrsTime to peak  $= 12.33 \, hrs$ Time interval = 2 min Hyd. volume = 846 cuft Inflow hyd. No. = 3 - TO BERM #1 Max. Elevation = 683.06 ft= BERM #1 Reservoir name Max. Storage = 1,897 cuft



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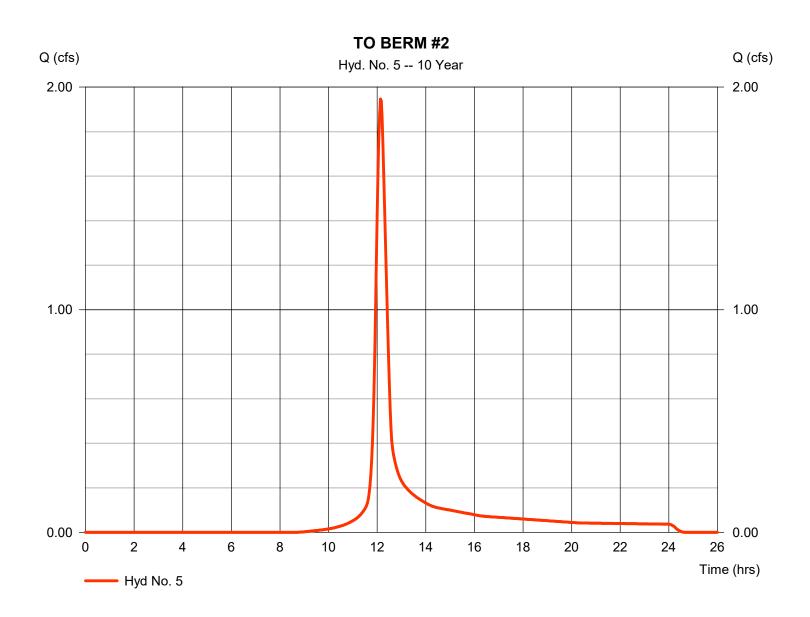
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#### Hyd. No. 5

TO BERM #2

Hydrograph type = SCS Runoff Peak discharge = 1.946 cfsStorm frequency = 10 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 7,185 cuftDrainage area = 0.890 acCurve number = 77\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 26.60 min = TR55 Total precip. = 4.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.130 \times 98) + (0.130 \times 71) + (0.170 \times 70) + (0.300 \times 74) + (0.100 \times 77) + (0.060 \times 80)] / 0.890$ 



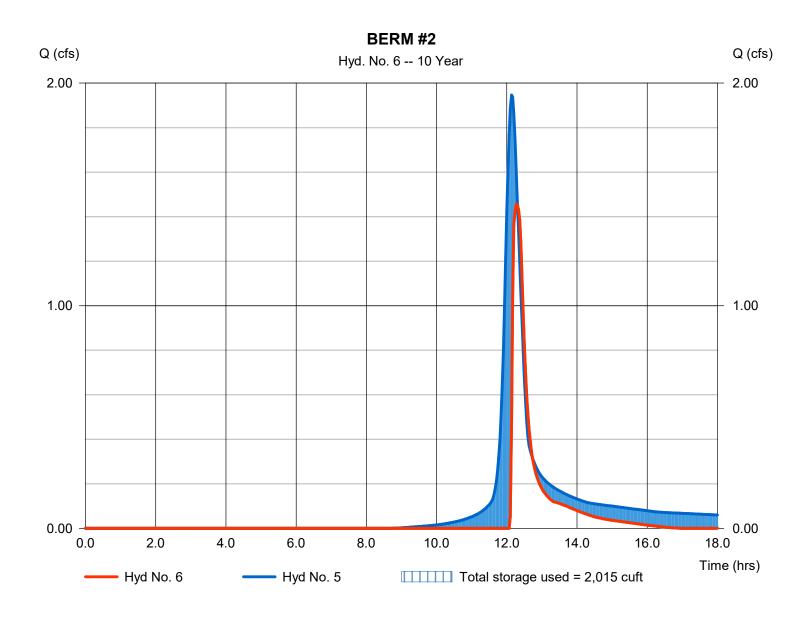
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#### Hyd. No. 6

BERM #2

Hydrograph type = Reservoir Peak discharge = 1.455 cfsStorm frequency = 10 yrsTime to peak  $= 12.27 \, hrs$ Time interval = 2 min Hyd. volume = 3,037 cuftInflow hyd. No. = 5 - TO BERM #2 Max. Elevation = 693.02 ft= BERM #2 Reservoir name Max. Storage = 2,015 cuft



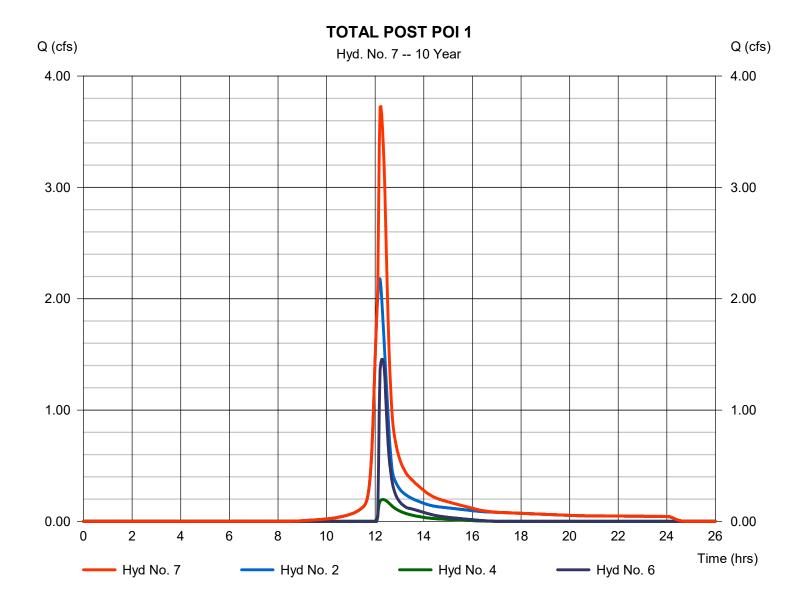
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#### Hyd. No. 7

**TOTAL POST POI 1** 

Hydrograph type = Combine Peak discharge = 3.726 cfsTime to peak Storm frequency = 10 yrs $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 12,642 cuft Inflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac



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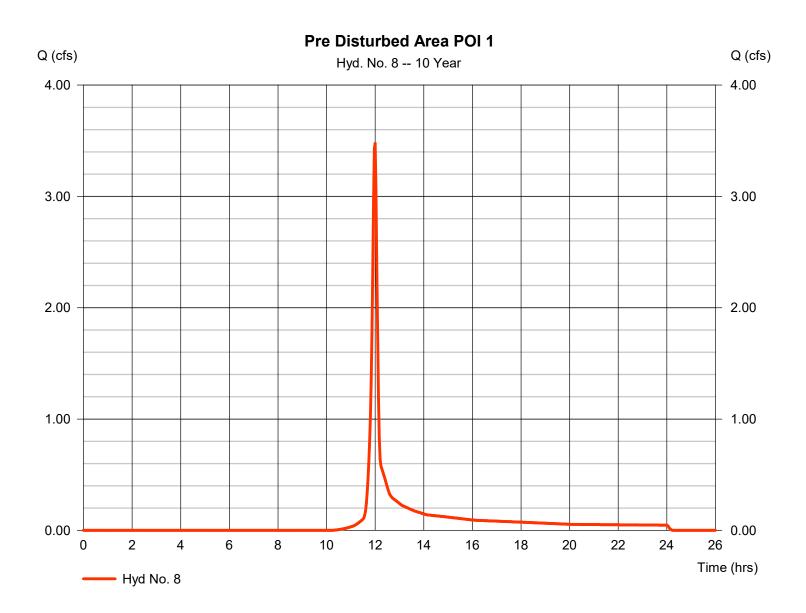
Wednesday, 02 / 21 / 2024

#### Hyd. No. 8

Pre Disturbed Area POI 1

Hydrograph type = SCS Runoff Peak discharge = 3.477 cfsStorm frequency = 10 yrsTime to peak = 12.00 hrsTime interval = 2 min Hyd. volume = 7,975 cuftDrainage area = 1.280 acCurve number = 70\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 7.60 \, \text{min}$ = TR55 Total precip. = 4.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 77) + (1.210 x 70)] / 1.280



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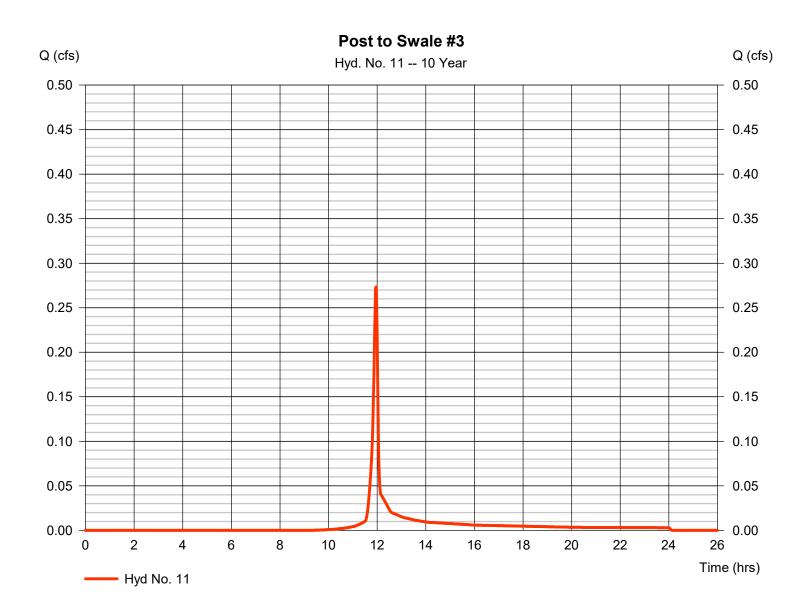
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#### Hyd. No. 11

Post to Swale #3

Hydrograph type = SCS Runoff Peak discharge = 0.273 cfsStorm frequency = 10 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 550 cuft Drainage area Curve number = 0.080 ac= 74\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 5.00 min = User Total precip. = 4.56 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 74) + (0.010 x 70)] / 0.080



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#### Hyd. No. 1

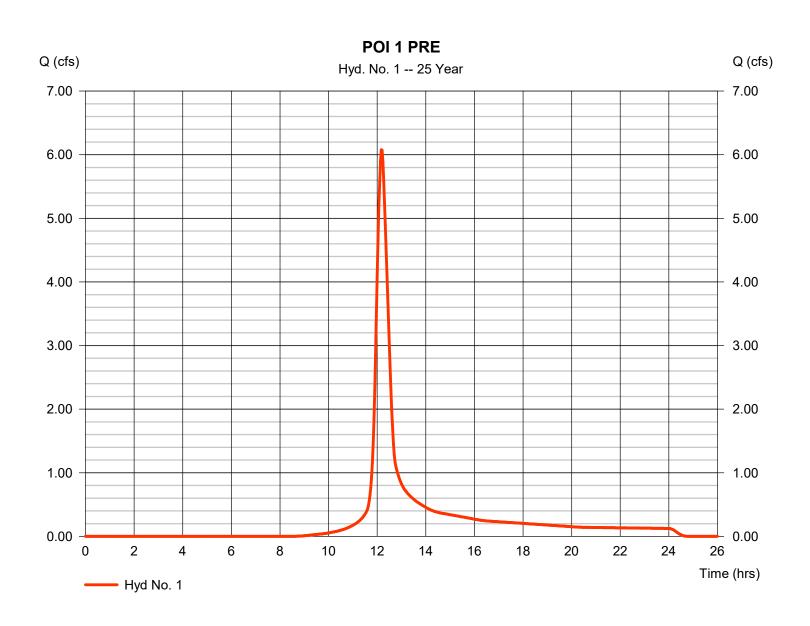
POI 1 PRE

Hydrograph type = SCS Runoff Peak discharge = 6.077 cfsStorm frequency = 25 yrs Time to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 24.449 cuft = 2.330 acCurve number Drainage area = 73\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 28.20 min = TR55

Total precip. = 5.76 in Distribution = 28.20 ml

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.150 \times 98) + (0.290 \times 77) + (1.740 \times 70) + (0.150 \times 80)] / 2.330$ 



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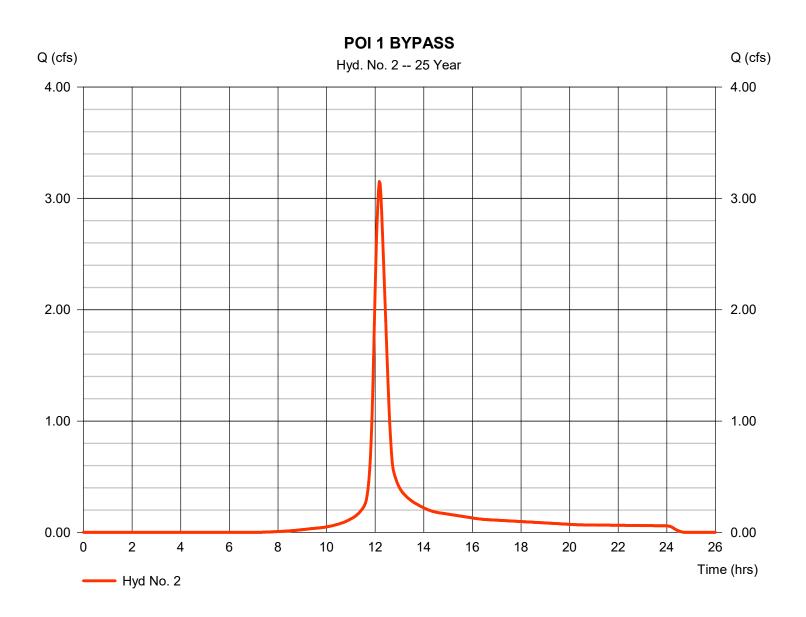
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#### Hyd. No. 2

POI 1 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 3.151 cfsStorm frequency = 25 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 12.592 cuft Curve number Drainage area = 1.030 ac= 78\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 27.70 min = TR55 Total precip. Distribution = Type II = 5.76 inStorm duration = 24 hrs = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.110 \times 77) + (0.200 \times 98) + (0.100 \times 79) + (0.300 \times 71) + (0.290 \times 70) + (0.030 \times 78)] / 1.030$ 



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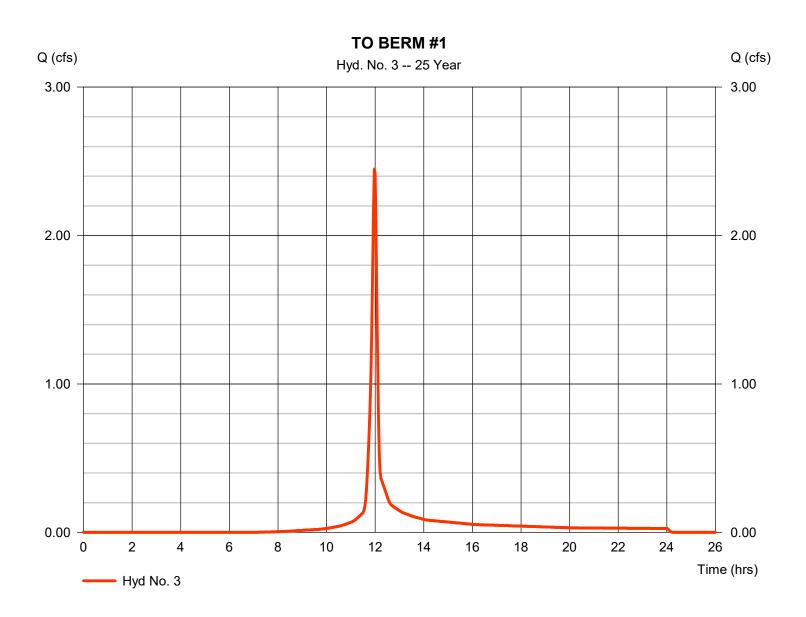
Wednesday, 02 / 21 / 2024

#### Hyd. No. 3

TO BERM #1

Hydrograph type = SCS Runoff Peak discharge = 2.448 cfsStorm frequency = 25 yrs Time to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 5,623 cuft= 78\* Drainage area = 0.460 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 9.00 min = TR55 Total precip. Distribution = Type II = 5.76 inStorm duration = 24 hrs = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.080 \times 98) + (0.180 \times 74) + (0.070 \times 71) + (0.070 \times 70) + (0.010 \times 77) + (0.050 \times 80)] / 0.460$ 



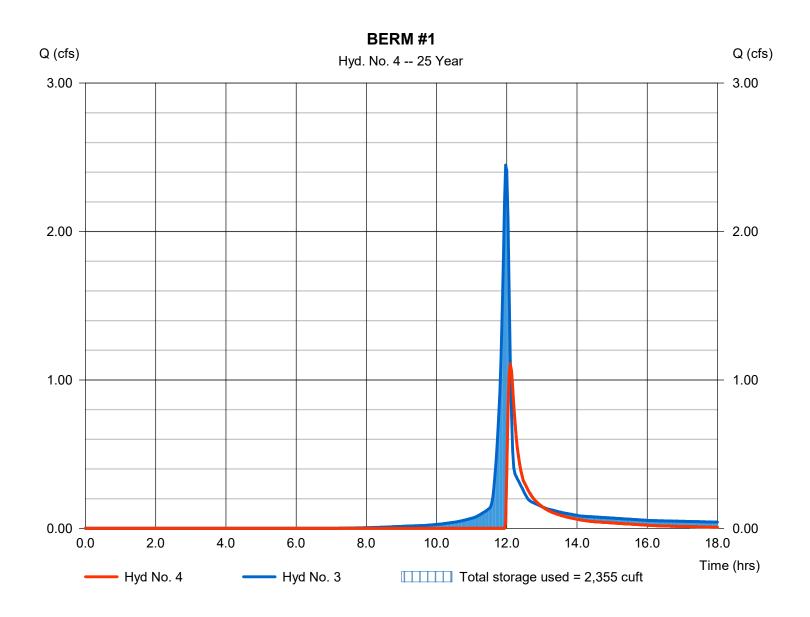
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#### Hyd. No. 4

BERM #1

Hydrograph type = Reservoir Peak discharge = 1.108 cfsStorm frequency = 25 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 2,328 cuft Inflow hyd. No. = 3 - TO BERM #1 Max. Elevation = 683.23 ft= BERM #1 Reservoir name Max. Storage = 2,355 cuft



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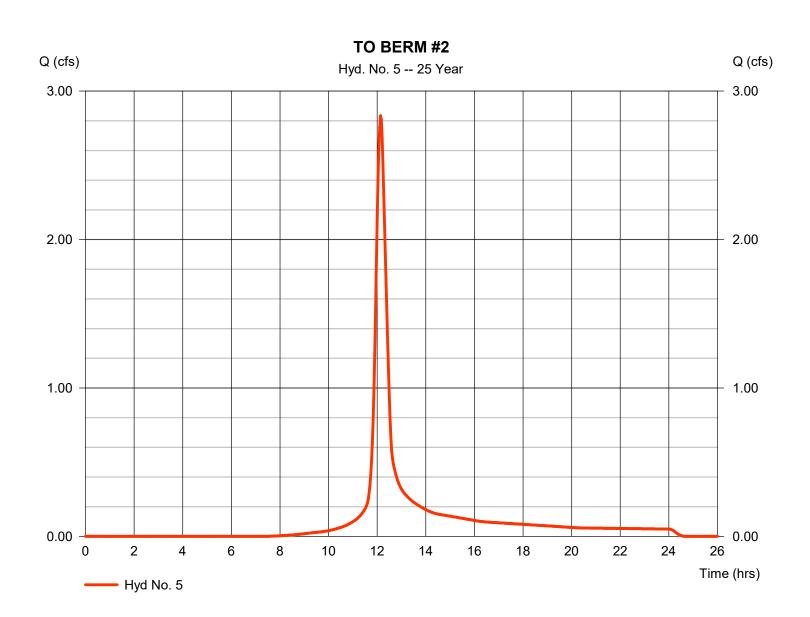
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#### Hyd. No. 5

TO BERM #2

Hydrograph type = SCS Runoff Peak discharge = 2.834 cfsStorm frequency = 25 yrs Time to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 10.401 cuftDrainage area = 0.890 acCurve number = 77\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 26.60 min = TR55 Total precip. Distribution = Type II = 5.76 inStorm duration = 24 hrs = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.130 \times 98) + (0.130 \times 71) + (0.170 \times 70) + (0.300 \times 74) + (0.100 \times 77) + (0.060 \times 80)] / 0.890$ 



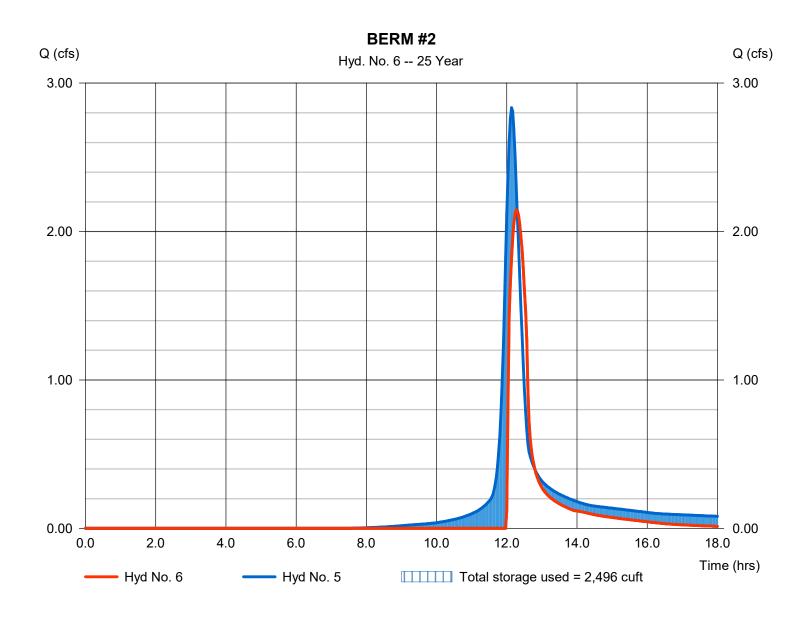
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 02 / 21 / 2024

#### Hyd. No. 6

BERM #2

Hydrograph type = Reservoir Peak discharge = 2.146 cfsStorm frequency = 25 yrsTime to peak  $= 12.27 \, hrs$ Time interval = 2 min Hyd. volume = 5,738 cuftInflow hyd. No. = 5 - TO BERM #2 Max. Elevation = 693.19 ft= BERM #2 Reservoir name Max. Storage = 2,496 cuft



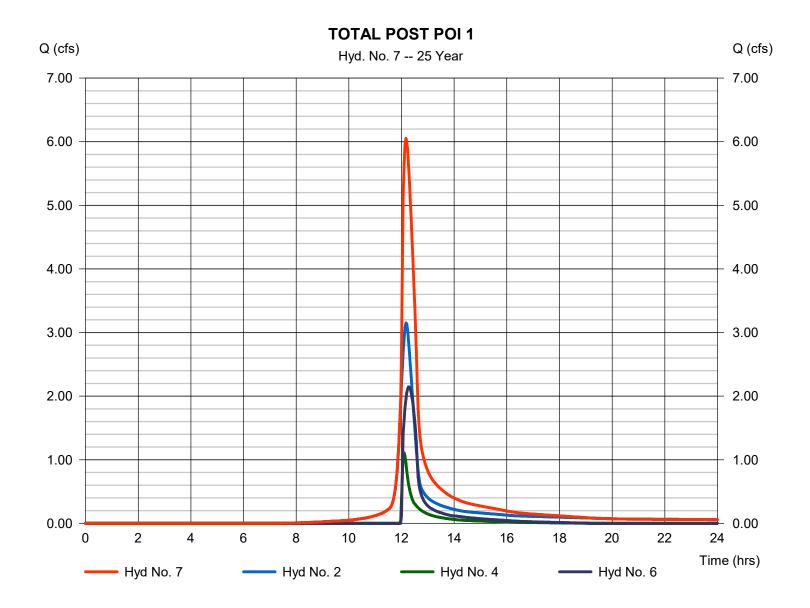
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 02 / 21 / 2024

#### Hyd. No. 7

**TOTAL POST POI 1** 

Hydrograph type = Combine Peak discharge = 6.052 cfsTime to peak Storm frequency = 25 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 20,657 cuft Inflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

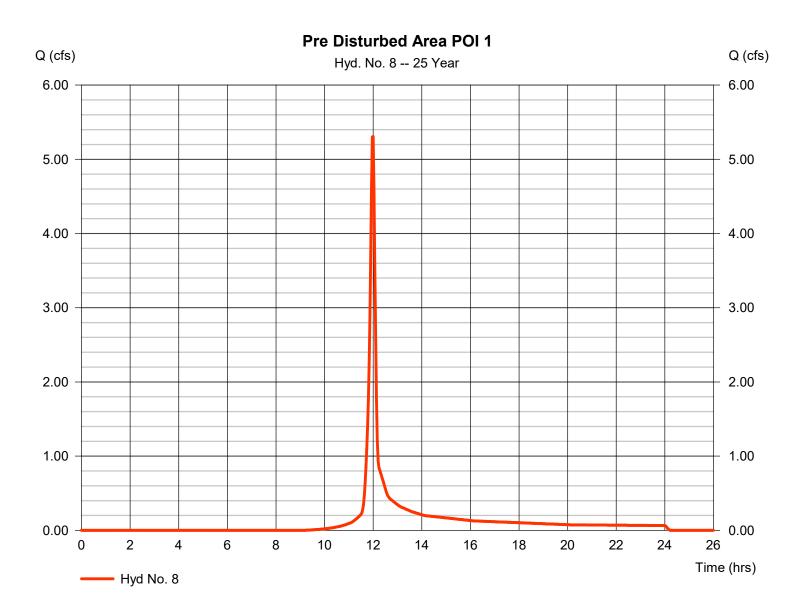
Wednesday, 02 / 21 / 2024

#### Hyd. No. 8

Pre Disturbed Area POI 1

Hydrograph type = SCS Runoff Peak discharge = 5.307 cfsStorm frequency = 25 yrs Time to peak = 12.00 hrsTime interval = 2 min Hyd. volume = 12,155 cuft Curve number Drainage area = 1.280 ac= 70\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 7.60 \, \text{min}$ = TR55 Total precip. Distribution = Type II = 5.76 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 77) + (1.210 x 70)] / 1.280



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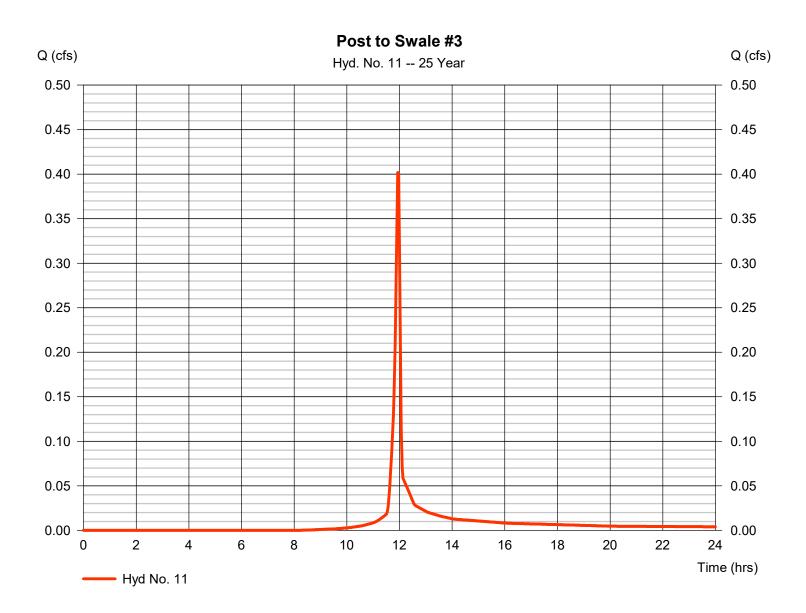
Wednesday, 02 / 21 / 2024

#### Hyd. No. 11

Post to Swale #3

Hydrograph type = SCS Runoff Peak discharge = 0.402 cfsStorm frequency = 25 yrs Time to peak  $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 812 cuft Drainage area Curve number = 0.080 ac= 74\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 5.00 min = User Total precip. = 5.76 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 74) + (0.010 x 70)] / 0.080



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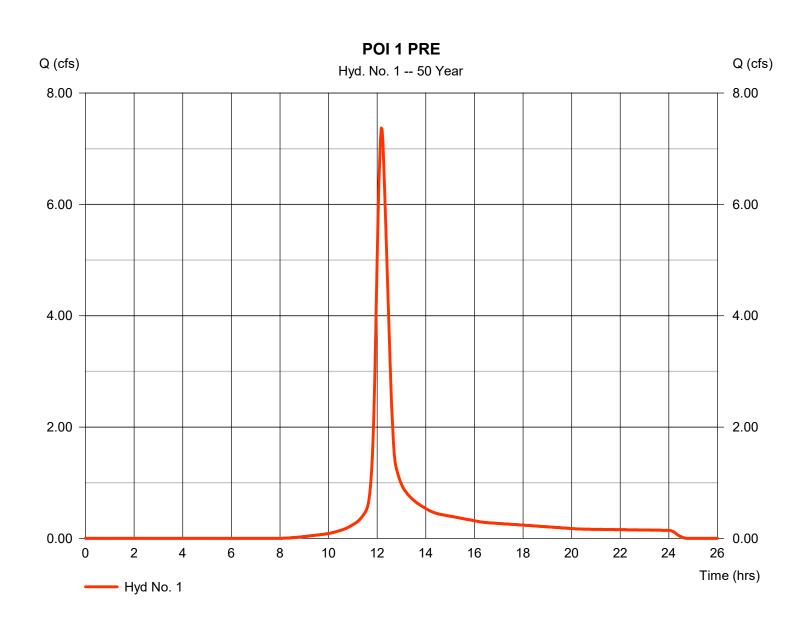
Wednesday, 02 / 21 / 2024

#### Hyd. No. 1

POI 1 PRE

Hydrograph type = SCS Runoff Peak discharge = 7.371 cfsStorm frequency = 50 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 29.526 cuft = 2.330 acCurve number Drainage area = 73\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 28.20 min = TR55 Total precip. = 6.48 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.150 \times 98) + (0.290 \times 77) + (1.740 \times 70) + (0.150 \times 80)] / 2.330$ 



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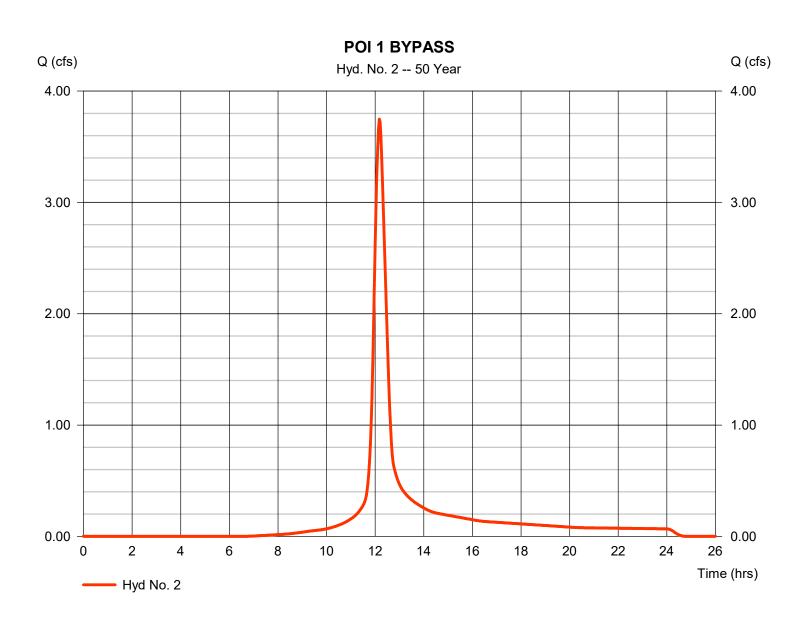
Wednesday, 02 / 21 / 2024

#### Hyd. No. 2

POI 1 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 3.747 cfsStorm frequency = 50 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 14,978 cuft Curve number Drainage area = 1.030 ac= 78\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 27.70 min = TR55 Total precip. Distribution = Type II = 6.48 inStorm duration = 24 hrs = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.110 \times 77) + (0.200 \times 98) + (0.100 \times 79) + (0.300 \times 71) + (0.290 \times 70) + (0.030 \times 78)] / 1.030$ 



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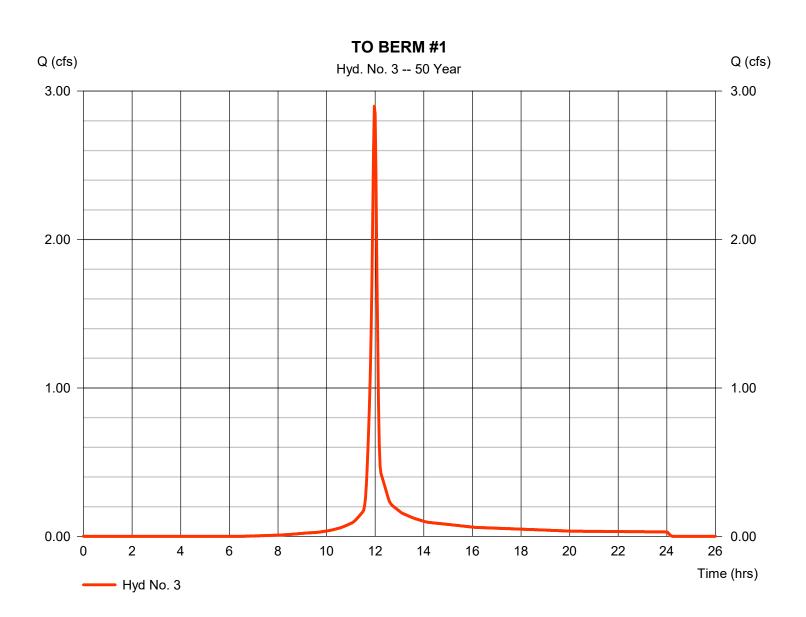
Wednesday, 02 / 21 / 2024

#### Hyd. No. 3

TO BERM #1

Hydrograph type = SCS Runoff Peak discharge = 2.899 cfsStorm frequency = 50 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 6,689 cuft= 78\* Drainage area = 0.460 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 9.00 min = TR55 Total precip. = 6.48 inDistribution = Type II Storm duration = 24 hrs = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.080 \times 98) + (0.180 \times 74) + (0.070 \times 71) + (0.070 \times 70) + (0.010 \times 77) + (0.050 \times 80)] / 0.460$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 02 / 21 / 2024

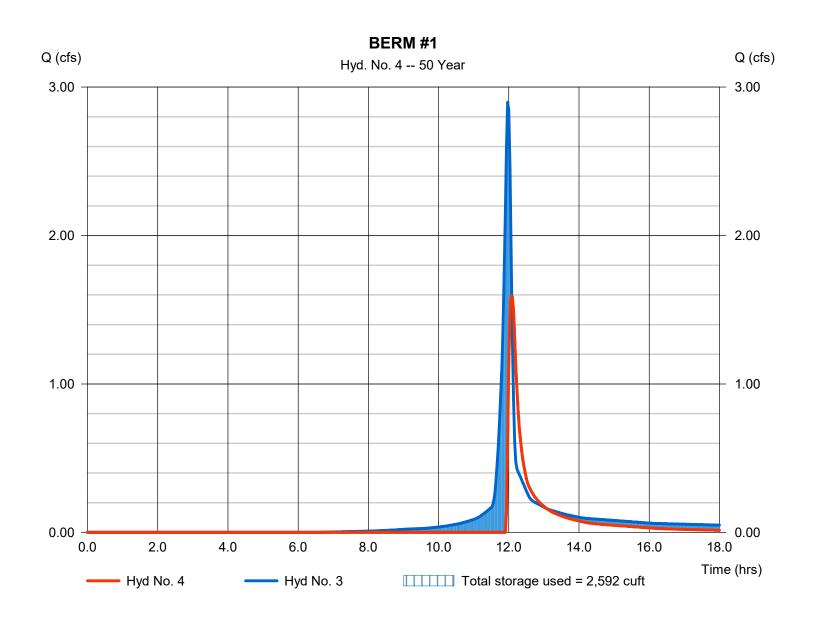
## Hyd. No. 4

BERM #1

Hydrograph type Peak discharge = 1.594 cfs= Reservoir Storm frequency = 50 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 3,284 cuft Inflow hyd. No. Max. Elevation = 3 - TO BERM #1 = 683.32 ft= BERM #1 Reservoir name Max. Storage = 2,592 cuft

Storage Indication method used. Exfiltration extracted from Outflow.

### **USED FLOW FOR RIPRAP APRON #2**



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 02 / 21 / 2024

## Hyd. No. 5

TO BERM #2

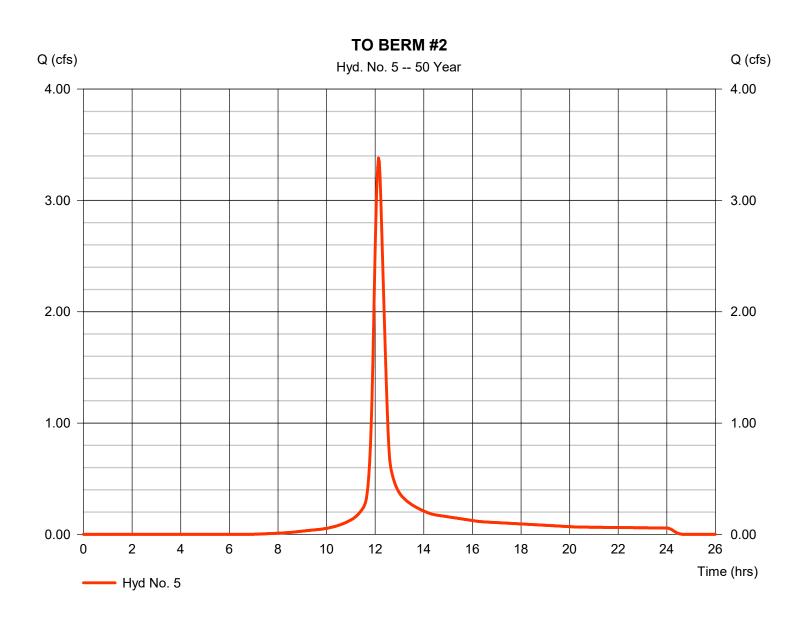
Hydrograph type = SCS Runoff Peak discharge = 3.381 cfsStorm frequency = 50 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 12.408 cuft Curve number Drainage area = 0.890 ac= 77\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 26.60 min = TR55

Tc method = TR55 Time of conc. (Tc) = 26.60 min

Total precip. = 6.48 in Distribution = Type II

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.130 \times 98) + (0.130 \times 71) + (0.170 \times 70) + (0.300 \times 74) + (0.100 \times 77) + (0.060 \times 80)] / 0.890$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 02 / 21 / 2024

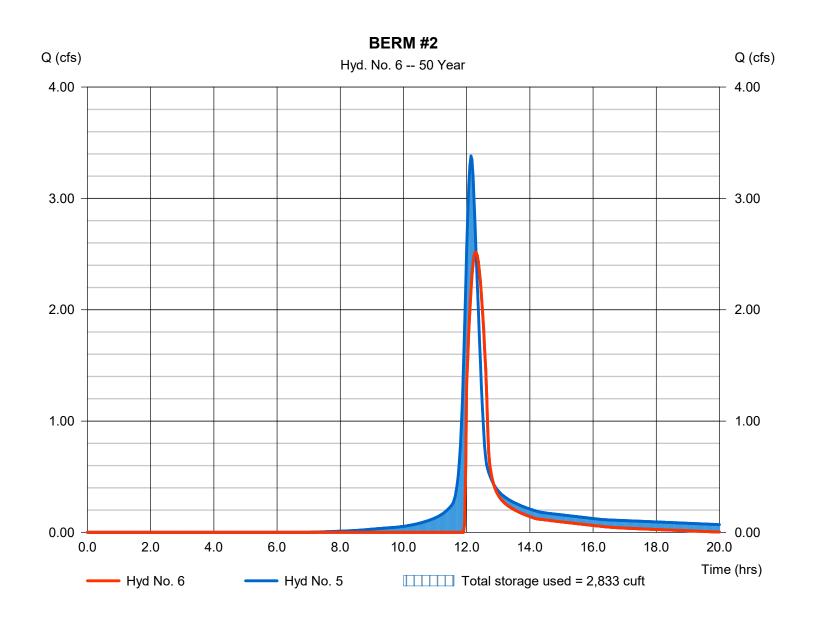
## Hyd. No. 6

BERM #2

Hydrograph type Peak discharge = 2.515 cfs= Reservoir Storm frequency = 50 yrsTime to peak  $= 12.27 \, hrs$ Time interval = 2 min Hyd. volume = 7,488 cuft Inflow hyd. No. = 5 - TO BERM #2 Max. Elevation  $= 693.31 \, \text{ft}$ = BERM #2 Reservoir name Max. Storage = 2,833 cuft

Storage Indication method used. Exfiltration extracted from Outflow.

#### **USED FLOW FOR RIPRAP APRON #3**



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

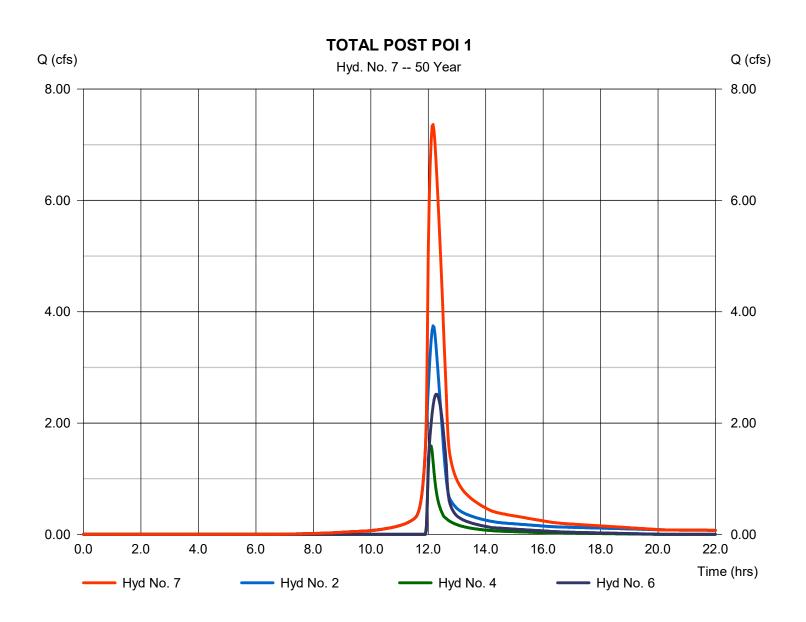
Wednesday, 02 / 21 / 2024

## Hyd. No. 7

**TOTAL POST POI 1** 

Hydrograph type = Combine Peak discharge = 7.364 cfsStorm frequency Time to peak = 50 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 25,750 cuftInflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac

#### **USED FLOW FOR RIPRAP APRON #1**



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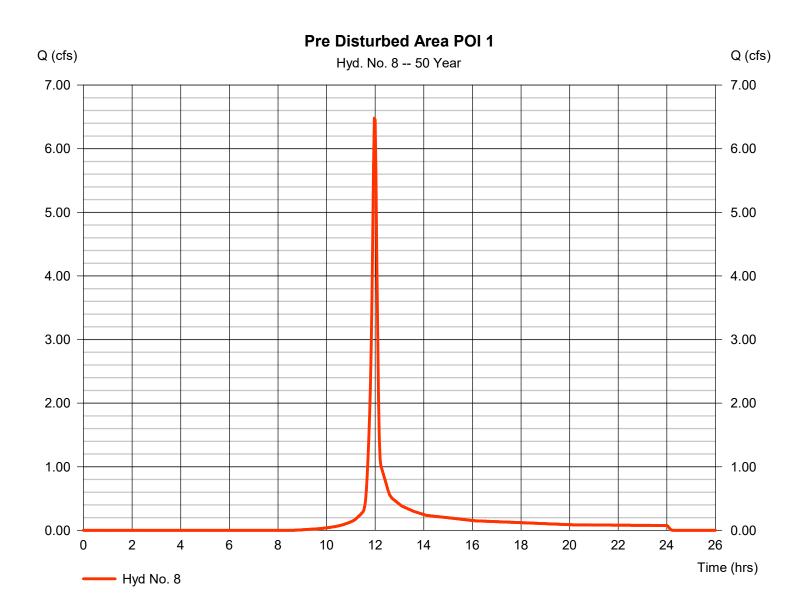
Wednesday, 02 / 21 / 2024

## Hyd. No. 8

Pre Disturbed Area POI 1

Hydrograph type = SCS Runoff Peak discharge = 6.480 cfsStorm frequency = 50 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 14.826 cuft Drainage area = 1.280 acCurve number = 70\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 7.60 \, \text{min}$ = TR55 Total precip. Distribution = Type II = 6.48 inStorm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 77) + (1.210 x 70)] / 1.280



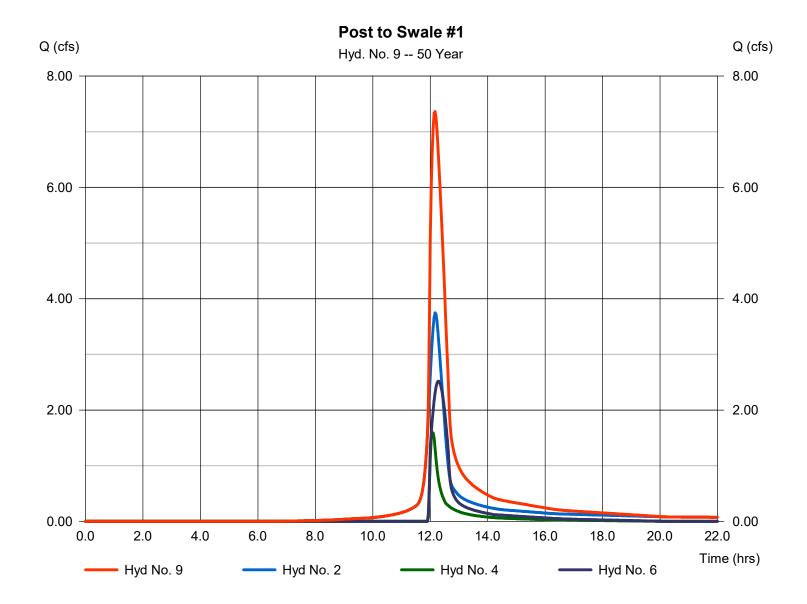
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Wednesday, 02 / 21 / 2024

## Hyd. No. 9

Post to Swale #1

Hydrograph type = Combine Peak discharge = 7.364 cfsTime to peak Storm frequency = 50 yrs $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 25,750 cuftInflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac



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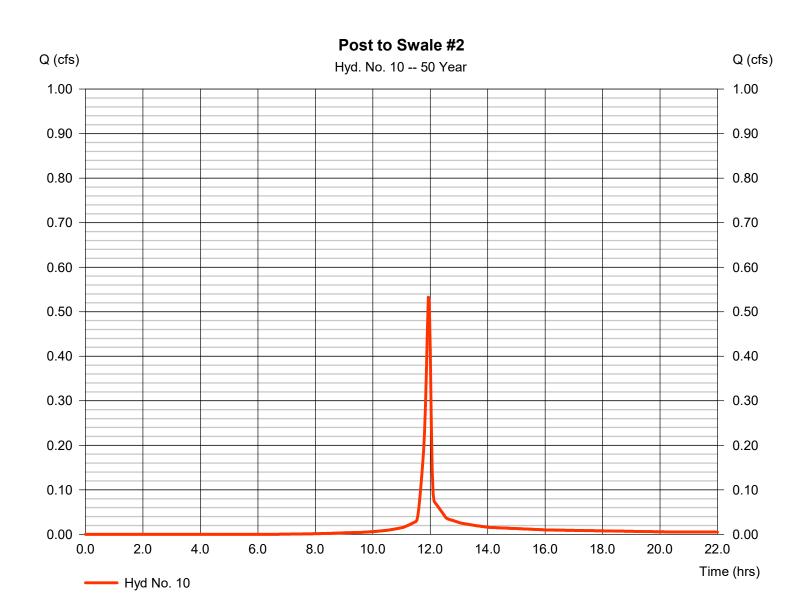
Wednesday, 02 / 21 / 2024

## Hyd. No. 10

Post to Swale #2

Hydrograph type = SCS Runoff Peak discharge = 0.533 cfsStorm frequency = 50 yrsTime to peak  $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 1.091 cuftCurve number = 78\* Drainage area = 0.080 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 5.00 min = User Total precip. Distribution = Type II = 6.48 inStorm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.050 \times 80) + (0.010 \times 74) + (0.010 \times 77) + (0.010 \times 70)] / 0.080$ 



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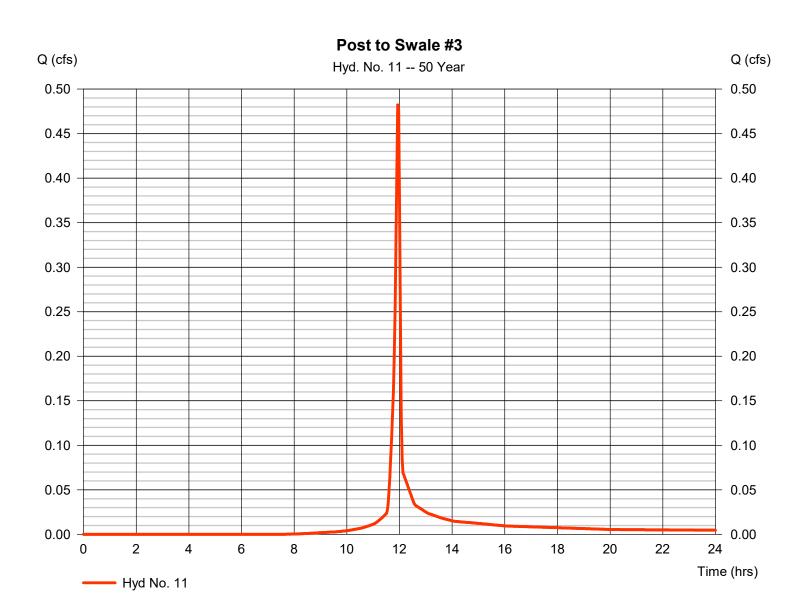
Wednesday, 02 / 21 / 2024

## Hyd. No. 11

Post to Swale #3

Hydrograph type = SCS Runoff Peak discharge = 0.482 cfsStorm frequency = 50 yrsTime to peak  $= 11.93 \, hrs$ Time interval = 2 min Hyd. volume = 978 cuft Drainage area Curve number = 74\* = 0.080 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 5.00 min = User Total precip. Distribution = Type II = 6.48 inStorm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 74) + (0.010 x 70)] / 0.080



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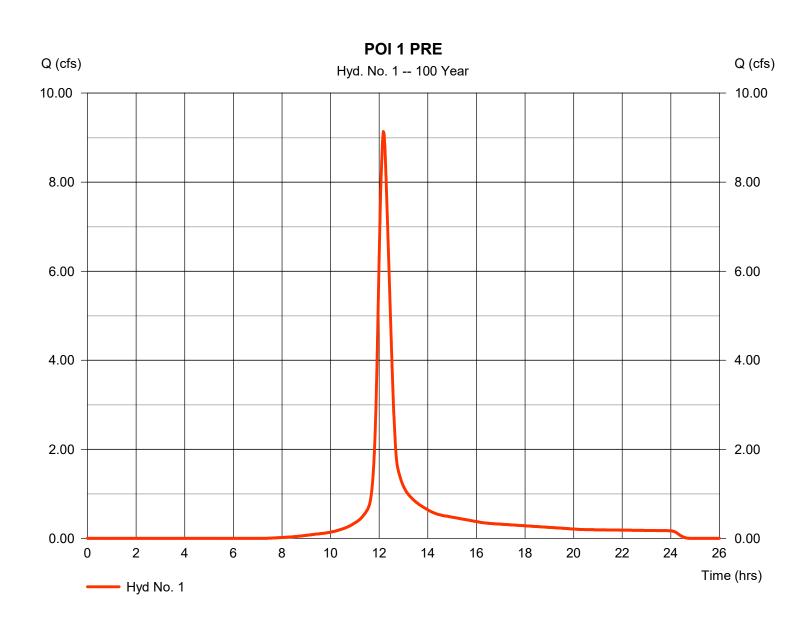
Wednesday, 02 / 21 / 2024

## Hyd. No. 1

POI 1 PRE

Hydrograph type = SCS Runoff Peak discharge = 9.137 cfsStorm frequency = 100 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 36.514 cuft = 2.330 acCurve number = 73\* Drainage area Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 28.20 min = TR55 Total precip. = 7.44 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.150 \times 98) + (0.290 \times 77) + (1.740 \times 70) + (0.150 \times 80)] / 2.330$ 



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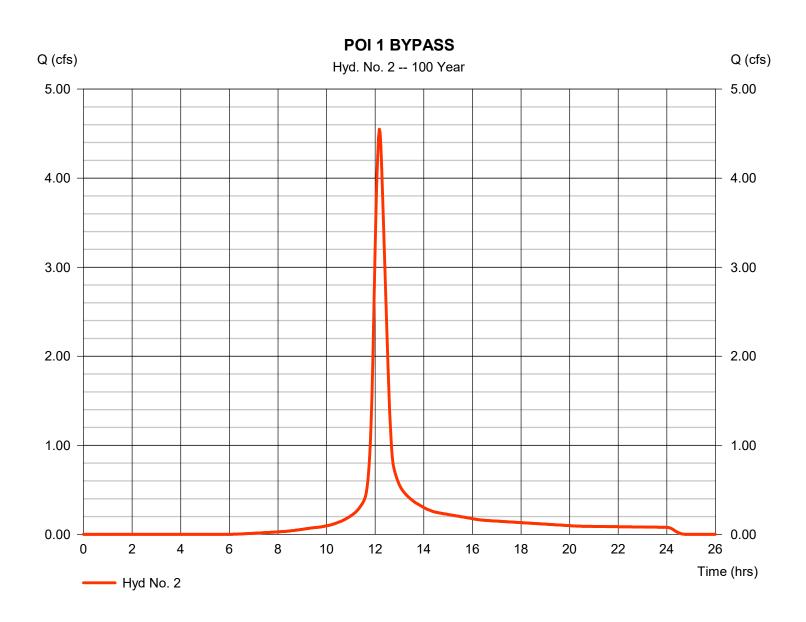
Wednesday, 02 / 21 / 2024

## Hyd. No. 2

POI 1 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 4.551 cfsStorm frequency = 100 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 2 min Hyd. volume = 18.230 cuft Drainage area = 1.030 acCurve number = 78\* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) = 27.70 min Tc method = TR55 Total precip. = 7.44 inDistribution = Type II Storm duration = 24 hrs = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.110 \times 77) + (0.200 \times 98) + (0.100 \times 79) + (0.300 \times 71) + (0.290 \times 70) + (0.030 \times 78)] / 1.030$ 



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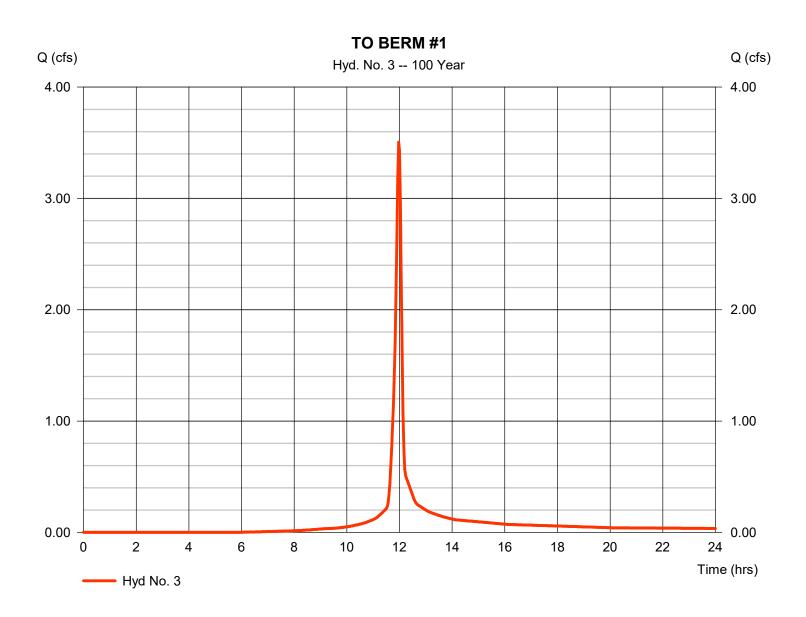
Wednesday, 02 / 21 / 2024

## Hyd. No. 3

TO BERM #1

Hydrograph type = SCS Runoff Peak discharge = 3.505 cfsStorm frequency = 100 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 8,142 cuft Curve number Drainage area = 0.460 ac= 78\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 9.00 min = TR55 Total precip. = 7.44 inDistribution = Type II Storm duration = 24 hrs = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.080 \times 98) + (0.180 \times 74) + (0.070 \times 71) + (0.070 \times 70) + (0.010 \times 77) + (0.050 \times 80)] / 0.460$ 



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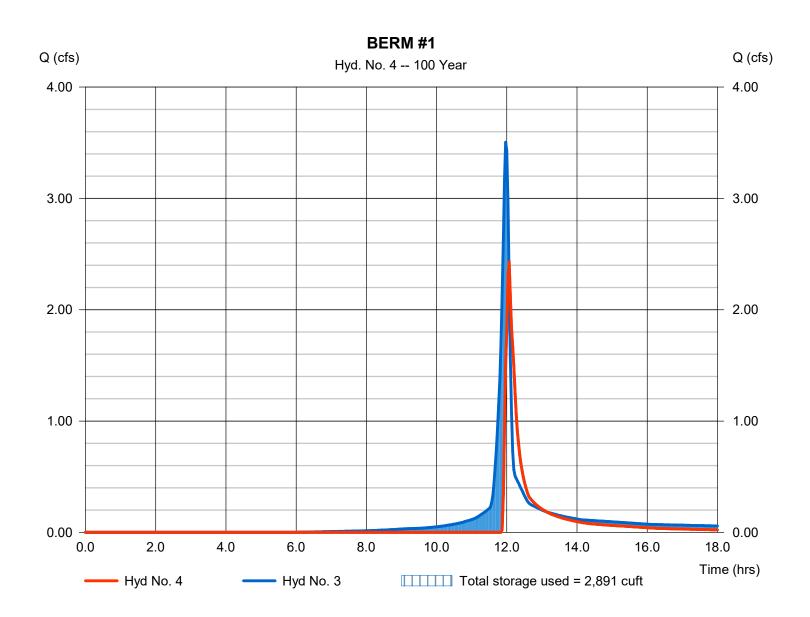
Wednesday, 02 / 21 / 2024

## Hyd. No. 4

BERM #1

Hydrograph type Peak discharge = 2.431 cfs= Reservoir Storm frequency = 100 yrsTime to peak  $= 12.07 \, hrs$ Time interval = 2 min Hyd. volume = 4,629 cuftInflow hyd. No. = 3 - TO BERM #1 Max. Elevation = 683.43 ft= BERM #1 Reservoir name Max. Storage = 2,891 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## Hyd. No. 5

TO BERM #2

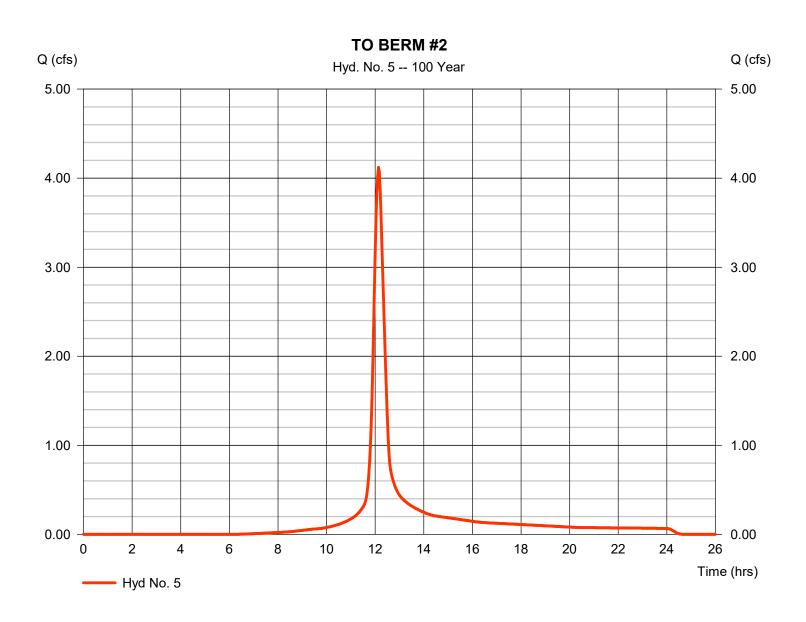
Hydrograph type = SCS Runoff Peak discharge = 4.120 cfsStorm frequency = 100 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 15,148 cuft Drainage area = 0.890 acCurve number = 77\* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) = 26.60 min Tc method = TR55

Tc method = TR55 Time of conc. (Tc) = 26.60 min

Total precip. = 7.44 in Distribution = Type II

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.130 \times 98) + (0.130 \times 71) + (0.170 \times 70) + (0.300 \times 74) + (0.100 \times 77) + (0.060 \times 80)] / 0.890$ 



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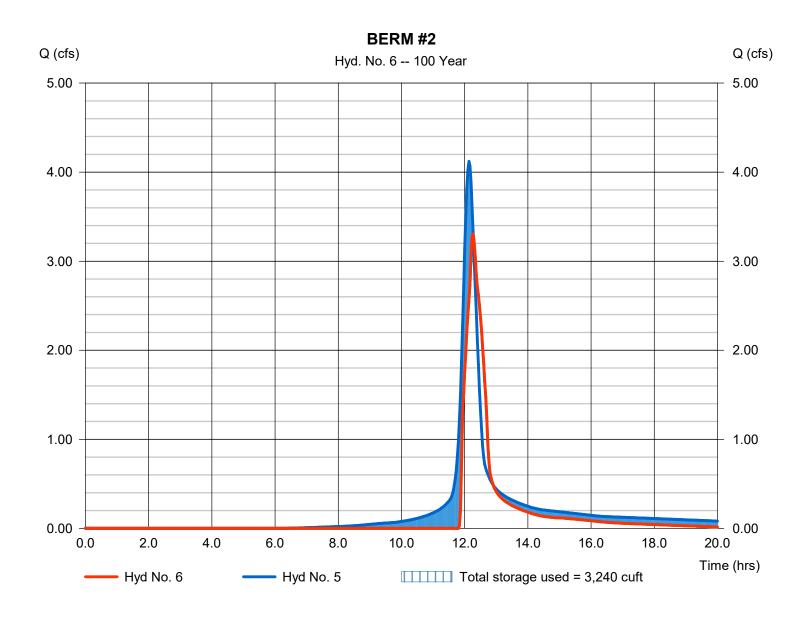
Wednesday, 02 / 21 / 2024

## Hyd. No. 6

BERM #2

Hydrograph type Peak discharge = 3.307 cfs= Reservoir Storm frequency = 100 yrsTime to peak  $= 12.27 \, hrs$ Time interval = 2 min Hyd. volume = 9,943 cuftInflow hyd. No. = 5 - TO BERM #2 Max. Elevation  $= 693.45 \, \text{ft}$ = BERM #2 Reservoir name Max. Storage = 3,240 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



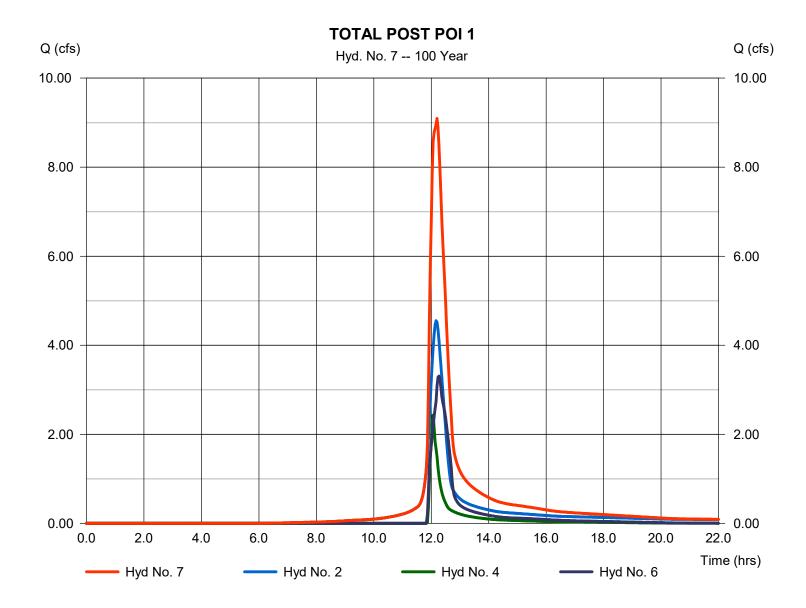
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Wednesday, 02 / 21 / 2024

## Hyd. No. 7

**TOTAL POST POI 1** 

Hydrograph type = Combine Peak discharge = 9.091 cfsTime to peak Storm frequency = 100 yrs $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 32,803 cuft Inflow hyds. = 2, 4, 6Contrib. drain. area = 1.030 ac



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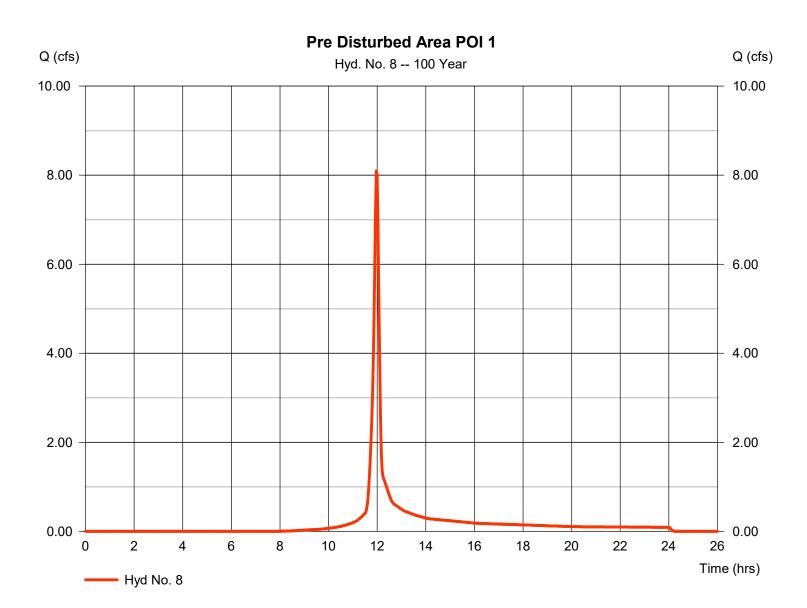
Wednesday, 02 / 21 / 2024

## Hyd. No. 8

Pre Disturbed Area POI 1

Hydrograph type = SCS Runoff Peak discharge = 8.093 cfsStorm frequency = 100 yrsTime to peak  $= 11.97 \, hrs$ Time interval = 2 min Hyd. volume = 18.526 cuft Drainage area = 1.280 acCurve number = 70\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 7.60 \, \text{min}$ = TR55 Total precip. = 7.44 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.070 x 77) + (1.210 x 70)] / 1.280



## **Pond Report**

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 02 / 21 / 2024

#### Pond No. 1 - BERM #1

#### **Pond Data**

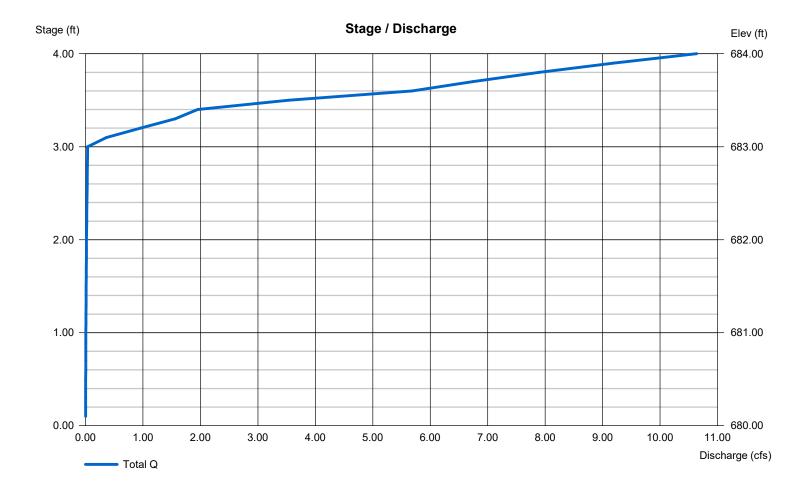
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 680.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft) 680.00 681.00 682.00 683.00 684.00	Contour area (sqft)	Contour area (sqft) Incr. Storage (cuft) Total			
0.00	680.00	00	0	0		
1.00	681.00	242	121	121		
2.00	682.00	719	481	602		
3.00	683.00	1,550	1,135	1,736		
4.00	684.00	3,770	2,660	4,396		

#### **Culvert / Orifice Structures Weir Structures** [A] [B] [C] [PrfRsr] [A] [B] [C] [D] = 12.003.00 0.00 = 12.00 5.00 0.00 0.00 Rise (in) 0.00 Crest Len (ft) = 12.00 36.00 0.00 0.00 Crest El. (ft) = 683.40 683.50 0.00 0.00 Span (in) 2.60 No. Barrels = 1 1 0 Weir Coeff. = 3.333.33 3.33 Invert El. (ft) = 681.00 683.00 0.00 0.00 Weir Type = 1 Broad = 15.00 0.00 0.00 0.00 Multi-Stage Length (ft) = Yes No No No 0.00 = 1.00 0.00 Slope (%) n/a N-Value = .013 .013 .013 n/a 0.60 0.60 0.60 Orifice Coeff. = 0.60Exfil.(in/hr) = 1.000 (by Contour) TW Elev. (ft) Multi-Stage = n/aYes No No = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



## **Pond Report**

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 02 / 21 / 2024

#### Pond No. 2 - BERM #2

#### **Pond Data**

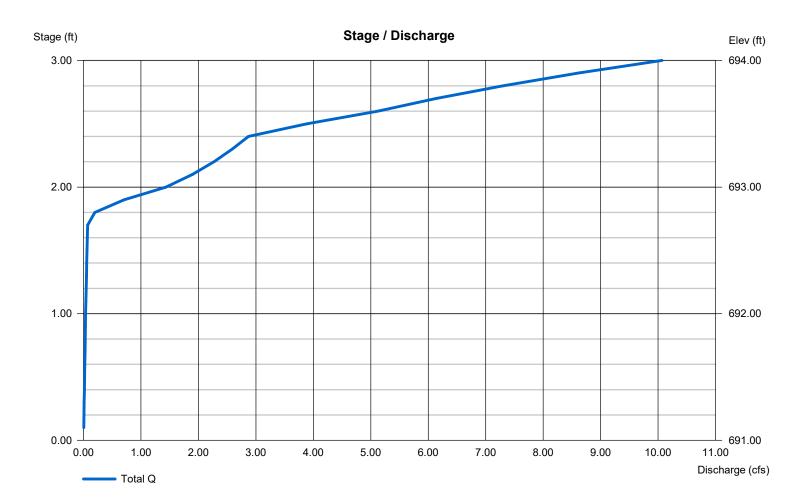
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 691.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	691.00	00	0	0
1.00	692.00	893	447	447
2.00	693.00	2,111	1,502	1,949
3.00	694.00	3,580	2,846	4,794

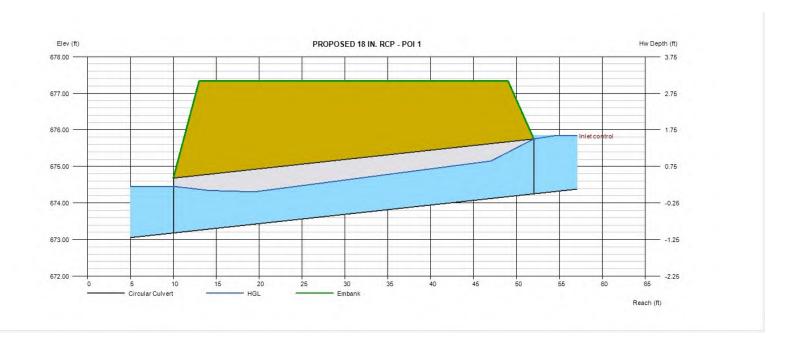
#### **Culvert / Orifice Structures Weir Structures** [B] [PrfRsr] [A] [C] [D] [A] [B] [C] = 12.00 Rise (in) 3.00 0.00 0.00 Crest Len (ft) = 12.00 5.00 0.00 0.00 = 12.0038.00 0.00 0.00 Crest El. (ft) = 693.40 693.50 0.00 0.00 Span (in) No. Barrels = 1 0 Weir Coeff. = 3.332.60 3.33 3.33 1 = 691.50 692.75 0.00 0.00 Broad Invert El. (ft) Weir Type = 1 = 25.000.00 0.00 0.00 Multi-Stage Length (ft) = Yes No No No Slope (%) = 1.00 0.00 0.00 n/a N-Value = .013 .013 .013 n/a 0.60 0.60 = 1.750 (by Contour) = 0.600.60 Exfil.(in/hr) Orifice Coeff. Multi-Stage = n/aNo TW Elev. (ft) = 0.00Yes No

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



## PROPOSED 18 IN. RCP - POI 1

Invert Elev Dn (ft)	= 673.18	Calculations	
Pipe Length (ft)	= 42.00	Qmin (cfs)	= 7.36
Slope (%)	= 2.55	Qmax (cfs)	= 7.36
Invert Elev Up (ft)	= 674.25	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 18.0		
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 7.36
No. Barrels	= 1	Qpipe (cfs)	= 7.36
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	<ul><li>Circular Concrete</li></ul>	Veloc Dn (ft/s)	= 4.60
Culvert Entrance	<ul><li>= Groove end projecting (C)</li></ul>	Veloc Up (ft/s)	= 5.57
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 674.45
		HGL Up (ft)	= 675.30
Embankment		Hw Elev (ft)	= 675.84
Top Elevation (ft)	= 677.33	Hw/D (ft)	= 1.06
Top Width (ft)	= 36.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		



## **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Feb 20 2024

#### Swale #1

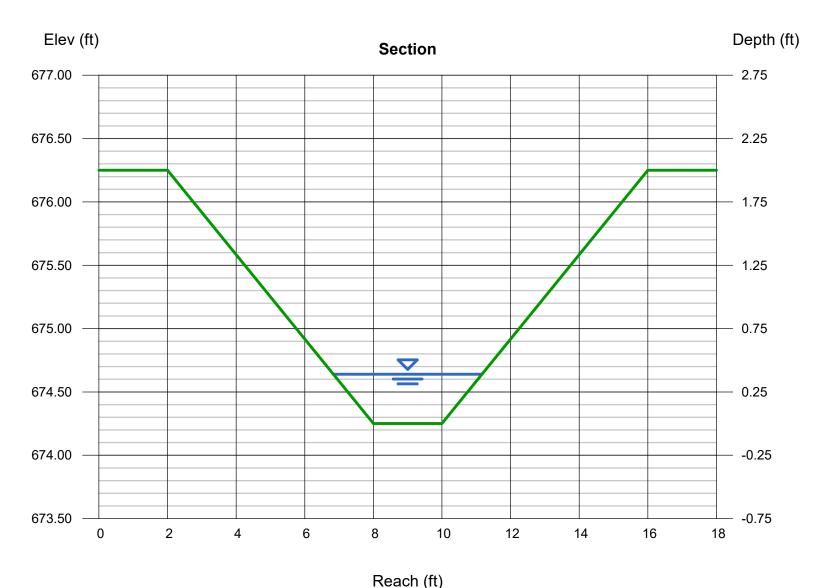
Bottom Width (ft) = 2.00 Side Slopes (z:1) = 3.00, 3.00 Total Depth (ft) = 2.00 Invert Elev (ft) = 674.25 Slope (%) = 6.60 N-Value = 0.026

#### Calculations

Compute by: Known Q Known Q (cfs) = 7.36

#### Highlighted

= 0.39Depth (ft) Q (cfs) = 7.360Area (sqft) = 1.24Velocity (ft/s) = 5.95Wetted Perim (ft) = 4.47Crit Depth, Yc (ft) = 0.57Top Width (ft) = 4.34EGL (ft) = 0.94



## **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Feb 20 2024

#### Swale #2

T	ra	p	ez	0	į	d	a	l

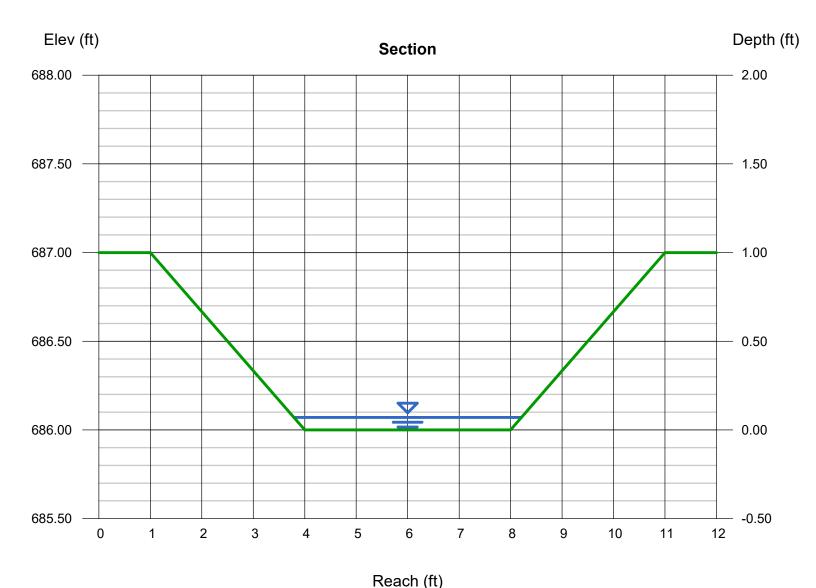
Bottom Width (ft) = 4.00 Side Slopes (z:1) = 3.00, 3.00 Total Depth (ft) = 1.00 Invert Elev (ft) = 686.00 Slope (%) = 5.71 N-Value = 0.026

#### Calculations

Compute by: Known Q Known Q (cfs) = 0.53

### Highlighted

Depth (ft) = 0.07Q (cfs) = 0.533Area (sqft) = 0.29Velocity (ft/s) = 1.81 Wetted Perim (ft) = 4.44Crit Depth, Yc (ft) = 0.09Top Width (ft) = 4.42EGL (ft) = 0.12



# **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Feb 20 2024

#### Swale #3

Trapezoidal	
Bottom Width (ft)	= 3.00
Side Slopes (z:1)	= 8.00, 8.00
Total Depth (ft)	= 1.00
Invert Elev (ft)	= 694.00

Invert Elev (ft) = 694.00 Slope (%) = 7.10 N-Value = 0.026

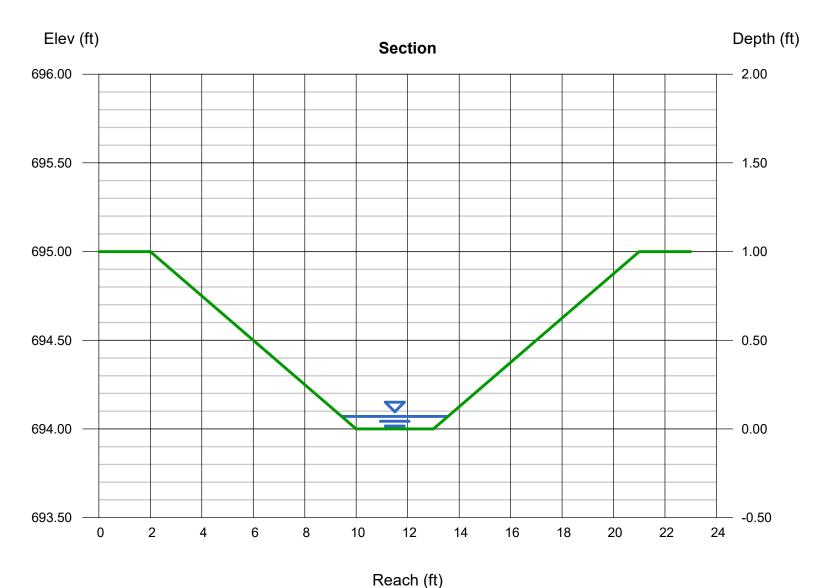
**Calculations** 

Compute by: Known Q Known Q (cfs) = 0.48

inginigittou	
Depth (ft)	= 0.07
Q (cfs)	= 0.482

Highlighted

Q (cfs) = 0.482 Area (sqft) = 0.25 Velocity (ft/s) = 1.93 Wetted Perim (ft) = 4.13 Crit Depth, Yc (ft) = 0.09 Top Width (ft) = 4.12 EGL (ft) = 0.13



#### CHANNEL ANALYSIS

Home > View Projects > Project > Swale #1

Name Swale #1

Discharge 7,364

Channel Slope 0.066

Channel Bottom Width 2

Left Side Slope 3

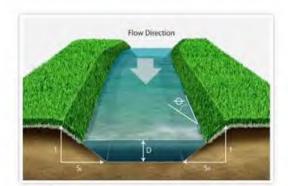
Right Side Slope 3

Low Flow Liner

Retardence Class C 6-12 in

Vegetation Type Mix (Sod and Bunch)
Vegetation Density Good 65-79%

Soil Type Silt Loam (SM)



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View Computations

Duplicate Analysis Delete Analysis

#### S150BN

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	DATE SELECT	Staple Pattern
S150BN Unvegetated	Straight	7.36 cfs	5.27 <sup>ft</sup> / <sub>s</sub>	0.43 ft	0.032	1.9 lbs/ft2	1.75 lbs/ <sub>ft2</sub>	1.08	STABLE	D
Underlying Substrate	Straight	7.36 cfs	5.27 <sup>ft</sup> / <sub>s</sub>	0.43 ft	0.032	1.39 lbs/ft2	1.22 lbs/ft2	1.14	STABLE	D

## Unreinforced Vegetation

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
Unreinforced Vegetation	Straight	7.36 cfs	4,39 <sup>ft</sup> / <sub>s</sub>	0.48 ft	0.041	4 lbs/ft2	1.99 lbs/ft2	2.01	STABLE	44
Underlying Substrate	Straight	7.36 cfs	4.39 <sup>ft</sup> / <sub>s</sub>	0.48 ft	0.041	1.88 lbs/ft2	1.36 lbs/ft2	1.39	STABLE	+

### CHANNEL ANALYSIS

Home > View Projects > Project > Swale #2

Swale #2
0.53
0.0571
4
3
3

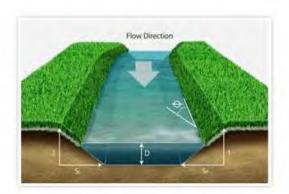
Low Flow Liner

Retardence Class C 6-12 in

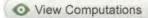
Vegetation Type Mix (Sod and Bunch)

Vegetation Density Good 65-79%

Soil Type Silt Loam (SM)



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## Unreinforced Vegetation

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
Unreinforced Vegetation	Straight	0.53 cfs	1.1 <sup>ft</sup> / <sub>s</sub>	0.11 ft	0.07	4 lbs/ft2	0.39 lbs/ft2	10.14	STABLE	
Underlying Substrate	Straight	0.53 cfs	1.1 <sup>ft</sup> / <sub>s</sub>	0.11 ft	0.07	4 lbs/ <sub>ft2</sub>	0.36 lbs/ft2	11	STABLE	-42

#### S75BN

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
S75BN Unvegetated	Straight	0.53 cfs	1.68 <sup>ft</sup> / <sub>s</sub>	0.07 ft	0.036	1.6 lbs/ft2	0.27 lbs/ft2	6.02	STABLE	D
Underlying Substrate	Straight	0.53 cfs	1.68 <sup>ft</sup> / <sub>s</sub>	0.07 ft	0.036	1.17 lbs/ft2	0.25 lbs/ft2	4.67	STABLE	D

#### CHANNEL ANALYSIS

Home > View Projects > Project > Swale #3

Name Swale #3

Discharge 0.48

Channel Slope 0.071

Channel Bottom Width 3

Left Side Slope 8

Right Side Slope 8

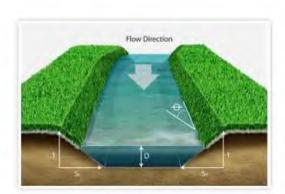
Low Flow Liner

Retardence Class C 6-12 in

Vegetation Type Mix (Sod and Bunch)

Vegetation Density Good 65-79%

Soil Type Silt Loam (SM)



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View Computations

Duplicate Analysis Delete Analysis

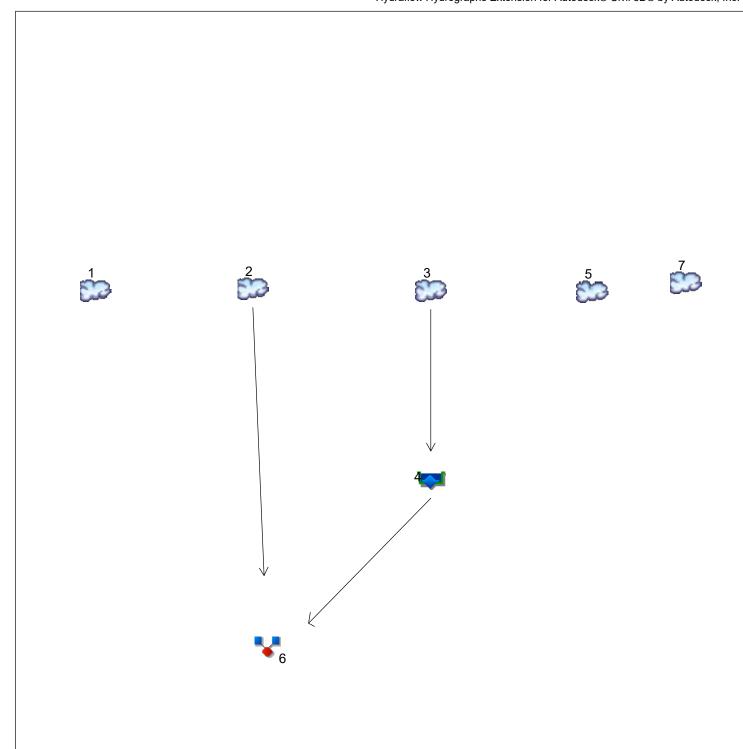
### Unreinforced Vegetation

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Remarks	Staple Pattern
Unreinforced Vegetation	Straight	0.48 cfs	1.15 <sup>ft</sup> / <sub>s</sub>	0.11 ft	0.068	4 lbs/ft2	0.48 lbs/ft2	8.35	STABLE	4-
Underlying Substrate	Straight	0.48 cfs	1.15 <sup>ft</sup> / <sub>s</sub>	0.11 ft	0.068	4 lbs/ft2	0.39 lbs/ft2	10.25	STABLE	+

#### S75BN

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	D non a rive	Staple Pattern
S75BN Unvegetated	Straight	0.48 cfs	1.79 <sup>ft</sup> / <sub>s</sub>	0.07 ft	0.035	1.6 lbs/ft2	0.33 lbs/ <sub>ft2</sub>	4.84	STABLE	D
Underlying Substrate	Straight	0.48 cfs	1.79 <sup>ft</sup> / <sub>s</sub>	0.07 ft	0.035	1.17 lbs/ <sub>ft2</sub>	0.28 lbs/ft2	4.14	STABLE	D

# **Watershed Model Schematic**



#### <u>Legend</u>

<u>Hyd.</u>	<u>Origin</u>	<u>Description</u>
1	SCS Runoff	POI 2 PRE
2	SCS Runoff	POI 2 BYPASS
3	SCS Runoff	TO BERM #3
4	Reservoir	BERM #3
5	SCS Runoff	POI 2 PRE - CHANGED AREA
6	Combine	TOTAL POST POI 2
7	SCS Runoff	Post to Swale #4

Project: 21-4-16 stormwater.gpw POI2.gpw

Thursday, 02 / 22 / 2024

# Hydrograph Return Period Recap

	Hydrograph	Inflow				Peak Out	tflow (cfs)	)			Hydrograph
0.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff		5.768	9.134		14.76	22.98	34.08	40.96	50.30	POI 2 PRE
2	SCS Runoff		3.881	6.145		9.927	15.46	22.93	27.56	33.84	POI 2 BYPASS
3	SCS Runoff		2.036	3.156		5.011	7.718	11.34	13.58	16.60	TO BERM #3
4	Reservoir	3	0.000	0.000		1.859	5.592	9.083	10.60	12.00	BERM #3
5	SCS Runoff		0.396	0.702		1.233	2.031	3.126	3.822	4.776	POI 2 PRE - CHANGED AREA
6	Combine	2, 4,	3.881	6.145		9.927	18.91	31.23	37.26	45.11	TOTAL POST POI 2
7	SCS Runoff		0.410	0.664		1.093	1.722	2.579	3.113	3.838	Post to Swale #4

Proj. file: 21-4-16 stormwater.gpw POI2.gpw

Thursday, 02 / 22 / 2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	5.768	2	728	22,698				POI 2 PRE	
2	SCS Runoff	3.881	2	728	15,271				POI 2 BYPASS	
3	SCS Runoff	2.036	2	728	7,834				TO BERM #3	
4	Reservoir	0.000	2	994	0	3	687.81	3,392	BERM #3	
5	SCS Runoff	0.396	2	728	1,781				POI 2 PRE - CHANGED AREA	
6	Combine	3.881	2	728	15,271	2, 4,			TOTAL POST POI 2	
7	SCS Runoff	0.410	2	728	1,655				Post to Swale #4	
21-	21-4-16 stormwater.gpw POI2.gpw					Period: 1 Ye	ear	Thursday, 02 / 22 / 2024		

No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	9.134	2	728	33,808				POI 2 PRE
2	SCS Runoff	6.145	2	728	22,745				POI 2 BYPASS
3	SCS Runoff	3.156	2	728	11,540				TO BERM #3
4	Reservoir	0.000	2	800	0	3	688.30	5,497	BERM #3
5	SCS Runoff	0.702	2	728	2,788				POI 2 PRE - CHANGED AREA
6	Combine	6.145	2	728	22,745	2, 4,			TOTAL POST POI 2
7	SCS Runoff	0.664	2	728	2,493				Post to Swale #4
	1-4-16 stormwater.gpw POI2.gpw Return Period: 2 Year						Thursday	02 / 22 / 2024	

						1	T	is Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2			
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description		
1	SCS Runoff	14.76	2	728	52,558				POI 2 PRE		
2	SCS Runoff	9.927	2	728	35,360				POI 2 BYPASS		
3	SCS Runoff	5.011	2	728	17,750				TO BERM #3		
4	Reservoir	1.859	2	744	3,677	3	688.58	6,906	BERM #3		
5	SCS Runoff	1.233	2	728	4,542				POI 2 PRE - CHANGED AREA		
6	Combine	9.927	2	728	39,037	2, 4,			TOTAL POST POI 2		
7	SCS Runoff	1.093	2	728	3,919				Post to Swale #4		
21-	21-4-16 stormwater.gpw POI2.gpw Return Period: 5 Year						ear	Thursday, 0	02 / 22 / 2024		

				1		1		Extension for Autodesk® Civil 3D® by Autodesk, Inc. V			
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description		
1	SCS Runoff	22.98	2	726	80,289				POI 2 PRE		
2	SCS Runoff	15.46	2	726	54,017				POI 2 BYPASS		
3	SCS Runoff	7.718	2	726	26,875				TO BERM #3		
4	Reservoir	5.592	2	736	10,699	3	688.78	7,924	BERM #3		
5	SCS Runoff	2.031	2	728	7,209				POI 2 PRE - CHANGED AREA		
6	Combine	18.91	2	732	64,716	2, 4,			TOTAL POST POI 2		
7	SCS Runoff	1.722	2	728	6,041				Post to Swale #4		
21-	21-4-16 stormwater.gpw POI2.gpw Return Period: 10 Year						Thursday, (	)2 / 22 / 2024			

			1			,	7 0 1	IS Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2			
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description		
1	SCS Runoff	34.08	2	726	117,842				POI 2 PRE		
2	SCS Runoff	22.93	2	726	79,282				POI 2 BYPASS		
3	SCS Runoff	11.34	2	726	39,169				TO BERM #3		
4	Reservoir	9.083	2	734	20,953	3	689.03	9,263	BERM #3		
5	SCS Runoff	3.126	2	726	10,900				POI 2 PRE - CHANGED AREA		
6	Combine	31.23	2	728	100,235	2, 4,			TOTAL POST POI 2		
7	SCS Runoff	2.579	2	726	8,931				Post to Swale #4		
21-	21-4-16 stormwater.gpw POI2.gpw Return Period: 2						l ⁄ear	Thursday, (	)2 / 22 / 2024		

	1		1	1	1			S Extension for Autodesk® Civil 3D® by Autodesk, Inc.			
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description		
1	SCS Runoff	40.96	2	726	141,430				POI 2 PRE		
2	SCS Runoff	27.56	2	726	95,151				POI 2 BYPASS		
3	SCS Runoff	13.58	2	726	46,867				TO BERM #3		
4	Reservoir	10.60	2	734	27,663	3	689.18	10,414	BERM #3		
5	SCS Runoff	3.822	2	726	13,250				POI 2 PRE - CHANGED AREA		
6	Combine	37.26	2	728	122,814	2, 4,			TOTAL POST POI 2		
7	SCS Runoff	3.113	2	726	10,752				Post to Swale #4		
21-	21-4-16 stormwater.gpw POI2.gpw Return Period: 50						ear	Thursday, (	02 / 22 / 2024		

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	50.30	2	726	173,760				POI 2 PRE
2	SCS Runoff	33.84	2	726	116,902				POI 2 BYPASS
3	SCS Runoff	16.60	2	726	57,398				TO BERM #3
4	Reservoir	12.00	2	734	37,031	3	689.43	12,315	BERM #3
5	SCS Runoff	4.776	2	726	16,499				POI 2 PRE - CHANGED AREA
6	Combine	45.11	2	728	153,933	2, 4,			TOTAL POST POI 2
7	SCS Runoff	3.838	2	726	13,252				Post to Swale #4
21-	21-4-16 stormwater.gpw POI2.gpw					Period: 100	Year	Thursday	02 / 22 / 2024

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Thursday, 02 / 22 / 2024

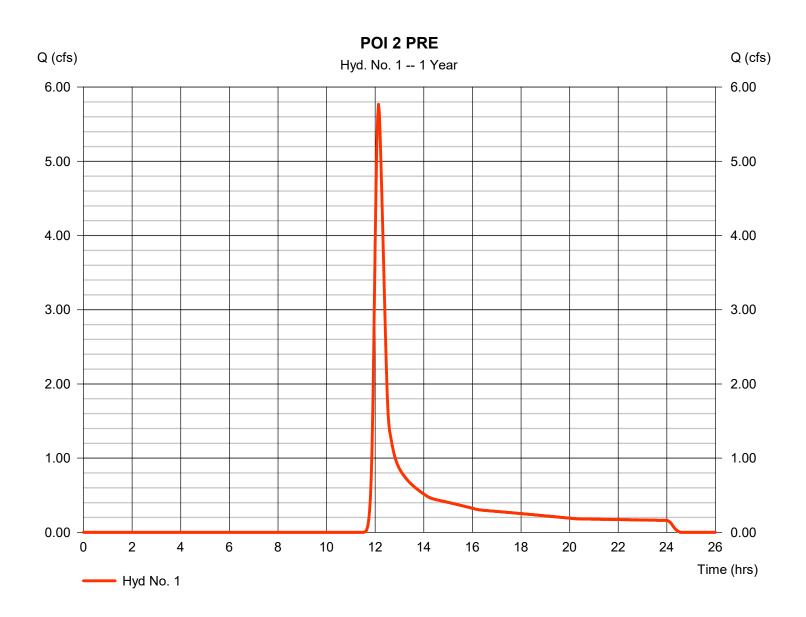
## Hyd. No. 1

POI 2 PRE

Hydrograph type = SCS Runoff Peak discharge = 5.768 cfsStorm frequency = 1 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 22.698 cuft Curve number = 75\* Drainage area = 10.360 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55

Total precip. = 2.40 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.700 x 98) + (3.510 x 77) + (5.400 x 70) + (0.480 x 80) + (0.270 x 74)] / 10.360



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

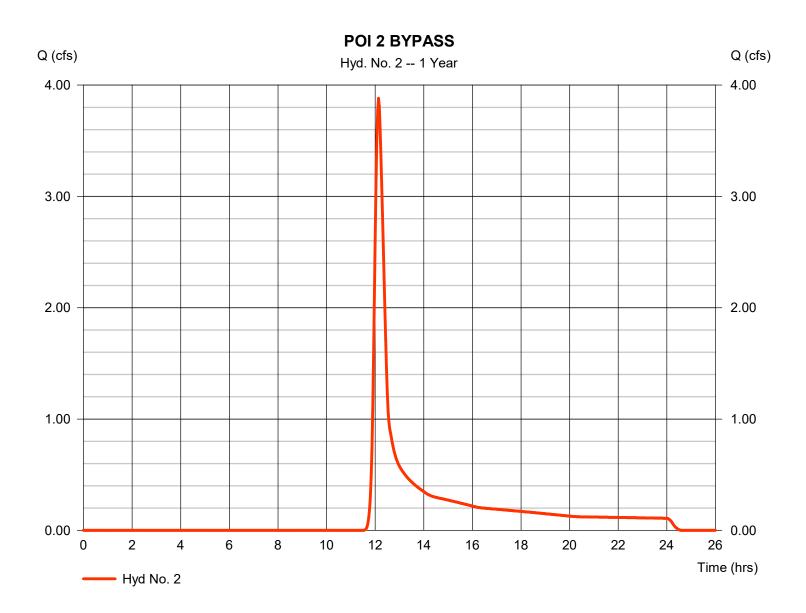
Thursday, 02 / 22 / 2024

## Hyd. No. 2

POI 2 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 3.881 cfsStorm frequency = 1 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 15.271 cuft Curve number Drainage area = 6.970 ac= 75\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. = 2.40 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(1.710 \times 77) + (0.700 \times 98) + (3.610 \times 70) + (0.110 \times 78) + (0.220 \times 71) + (0.620 \times 77)] / 6.970$ 



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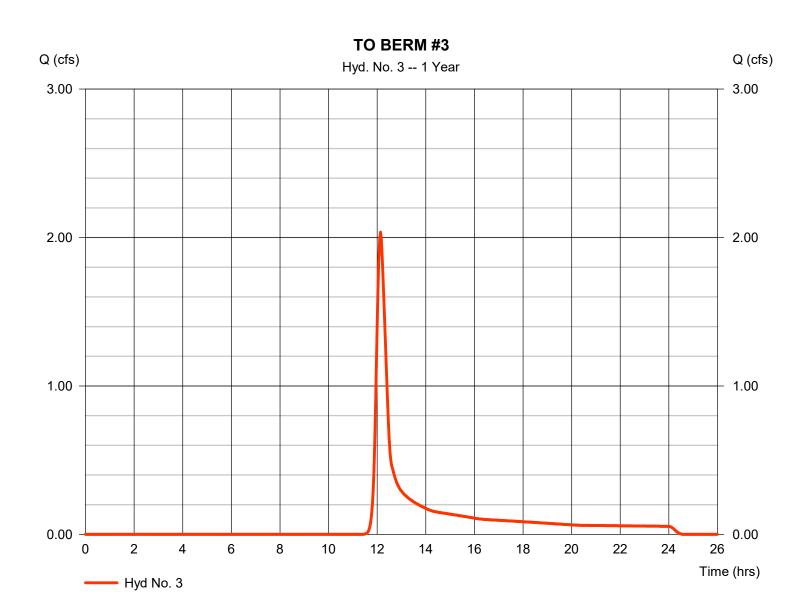
Thursday, 02 / 22 / 2024

#### Hyd. No. 3

TO BERM #3

Hydrograph type = SCS Runoff Peak discharge = 2.036 cfsStorm frequency = 1 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 7.834 cuft = 76\* Drainage area = 3.340 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.84 min = TR55 Total precip. = 2.40 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.160 \times 98) + (0.860 \times 70) + (1.640 \times 77) + (0.320 \times 74) + (0.210 \times 71) + (0.150 \times 80)] / 3.340$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

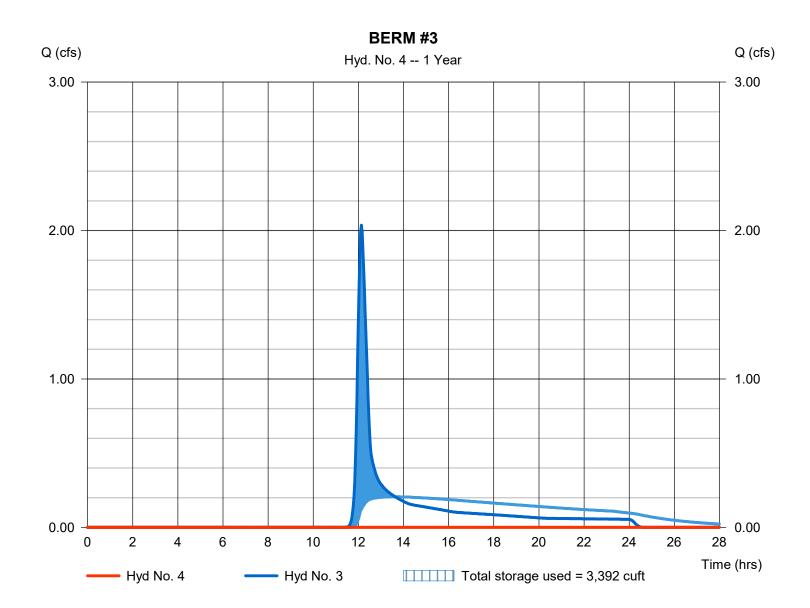
Thursday, 02 / 22 / 2024

#### Hyd. No. 4

BERM #3

= Reservoir Hydrograph type Peak discharge = 0.000 cfsStorm frequency = 1 yrsTime to peak  $= 16.57 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Inflow hyd. No. = 3 - TO BERM #3 Max. Elevation  $= 687.81 \, \text{ft}$ = BERM #3 Reservoir name Max. Storage = 3,392 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

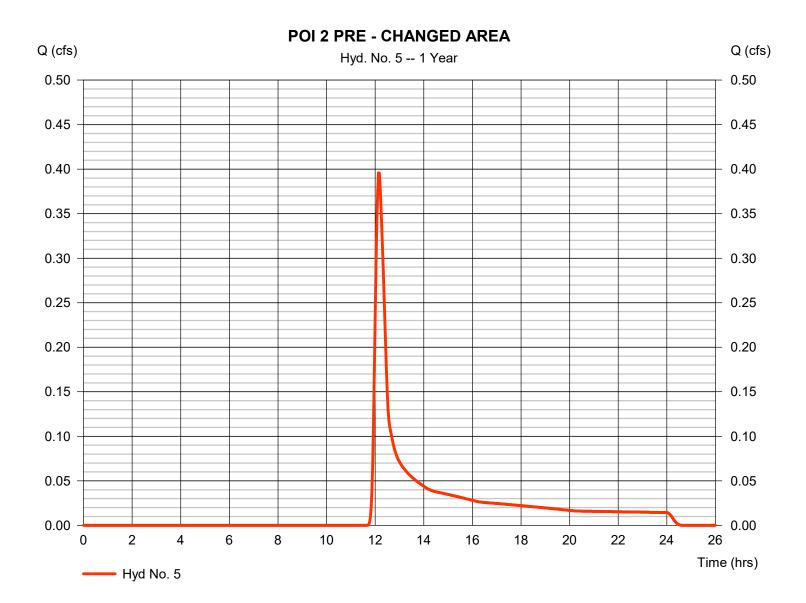
Thursday, 02 / 22 / 2024

#### Hyd. No. 5

#### POI 2 PRE - CHANGED AREA

Hydrograph type = SCS Runoff Peak discharge = 0.396 cfsStorm frequency = 1 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 1.781 cuft Drainage area Curve number = 71\* = 1.090 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.30 min = TR55 Total precip. = 2.40 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.930 x 70) + (0.160 x 77)] / 1.090



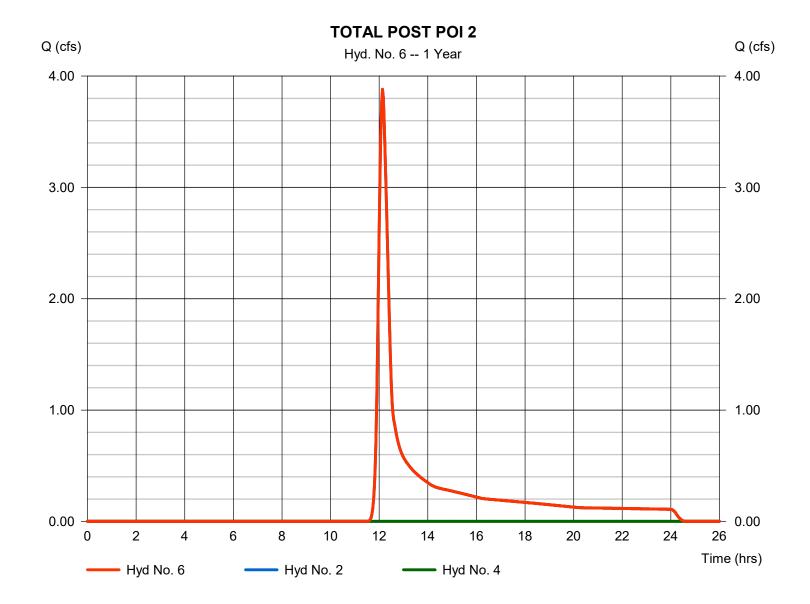
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Thursday, 02 / 22 / 2024

#### Hyd. No. 6

**TOTAL POST POI 2** 

Hydrograph type = Combine Peak discharge = 3.881 cfsTime to peak Storm frequency = 1 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 15,271 cuft Inflow hyds. = 2,4 Contrib. drain. area = 6.970 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

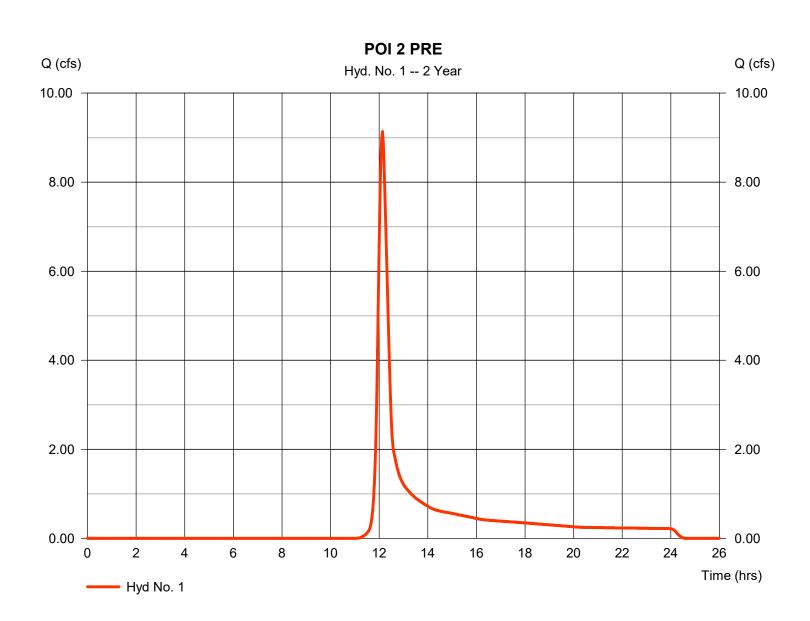
Thursday, 02 / 22 / 2024

#### Hyd. No. 1

POI 2 PRE

Hydrograph type = SCS Runoff Peak discharge = 9.134 cfsStorm frequency = 2 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 33.808 cuft Drainage area Curve number = 75\* = 10.360 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. = 2.88 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.700 \times 98) + (3.510 \times 77) + (5.400 \times 70) + (0.480 \times 80) + (0.270 \times 74)] / 10.360$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

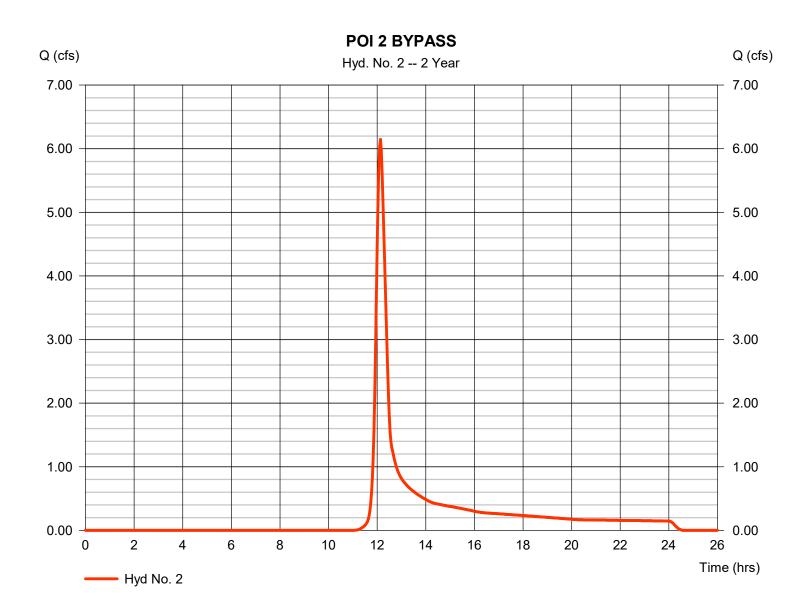
Thursday, 02 / 22 / 2024

#### Hyd. No. 2

POI 2 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 6.145 cfsStorm frequency = 2 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 22.745 cuft Drainage area Curve number = 75\* = 6.970 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. = 2.88 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(1.710 \times 77) + (0.700 \times 98) + (3.610 \times 70) + (0.110 \times 78) + (0.220 \times 71) + (0.620 \times 77)] / 6.970$ 



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= 24 hrs

Thursday, 02 / 22 / 2024

= 484

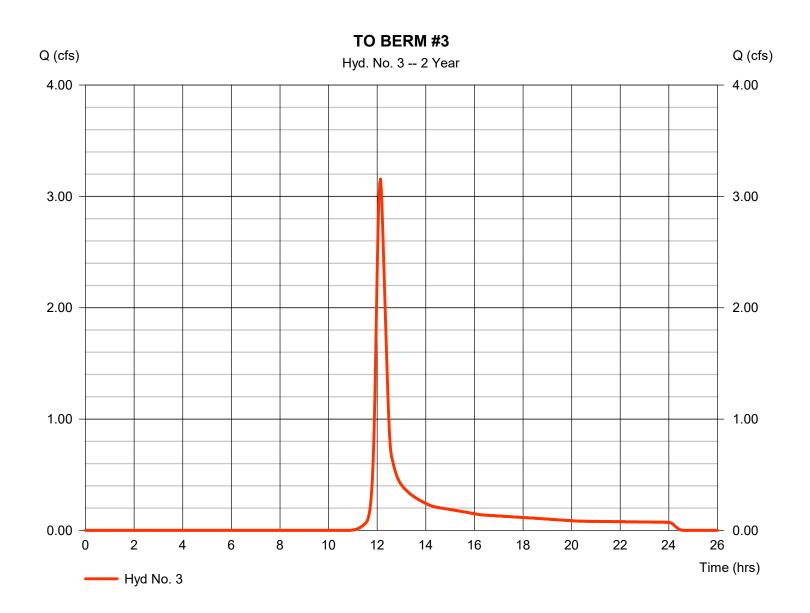
#### Hyd. No. 3

TO BERM #3

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 3.156 cfsStorm frequency = 2 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 11,540 cuftCurve number Drainage area = 3.340 ac= 76\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.84 min = TR55 Total precip. = 2.88 inDistribution = Type II Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.160 \times 98) + (0.860 \times 70) + (1.640 \times 77) + (0.320 \times 74) + (0.210 \times 71) + (0.150 \times 80)] / 3.340$ 



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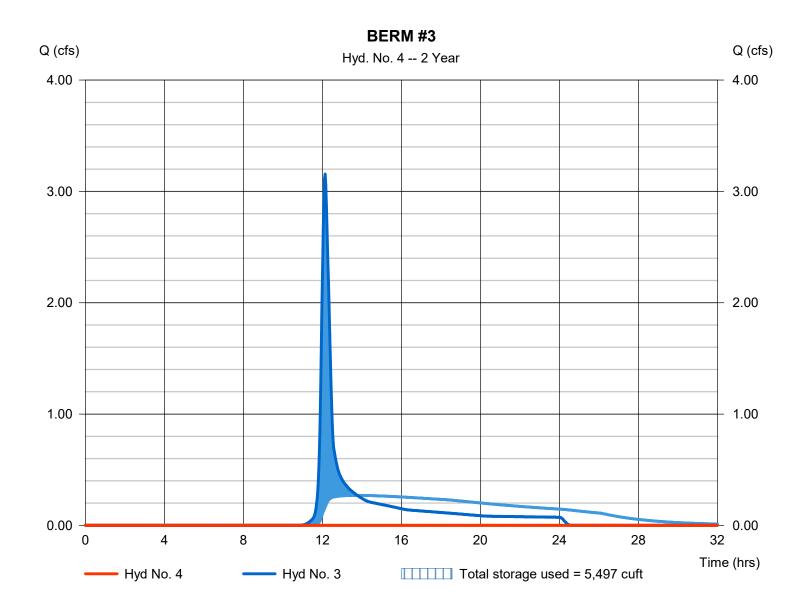
Thursday, 02 / 22 / 2024

#### Hyd. No. 4

BERM #3

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency = 2 yrsTime to peak  $= 13.33 \, hrs$ Time interval = 2 min Hyd. volume = 0 cuft Inflow hyd. No. = 3 - TO BERM #3 Max. Elevation = 688.30 ft= BERM #3 Reservoir name Max. Storage = 5,497 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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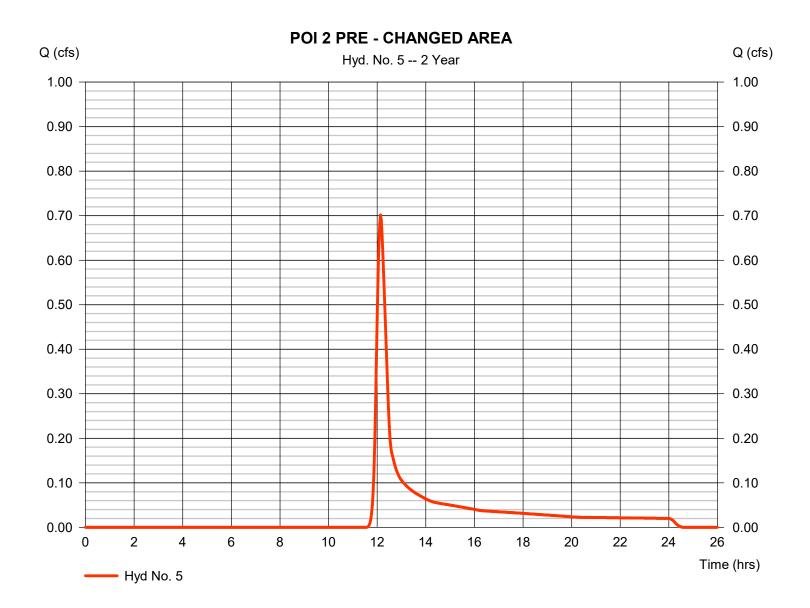
Thursday, 02 / 22 / 2024

#### Hyd. No. 5

#### POI 2 PRE - CHANGED AREA

Hydrograph type = SCS Runoff Peak discharge = 0.702 cfsStorm frequency = 2 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 2.788 cuft Curve number = 71\* Drainage area = 1.090 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.30 min = TR55 Total precip. = 2.88 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.930 \times 70) + (0.160 \times 77)] / 1.090$ 



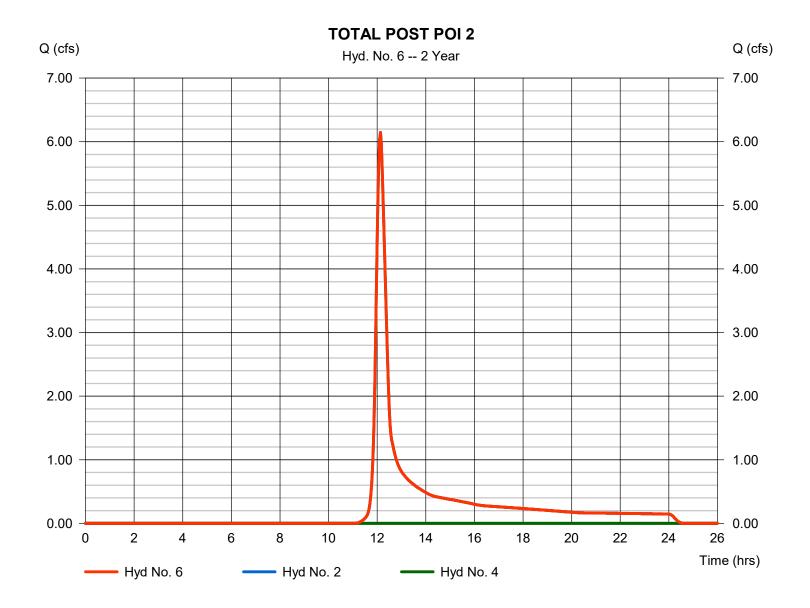
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#### Hyd. No. 6

**TOTAL POST POI 2** 

Hydrograph type = Combine Peak discharge = 6.145 cfsStorm frequency Time to peak = 2 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 22,745 cuft Inflow hyds. = 2,4 Contrib. drain. area = 6.970 ac



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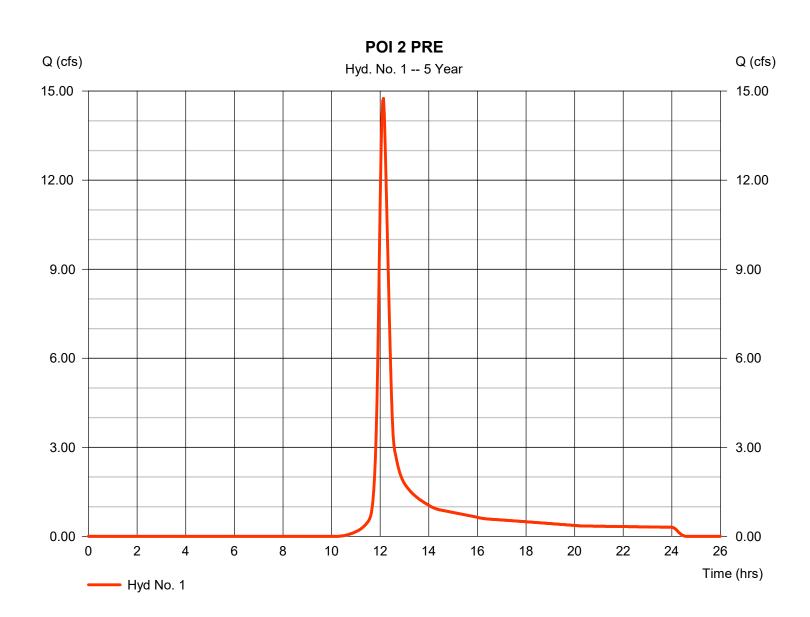
Thursday, 02 / 22 / 2024

#### Hyd. No. 1

POI 2 PRE

Hydrograph type = SCS Runoff Peak discharge = 14.76 cfsStorm frequency = 5 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 52.558 cuft Curve number = 75\* Drainage area = 10.360 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. Distribution = Type II = 3.60 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.700 \times 98) + (3.510 \times 77) + (5.400 \times 70) + (0.480 \times 80) + (0.270 \times 74)] / 10.360$ 



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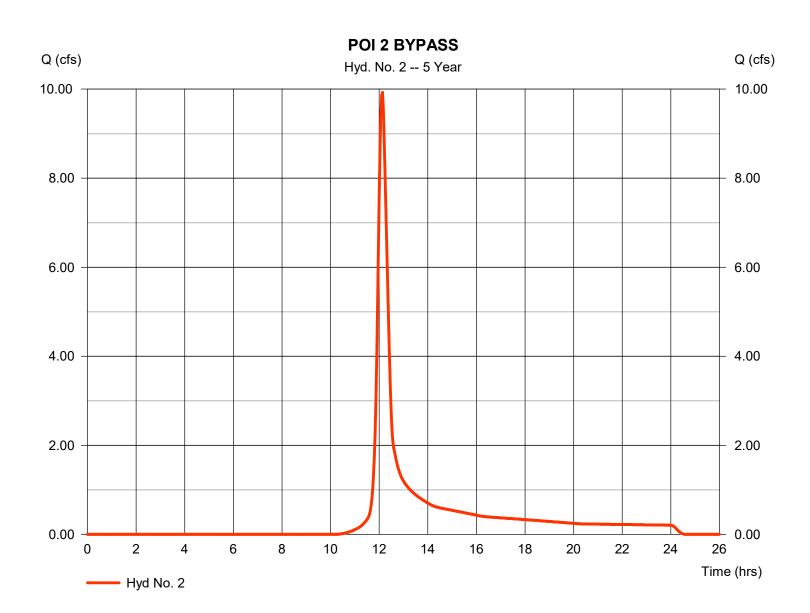
Thursday, 02 / 22 / 2024

#### Hyd. No. 2

POI 2 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 9.927 cfsStorm frequency = 5 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 35.360 cuft Curve number = 75\* Drainage area = 6.970 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. Distribution = Type II = 3.60 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(1.710 \times 77) + (0.700 \times 98) + (3.610 \times 70) + (0.110 \times 78) + (0.220 \times 71) + (0.620 \times 77)] / 6.970$ 



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#### Hyd. No. 3

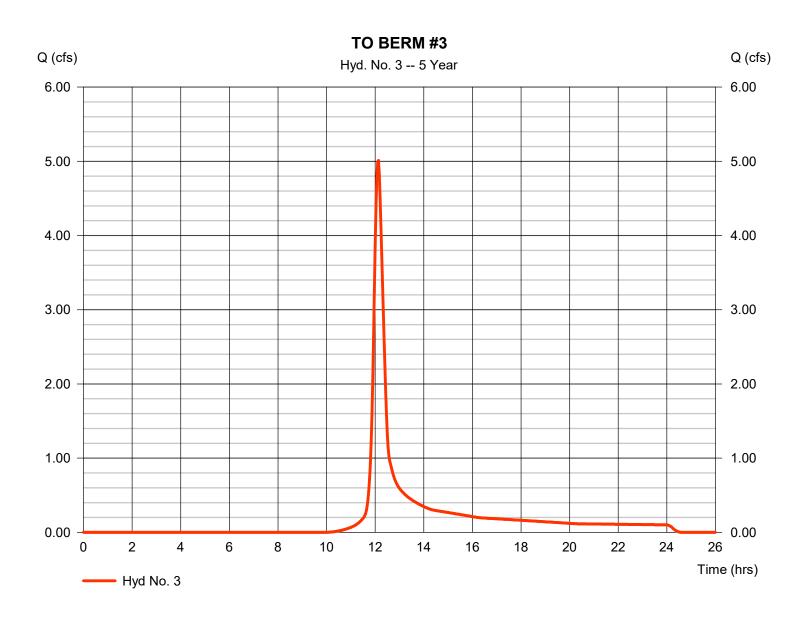
TO BERM #3

Hydrograph type = SCS Runoff Peak discharge = 5.011 cfsStorm frequency = 5 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 17,750 cuftCurve number Drainage area = 3.340 ac= 76\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.84 min = TR55

Total precip. = 3.60 in Distribution = 1895

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.160 \times 98) + (0.860 \times 70) + (1.640 \times 77) + (0.320 \times 74) + (0.210 \times 71) + (0.150 \times 80)] / 3.340$ 



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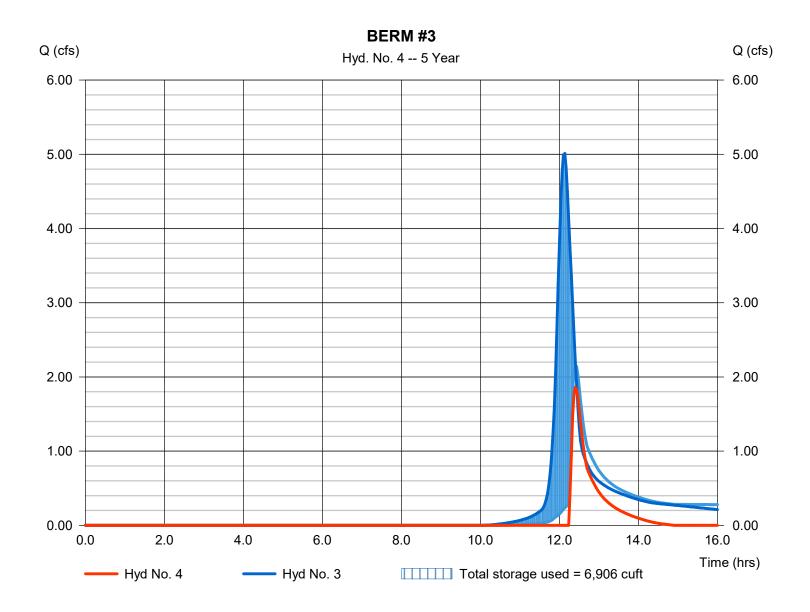
Thursday, 02 / 22 / 2024

#### Hyd. No. 4

BERM #3

Hydrograph type Peak discharge = 1.859 cfs= Reservoir Storm frequency = 5 yrsTime to peak  $= 12.40 \, hrs$ Time interval = 2 min Hyd. volume = 3,677 cuft= 3 - TO BERM #3 Max. Elevation Inflow hyd. No.  $= 688.58 \, \text{ft}$ = BERM #3 Reservoir name Max. Storage = 6,906 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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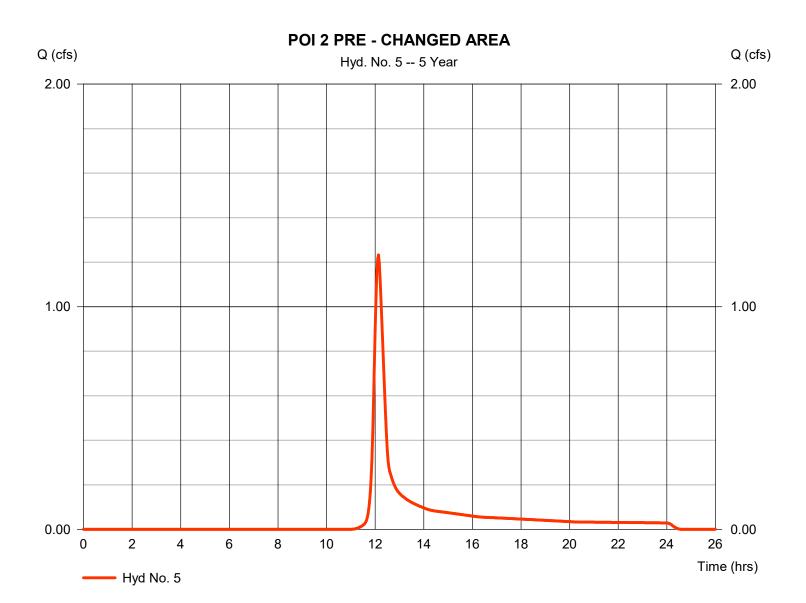
Thursday, 02 / 22 / 2024

#### Hyd. No. 5

#### POI 2 PRE - CHANGED AREA

Hydrograph type = SCS Runoff Peak discharge = 1.233 cfsStorm frequency = 5 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 4,542 cuftCurve number = 71\* Drainage area = 1.090 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.30 min = TR55 Total precip. = 3.60 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.930 \times 70) + (0.160 \times 77)] / 1.090$ 



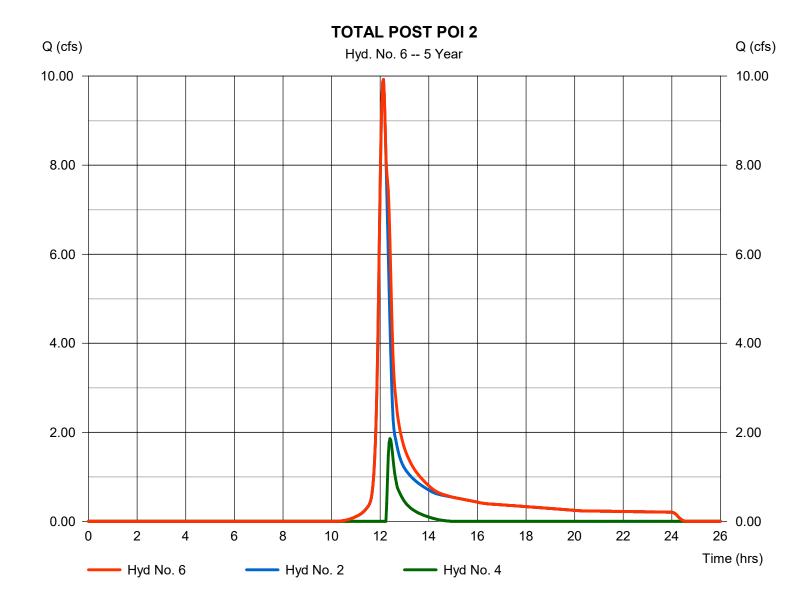
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#### Hyd. No. 6

**TOTAL POST POI 2** 

Hydrograph type = Combine Peak discharge = 9.927 cfsStorm frequency Time to peak = 5 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 39,037 cuft Inflow hyds. = 2,4 Contrib. drain. area = 6.970 ac



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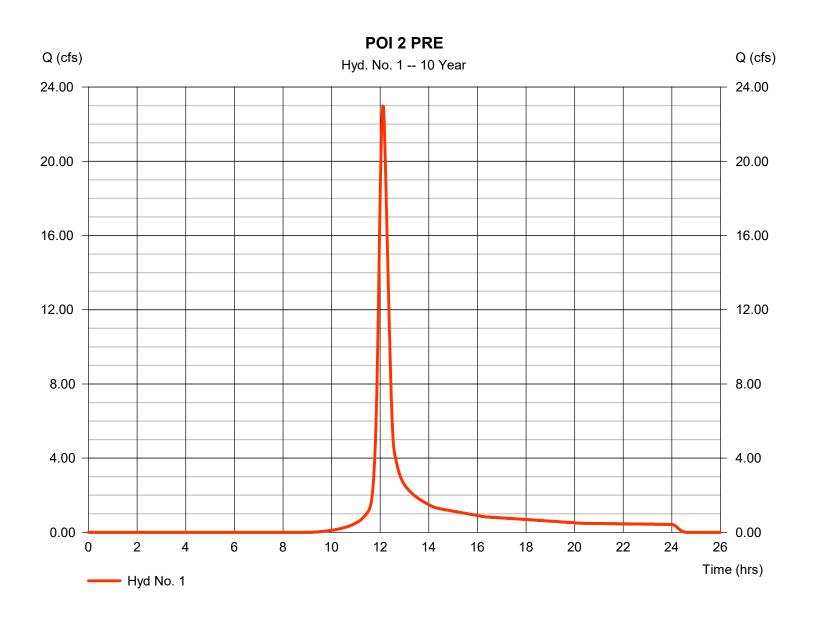
Thursday, 02 / 22 / 2024

#### Hyd. No. 1

POI 2 PRE

Hydrograph type = SCS Runoff Peak discharge = 22.98 cfsStorm frequency = 10 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 80.289 cuft Curve number Drainage area = 10.360 ac= 75\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. = 4.56 inDistribution = Type II

<sup>\*</sup> Composite (Area/CN) = [(0.700 x 98) + (3.510 x 77) + (5.400 x 70) + (0.480 x 80) + (0.270 x 74)] / 10.360



Storm duration = 24 hrs Shape factor = 484

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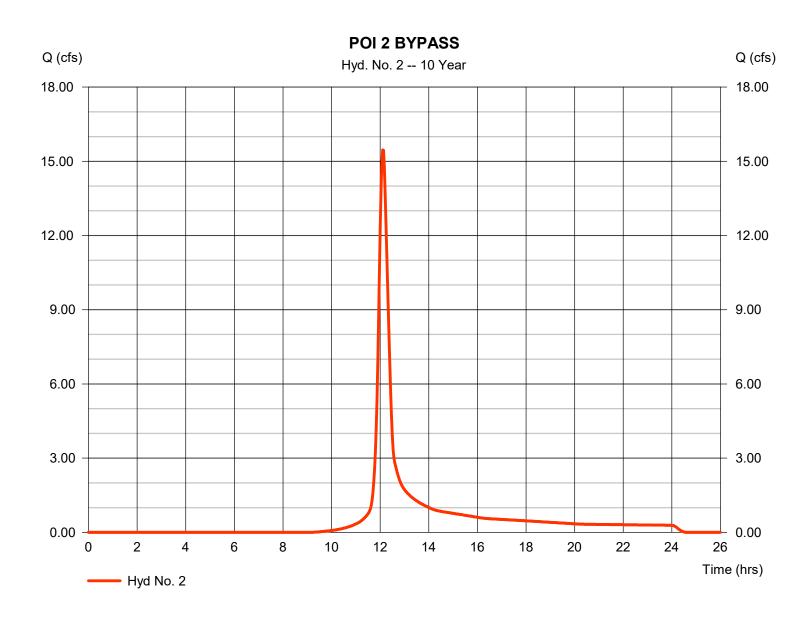
Thursday, 02 / 22 / 2024

#### Hyd. No. 2

POI 2 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 15.46 cfsStorm frequency = 10 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 54.017 cuftDrainage area Curve number = 75\* = 6.970 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. = 4.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(1.710 \times 77) + (0.700 \times 98) + (3.610 \times 70) + (0.110 \times 78) + (0.220 \times 71) + (0.620 \times 77)] / 6.970$ 



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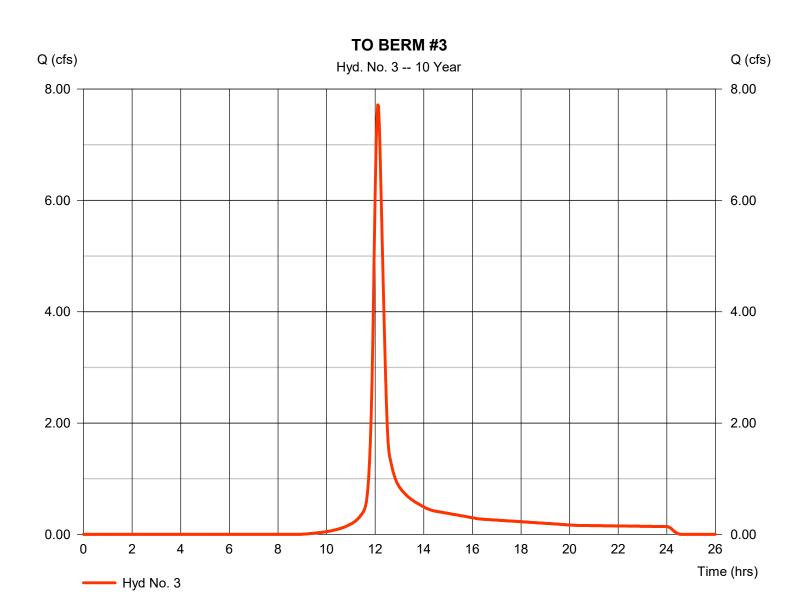
Thursday, 02 / 22 / 2024

#### Hyd. No. 3

TO BERM #3

Hydrograph type = SCS Runoff Peak discharge = 7.718 cfsStorm frequency = 10 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 26.875 cuft Drainage area = 3.340 acCurve number = 76\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.84 min = TR55 Total precip. = 4.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.160 \times 98) + (0.860 \times 70) + (1.640 \times 77) + (0.320 \times 74) + (0.210 \times 71) + (0.150 \times 80)] / 3.340$ 



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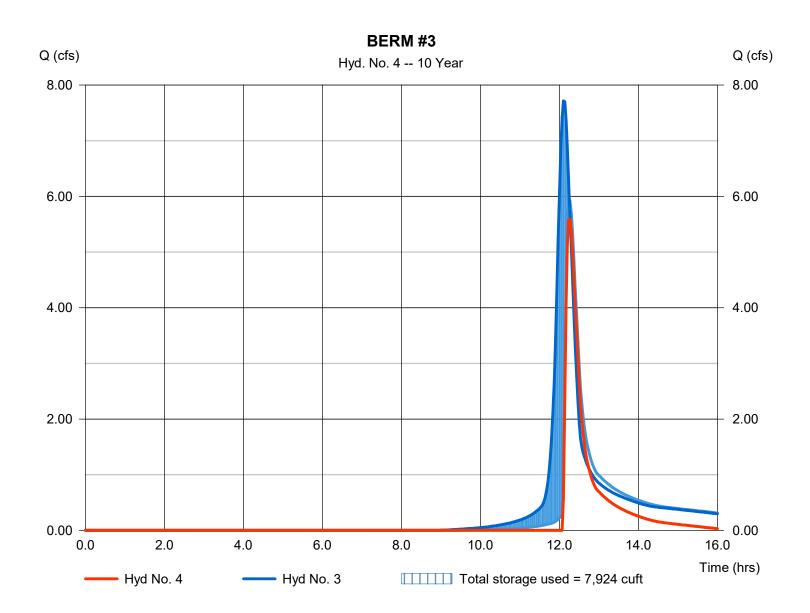
Thursday, 02 / 22 / 2024

#### Hyd. No. 4

BERM #3

Hydrograph type Peak discharge = 5.592 cfs= Reservoir Storm frequency = 10 yrsTime to peak  $= 12.27 \, hrs$ Time interval = 2 min Hyd. volume = 10,699 cuft= 3 - TO BERM #3 Max. Elevation Inflow hyd. No. = 688.78 ft= BERM #3 Reservoir name Max. Storage = 7,924 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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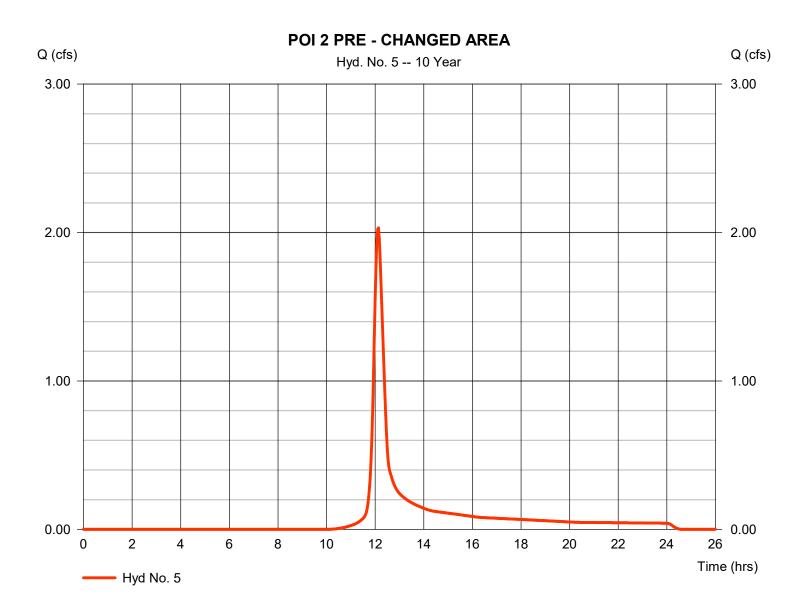
Thursday, 02 / 22 / 2024

#### Hyd. No. 5

#### POI 2 PRE - CHANGED AREA

Hydrograph type = SCS Runoff Peak discharge = 2.031 cfsStorm frequency = 10 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 7.209 cuft= 71\* Drainage area = 1.090 acCurve number Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.30 min = TR55 Total precip. = 4.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.930 \times 70) + (0.160 \times 77)] / 1.090$ 



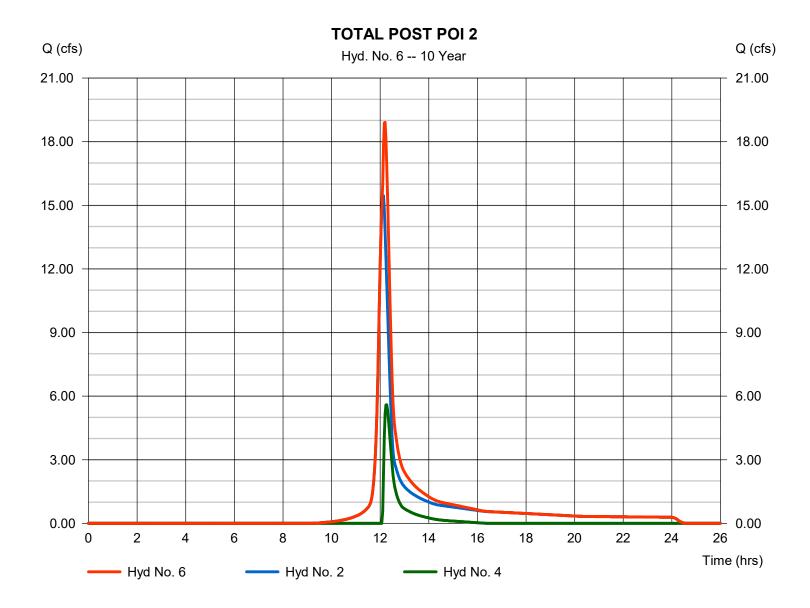
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#### Hyd. No. 6

**TOTAL POST POI 2** 

Hydrograph type = Combine Peak discharge = 18.91 cfsStorm frequency Time to peak = 10 yrs $= 12.20 \, hrs$ Time interval = 2 min Hyd. volume = 64,716 cuft Inflow hyds. = 2,4 Contrib. drain. area = 6.970 ac



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#### Hyd. No. 1

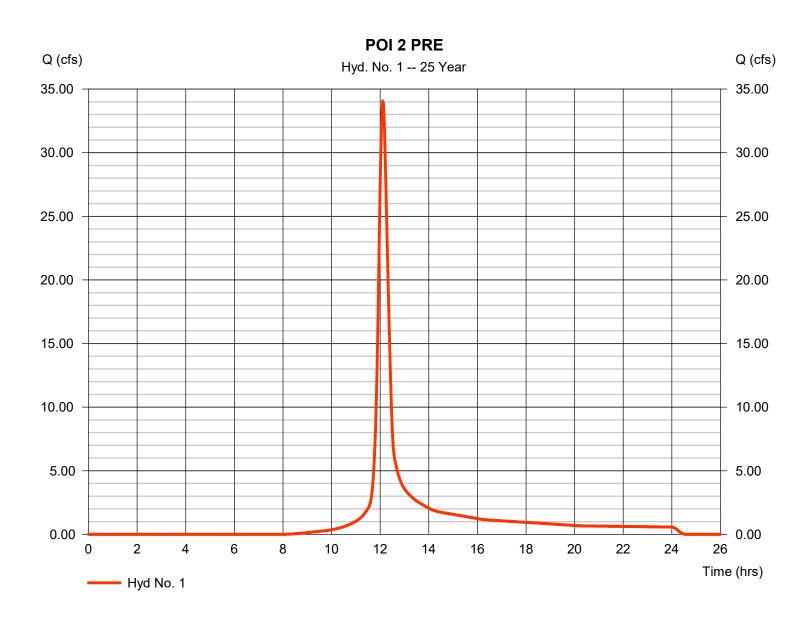
POI 2 PRE

Hydrograph type= SCS RunoffPeak discharge= 34.08 cfsStorm frequency= 25 yrsTime to peak= 12.10 hrsTime interval= 2 minHyd. volume= 117,842 cuft

Drainage area = 10.360 ac Curve number =  $75^*$  Basin Slope = 0.0 % Hydraulic length = 0.0 ft

Tc method = TR55 Time of conc. (Tc) = 23.00 min
Total precip. = 5.76 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.700 x 98) + (3.510 x 77) + (5.400 x 70) + (0.480 x 80) + (0.270 x 74)] / 10.360



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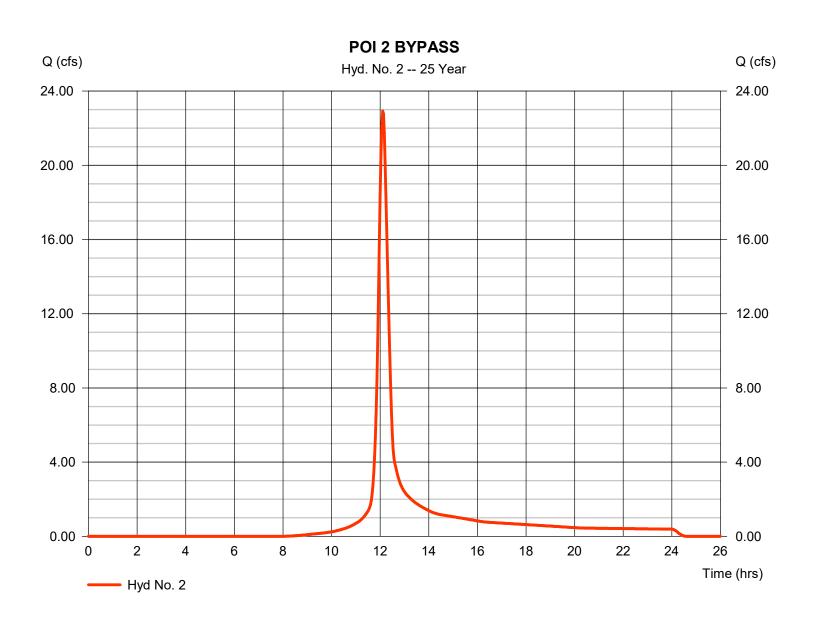
Thursday, 02 / 22 / 2024

#### Hyd. No. 2

POI 2 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 22.93 cfsStorm frequency = 25 yrs Time to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 79.282 cuft Curve number Drainage area = 6.970 ac= 75\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. Distribution = Type II = 5.76 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(1.710 \times 77) + (0.700 \times 98) + (3.610 \times 70) + (0.110 \times 78) + (0.220 \times 71) + (0.620 \times 77)] / (6.970) + (0.700 \times 98) + (0.700 \times 98) + (0.700 \times 78) + (0.700 \times 78)$ 



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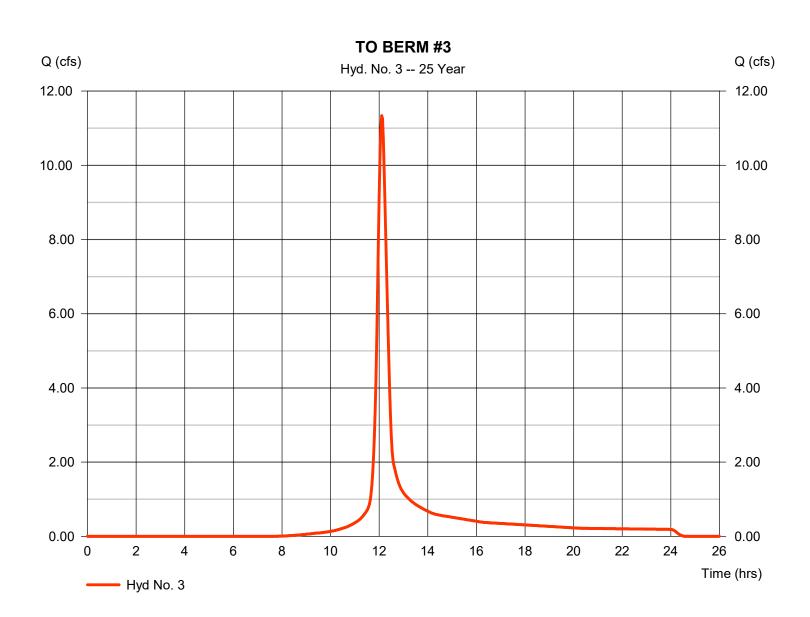
Thursday, 02 / 22 / 2024

#### Hyd. No. 3

TO BERM #3

Hydrograph type = SCS Runoff Peak discharge = 11.34 cfsStorm frequency = 25 yrs Time to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 39.169 cuft Curve number Drainage area = 3.340 ac= 76\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.84 min = TR55 Total precip. Distribution = Type II = 5.76 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.160 \times 98) + (0.860 \times 70) + (1.640 \times 77) + (0.320 \times 74) + (0.210 \times 71) + (0.150 \times 80)] / 3.340$ 



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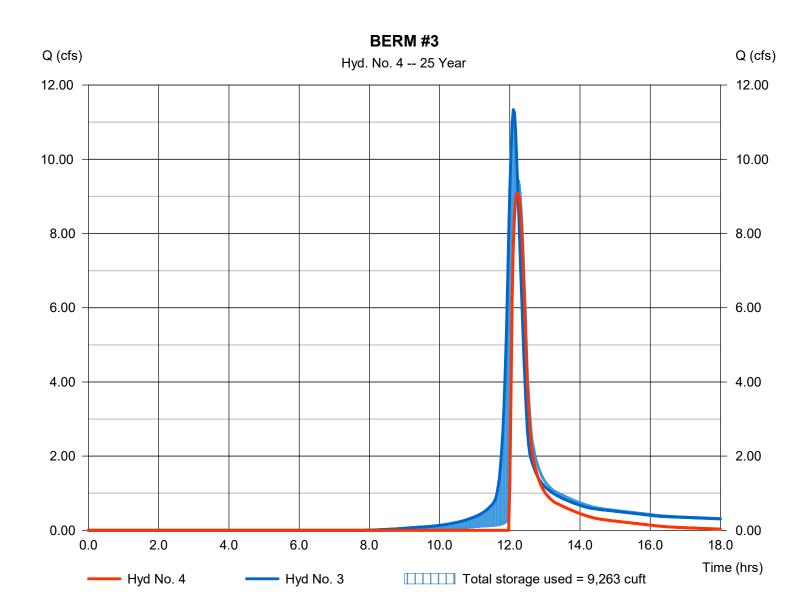
Thursday, 02 / 22 / 2024

#### Hyd. No. 4

BERM #3

Hydrograph type = Reservoir Peak discharge = 9.083 cfsStorm frequency = 25 yrsTime to peak  $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 20,953 cuftInflow hyd. No. = 3 - TO BERM #3 Max. Elevation = 689.03 ft= BERM #3 Reservoir name Max. Storage = 9,263 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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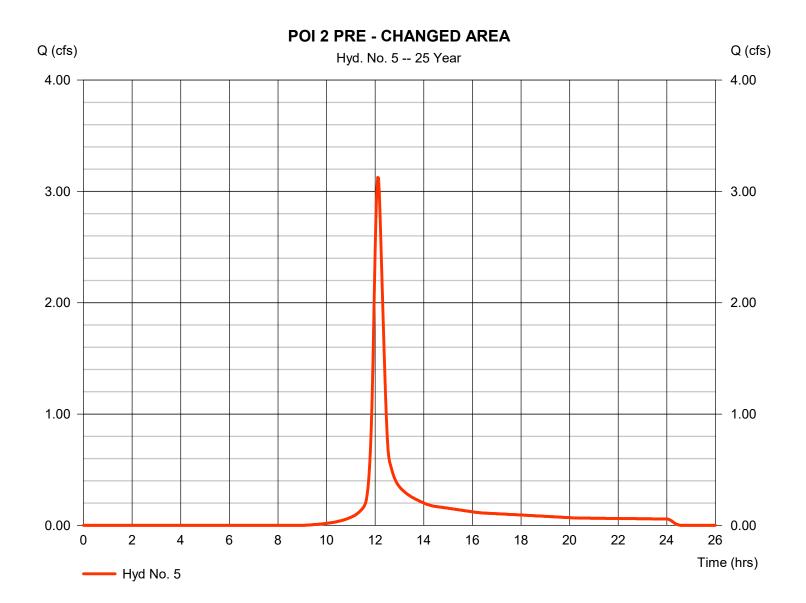
Thursday, 02 / 22 / 2024

#### Hyd. No. 5

#### POI 2 PRE - CHANGED AREA

Hydrograph type = SCS Runoff Peak discharge = 3.126 cfsStorm frequency = 25 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 10.900 cuftCurve number Drainage area = 1.090 ac= 71\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.30 min = TR55 Total precip. Distribution = Type II = 5.76 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.930 \times 70) + (0.160 \times 77)] / 1.090$ 



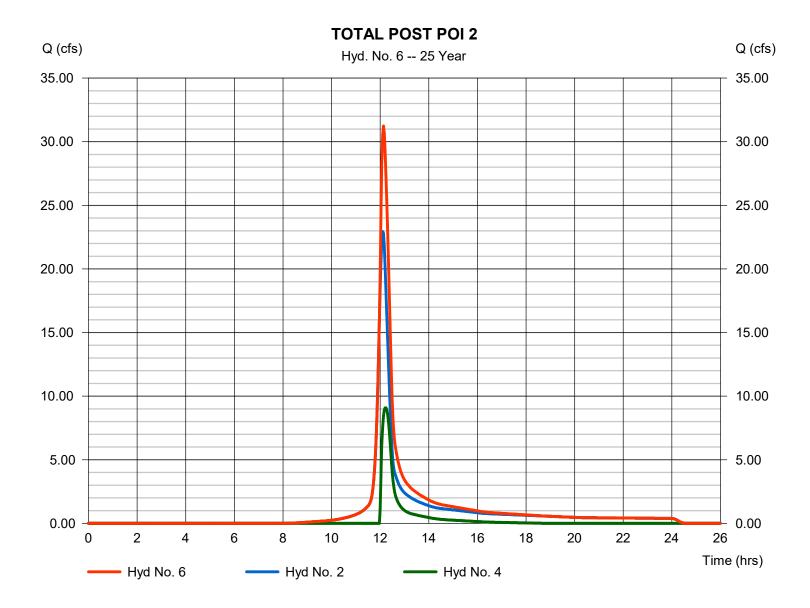
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#### Hyd. No. 6

**TOTAL POST POI 2** 

= 31.23 cfsHydrograph type = Combine Peak discharge Storm frequency = 25 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 100,235 cuft Inflow hyds. = 2,4 Contrib. drain. area = 6.970 ac



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#### Hyd. No. 1

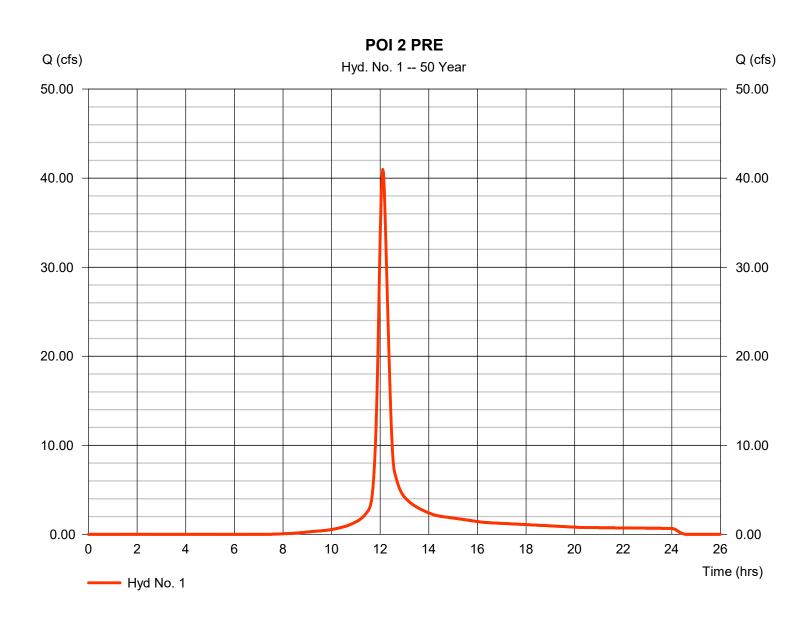
POI 2 PRE

Hydrograph type= SCS RunoffPeak discharge= 40.96 cfsStorm frequency= 50 yrsTime to peak= 12.10 hrsTime interval= 2 minHyd. volume= 141,430 cuft

Drainage area = 10.360 ac Curve number =  $75^*$  Basin Slope = 0.0 % Hydraulic length = 0.0 ft

Tc method = TR55 Time of conc. (Tc) = 23.00 min
Total precip. = 6.48 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.700 x 98) + (3.510 x 77) + (5.400 x 70) + (0.480 x 80) + (0.270 x 74)] / 10.360



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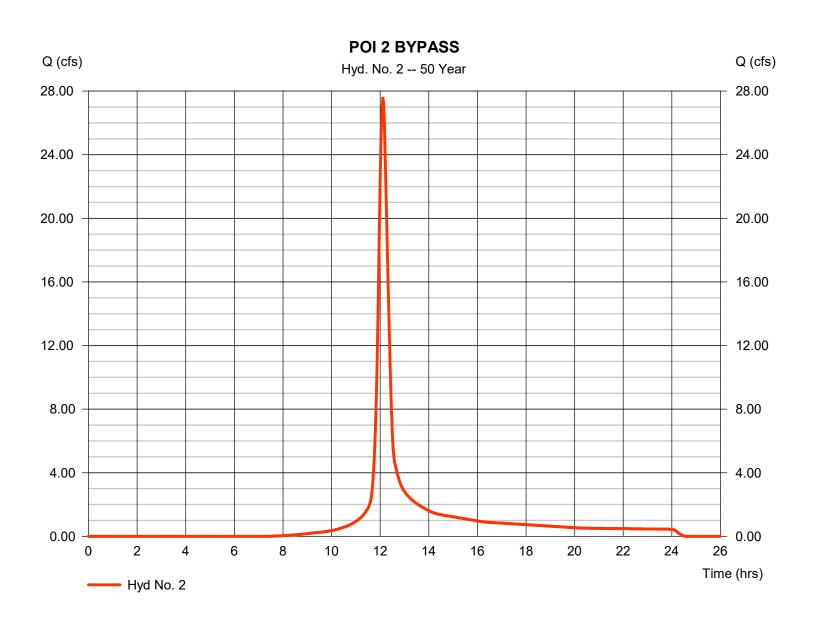
Thursday, 02 / 22 / 2024

#### Hyd. No. 2

POI 2 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 27.56 cfsStorm frequency = 50 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 95.151 cuft Curve number Drainage area = 6.970 ac= 75\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 23.00 min = TR55 Total precip. Distribution = Type II = 6.48 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(1.710 \times 77) + (0.700 \times 98) + (3.610 \times 70) + (0.110 \times 78) + (0.220 \times 71) + (0.620 \times 77)] / 6.970$ 



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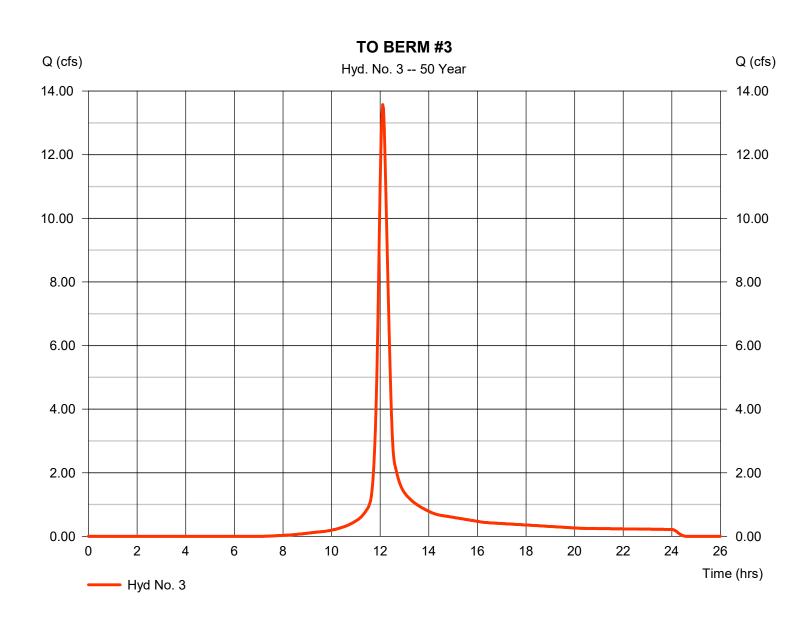
Thursday, 02 / 22 / 2024

#### Hyd. No. 3

TO BERM #3

Hydrograph type = SCS Runoff Peak discharge = 13.58 cfsStorm frequency = 50 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 46.867 cuft Drainage area = 3.340 acCurve number = 76\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.84 min = TR55 Total precip. Distribution = Type II = 6.48 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.160 \times 98) + (0.860 \times 70) + (1.640 \times 77) + (0.320 \times 74) + (0.210 \times 71) + (0.150 \times 80)] / 3.340$ 



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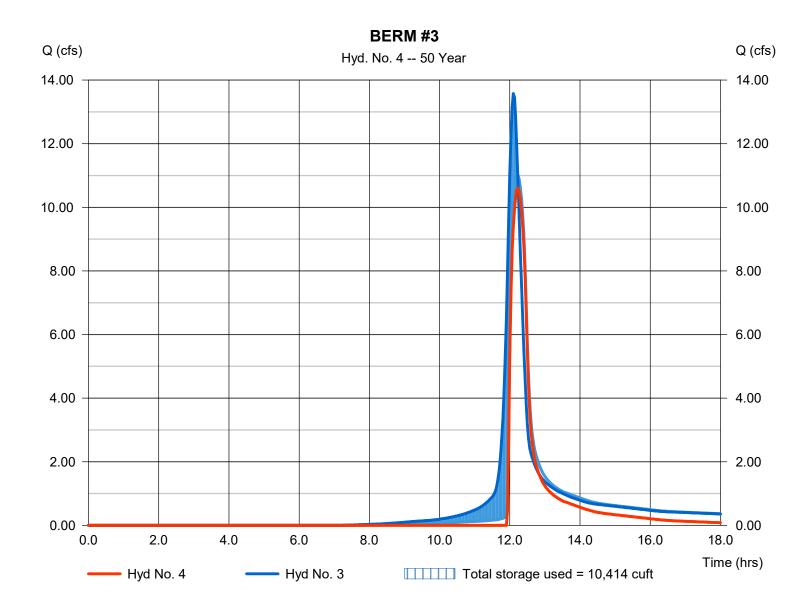
Thursday, 02 / 22 / 2024

#### Hyd. No. 4

BERM #3

Hydrograph type Peak discharge = 10.60 cfs= Reservoir Storm frequency = 50 yrsTime to peak  $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 27,663 cuft= 3 - TO BERM #3 Max. Elevation = 689.18 ftInflow hyd. No. = BERM #3 Reservoir name Max. Storage = 10,414 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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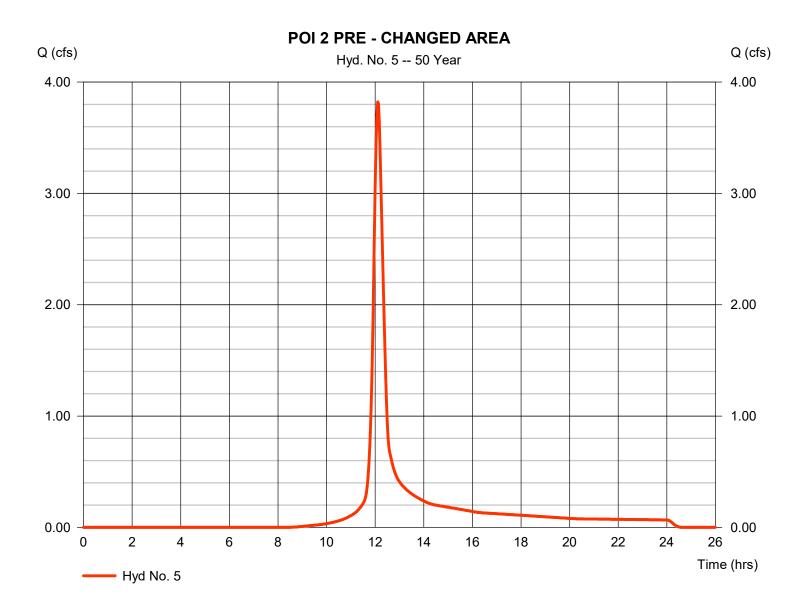
Thursday, 02 / 22 / 2024

#### Hyd. No. 5

#### POI 2 PRE - CHANGED AREA

Hydrograph type = SCS Runoff Peak discharge = 3.822 cfsStorm frequency = 50 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 13.250 cuft Curve number Drainage area = 1.090 ac= 71\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.30 min = TR55 Total precip. = 6.48 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) = [(0.930 x 70) + (0.160 x 77)] / 1.090



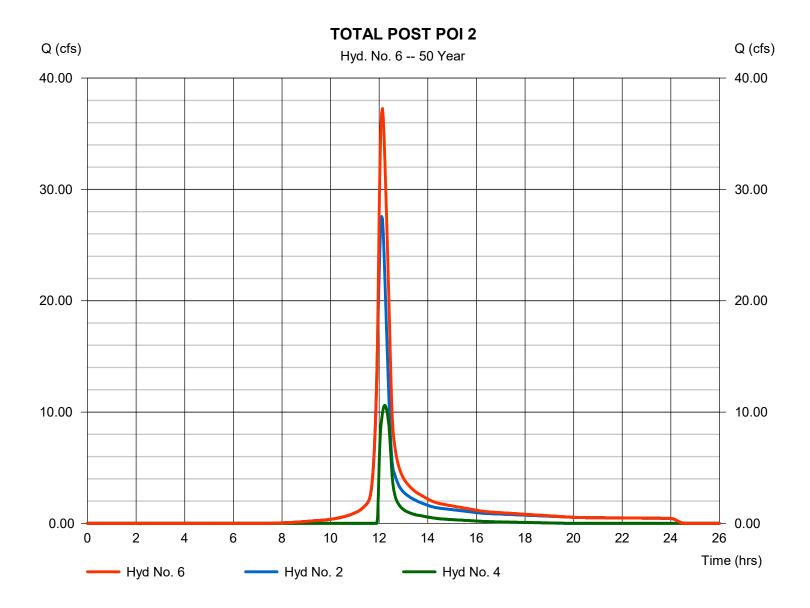
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Thursday, 02 / 22 / 2024

#### Hyd. No. 6

**TOTAL POST POI 2** 

= 37.26 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 50 yrs $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 122,814 cuft Inflow hyds. = 2,4 Contrib. drain. area = 6.970 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

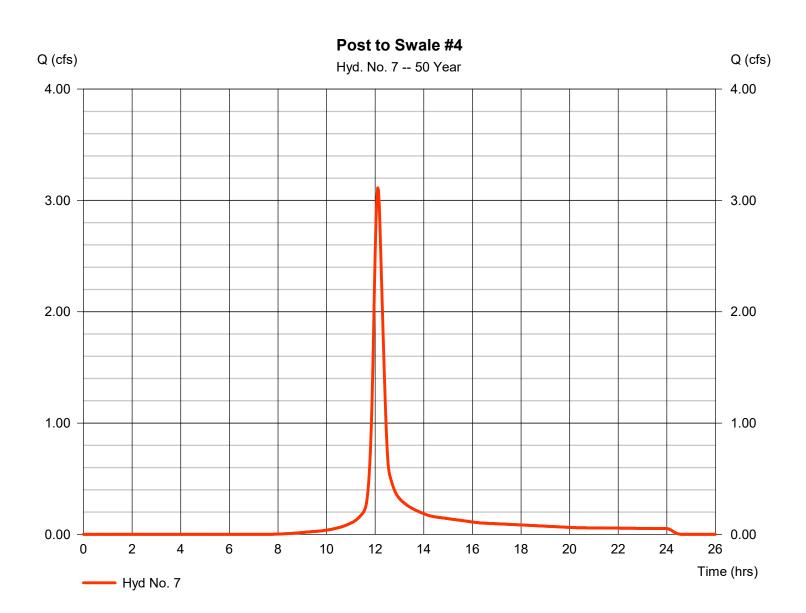
Thursday, 02 / 22 / 2024

#### Hyd. No. 7

Post to Swale #4

Hydrograph type = SCS Runoff Peak discharge = 3.113 cfsStorm frequency = 50 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 10,752 cuftDrainage area Curve number = 0.810 ac= 74\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 22.80 min = TR55 Total precip. = 6.48 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.470 \times 77) + (0.270 \times 70) + (0.070 \times 74)] / 0.810$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Thursday, 02 / 22 / 2024

#### Hyd. No. 1

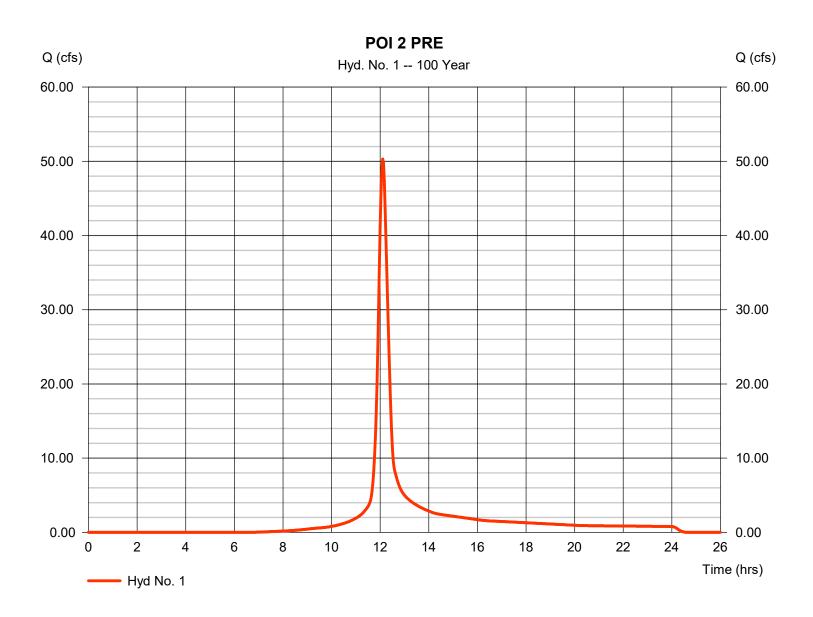
POI 2 PRE

Hydrograph type= SCS RunoffPeak discharge= 50.30 cfsStorm frequency= 100 yrsTime to peak= 12.10 hrsTime interval= 2 minHyd. volume= 173,760 cuftDrainage area= 10.360 acCurve number= 75\*

Drainage area = 10.360 ac Curve number =  $75^*$  Basin Slope = 0.0 % Hydraulic length = 0.0 ft

Tc method = TR55 Time of conc. (Tc) = 23.00 min
Total precip. = 7.44 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.700 x 98) + (3.510 x 77) + (5.400 x 70) + (0.480 x 80) + (0.270 x 74)] / 10.360



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Thursday, 02 / 22 / 2024

### Hyd. No. 2

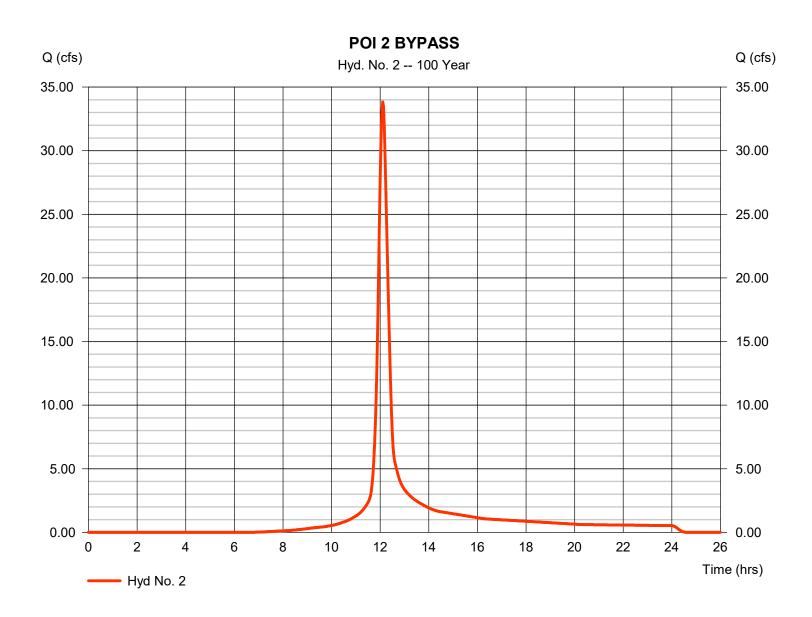
POI 2 BYPASS

Hydrograph type = SCS Runoff Peak discharge = 33.84 cfsStorm frequency = 100 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 116.902 cuft Curve number = 75\* Drainage area = 6.970 ac

Basin Slope = 0.0 % Hydraulic length = 0 ft
Tc method = TR55 Time of conc. (Tc) = 23.00 min

Total precip. = 7.44 in Distribution = Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(1.710 \times 77) + (0.700 \times 98) + (3.610 \times 70) + (0.110 \times 78) + (0.220 \times 71) + (0.620 \times 77)] / 6.970$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 24 hrs

Thursday, 02 / 22 / 2024

= 484

### Hyd. No. 3

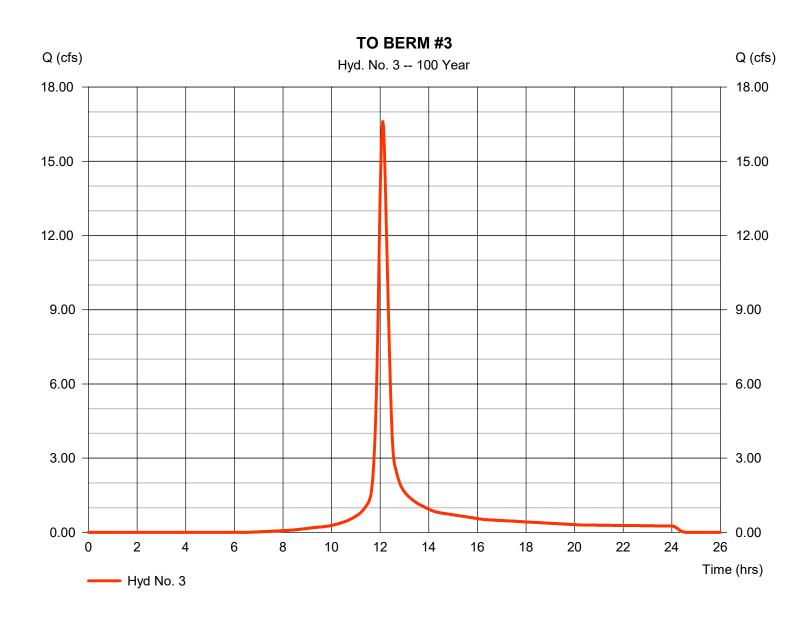
TO BERM #3

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 16.60 cfsStorm frequency = 100 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 57.398 cuft Curve number Drainage area = 3.340 ac= 76\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.84 min = TR55 Total precip. = 7.44 inDistribution = Type II

Shape factor

<sup>\*</sup> Composite (Area/CN) =  $[(0.160 \times 98) + (0.860 \times 70) + (1.640 \times 77) + (0.320 \times 74) + (0.210 \times 71) + (0.150 \times 80)] / 3.340$ 



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Thursday, 02 / 22 / 2024

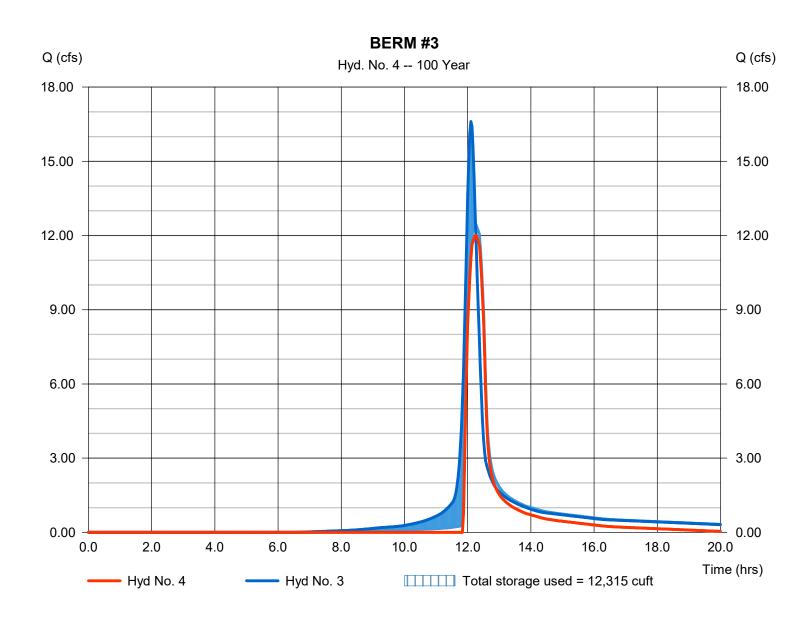
### Hyd. No. 4

BERM #3

Hydrograph type Peak discharge = 12.00 cfs= Reservoir Storm frequency = 100 yrsTime to peak  $= 12.23 \, hrs$ Time interval = 2 min Hyd. volume = 37,031 cuft= 3 - TO BERM #3 Max. Elevation Inflow hyd. No. = 689.43 ft= BERM #3 Reservoir name Max. Storage = 12,315 cuft

Storage Indication method used. Exfiltration extracted from Outflow.

#### **USED FOR LEVEL SPREADER #1**



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

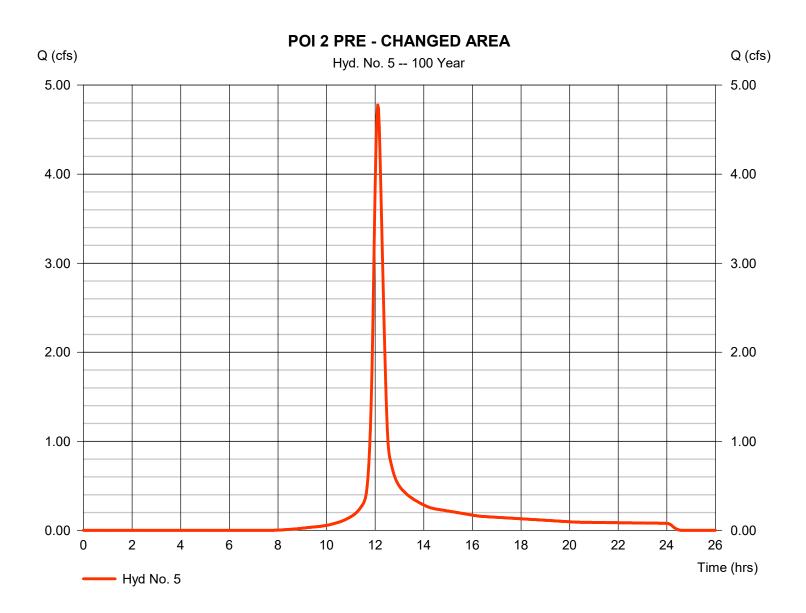
Thursday, 02 / 22 / 2024

### Hyd. No. 5

#### POI 2 PRE - CHANGED AREA

Hydrograph type = SCS Runoff Peak discharge = 4.776 cfsStorm frequency = 100 yrsTime to peak  $= 12.10 \, hrs$ Time interval = 2 min Hyd. volume = 16.499 cuft Curve number Drainage area = 1.090 ac= 71\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 21.30 min = TR55 Total precip. = 7.44 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.930 \times 70) + (0.160 \times 77)] / 1.090$ 



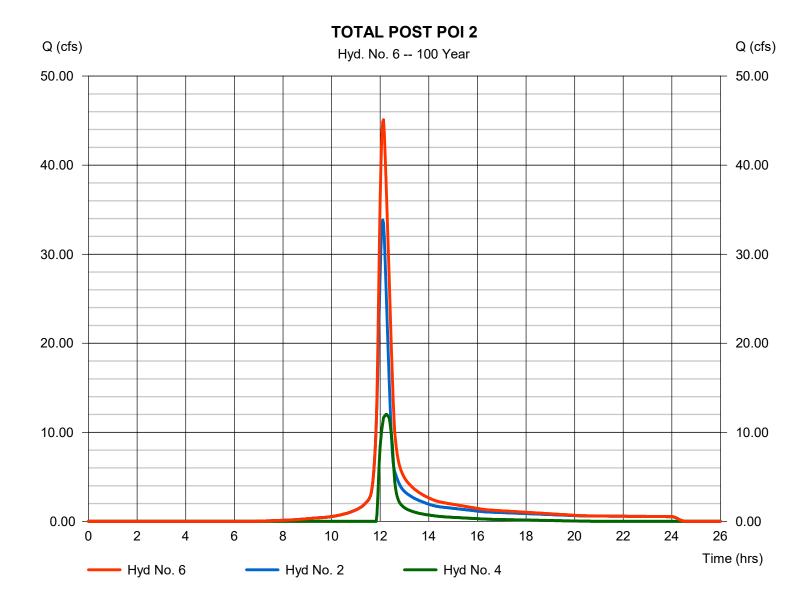
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Thursday, 02 / 22 / 2024

### Hyd. No. 6

**TOTAL POST POI 2** 

Hydrograph type = Combine Peak discharge = 45.11 cfsStorm frequency = 100 yrsTime to peak  $= 12.13 \, hrs$ Time interval = 2 min Hyd. volume = 153,933 cuft Inflow hyds. = 2,4 Contrib. drain. area = 6.970 ac



### **Pond Report**

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 02 / 20 / 2024

#### Pond No. 1 - BERM #3

#### **Pond Data**

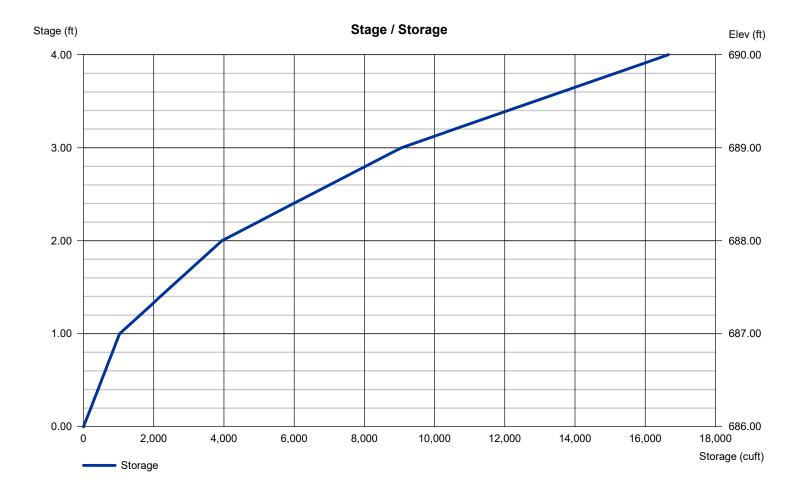
Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 686.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	686.00	179	0	0
1.00	687.00	1,876	1,028	1,028
2.00	688.00	3,947	2,912	3,939
3.00	689.00	6,278	5,113	9,052
4.00	690.00	8,941	7,610	16,661

#### **Culvert / Orifice Structures Weir Structures** [A] [B] [C] [PrfRsr] [A] [B] [C] [D] Rise (in) = 18.005.00 5.00 Crest Len (ft) = 12.00 5.00 0.00 0.00 0.00 = 18.00 36.00 24.00 0.00 Crest El. (ft) = 689.40 689.50 0.00 0.00 Span (in) 3.33 No. Barrels = 1 2 0 Weir Coeff. = 3.333.33 3.33 Invert El. (ft) = 686.00 688.40 688.40 0.00 Weir Type = 1 Broad = 27.00 0.00 0.00 0.00 Multi-Stage Length (ft) = Yes No No No 0.00 n/a = 13.89 0.00 Slope (%) = .013 N-Value .013 .013 n/a 0.60 0.60 0.60 Orifice Coeff. = 0.60Exfil.(in/hr) = 2.500 (by Contour) TW Elev. (ft) Multi-Stage = n/aYes Yes No = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



## **Channel Report**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Tuesday, Feb 20 2024

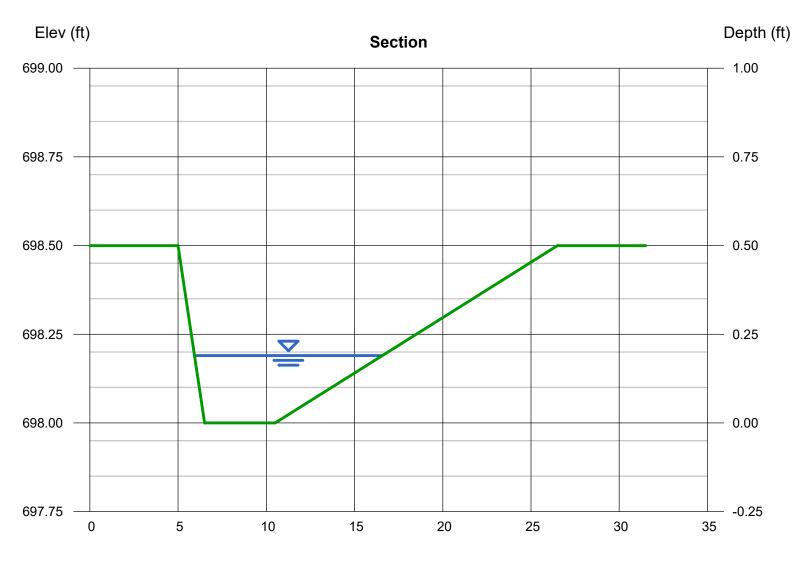
### Swale #4

Trapezoidal	
Bottom Width (ft)	= 4.00
Side Slopes (z:1)	= 3.00, 32.00
Total Depth (ft)	= 0.50
Invert Elev (ft)	= 698.00
Slope (%)	= 2.80
N-Value	= 0.026

**Calculations** 

Compute by: Known Q Known Q (cfs) = 3.11

Highlighted		
Depth (ft)	=	0.19
Q (cfs)	=	3.110
Area (sqft)	=	1.39
Velocity (ft/s)	=	2.23
Wetted Perim (ft)	=	10.68
Crit Depth, Yc (ft)	=	0.20
Top Width (ft)	=	10.65
EGL (ft)	=	0.27



Reach (ft)

#### CHANNEL ANALYSIS

Home > View Projects > Project > Swale #4

Name Swale #4

Discharge 3.11

Channel Slope 0.028

Channel Bottom Width 4 Left Side Slope 3

Right Side Slope 32

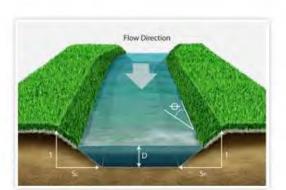
Low Flow Liner

Retardence Class C 6-12 in

Vegetation Type Mix (Sod and Bunch)

Vegetation Density Good 65-79%

Soil Type Silt Loam (SM)



Print This Page

View Computations

Duplicate Analysis Delete Analysis

### Unreinforced Vegetation

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor		Staple Pattern
Unreinforced Vegetation	Straight	3.11 cfs	1.13 <sup>ft</sup> / <sub>s</sub>	0.3 ft	0.073	4 lbs/ft2	0.52 lbs/ft2	7.66	STABLE	
Underlying Substrate	Straight	3.11 cfs	1.13 <sup>ft</sup> / <sub>s</sub>	0.3 ft	0.073	4 lbs/ft2	0.33 lbs/ <sub>ft2</sub>	12.05	STABLE	

#### S75BN

Phase	Reach	Discharge	Velocity	Normal Depth	Mannings N	Permissible Shear Stress	Calculated Shear Stress	Safety Factor	Momarke	Staple Pattern
S75BN Unvegetated	Straight	3.11 cfs	1.89 <sup>ft</sup> / <sub>s</sub>	0.21 ft	0.036	1.6 lbs/ft2	0.37 lbs/ft2	4.3	STABLE	D
Underlying Substrate	Straight	3.11 cfs	1.89 <sup>ft</sup> / <sub>s</sub>	0.21 ft	0.036	1.17 lbs/ft2	0.25 lbs/ft2	4.68	STABLE	D

# STANDARD E&S WORKSHEET #1 COMPOST FILTER SOCKS

PROJECT NAME: FRANKLIN HILL MANOR

LOCATION: ALBERT LANE

 PREPARED BY:
 TMM
 DATE:
 10-5-21

 CHECKED BY:
 JLS
 DATE:
 10-5-21

2"X 2"WOODEN STAKES PLACED 10" O.C.
COMPOST FILTER SOCK

BLOWN/PLACED FILTER MEDIA -DISTURBED AREA

UNDISTURBED AREA

12- MIN Harotharothar

				SLOPE LENGTH ABOVE
SOCK	DIA	LOCATION	SLOPE	BARRIER
(NO)	(IN.)		(%)	(FT)
1	12	WEST OF BERM 1	7.3	190
2	12	SOUTH OF LOT 1 HOUSE	5.8	140
3	12	SOUTH OF LOT 1 SEPTIC	8.4	200
4	18	SOUTH & WEST OF BERM 2	9	190
5	18	SOUTH OF LOT 2 SEPTIC	10.4	200
6	18	SOUTH OF LOT 3 DRIVEWAY	7.1	200
7	18	SOUTH OF BERM 3	10.4	200

TABLE B-1
DESIGN STORM RAINFALL AMOUNT (INCHES)

The design storm rainfall amount chosen for design should be obtained from the PennDOT region in which the site is located according to Figure B-2.

Source: "Field Manual of Pennsylvania Department of Transportation" STORM INTENSITY-DURATION-FREQUENCY CHARTS

PDT - IDF May 1986.

Region 4 Precipitation Depth (in)

Duration	1 Yr	2Yr	5Yr	10 Yr	25 Yr	50 Yr	100 Yr
5 min	0.30	0.35	0.41	0.45	0.50	0.55	0.61
15 min	0.58	0.68	0.80	0.93	1.03	1.13	1.25
1 hr	1.01	1.22	1.48	1.70	1.91	2.16	2.41
2 hrs	1.24	1.50	1.84	2.14	2.46	2.80	3.18
3 hrs	1.38	1.71	2.10	2.43	2.82	3.24	3.69
6 hrs	1.68	2.04	2.52	3.06	3.60	4.14	4.74
12 hrs	2.04	2.52	3.00	3.84	4.56	5.16	6.00
24 hrs	2.40	2.88	3.60	4.56	5.76	6.48	7.44

Region 5
Precipitation Depth (in)

Duration	1 Yr	2Yr	5Yr	10 Yr	25 Yr	50 Yr	100 Yr
5 min	0.33	0.38	0.45	0.50	0.56	0.63	0.68
15 min	0.64	0.75	0.90	1.00	1.15	1.35	1.50
1 hr	1.10	1.35	1.61	1.85	2.15	2.60	2.98
2 hrs	1.34	1.66	2.00	2.34	2.70	3.26	3.76
3 hrs	1.50	1.86	2.28	2.67	3.09	3.69	4.29
6 hrs	1.86	2.28	2.82	3.36	3.90	4.62	5.40
12 hrs	2.28	2.76	3.48	4.20	4.92	5.76	6.72
24 hrs	2.64	3.36	4.32	5.28	6.24	7.20	8.40

FIGURE B-3
PENNDOT STORM INTENSITY-DURATION-FREQUENCY CURVE

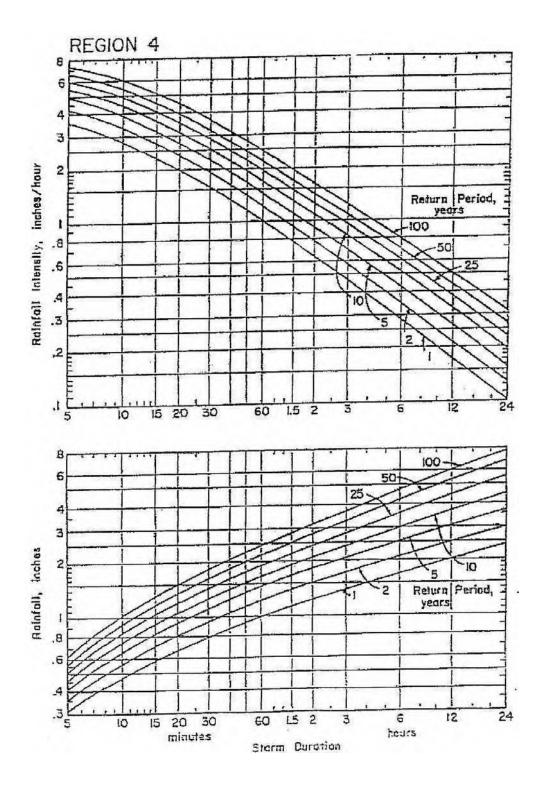


TABLE B-2 Runoff Curve Numbers (From NRCS (SCS) TR-55)

LAND USE	DESCRIPTION		HYDR	OLOGIC	SOIL	GROUP
		Hydro Condi	_	В	С	D
Open Spac	ce					
Gras	ss cover < 50%	Poor	68	79	86	89
Gras	ss cover 50% to 75%	Fair	49	69	79	84
Gras	ss cover > 75%	Good	39	61	74	80
Meadow			30	58	71	78
Agricultu	ıral					
	ture, grassland, or range tinuous forage for grazing		68	79	86	89
	ture, grassland, or range tinuous forage for grazing		49	69	79	84
	ture, grassland, or range tinuous forage for grazing		39	61	74	80
	sh-brush-weed-grass mixtur n brush the major element	re Poor	48	67	77	83
	sh-brush-weed-grass mixturn brush the major element	re Fair	35	56	70	77
	sh-brush-weed-grass mixturn brush the major element	re Good	30	48	65	73
Fallow	Bare soil		77	86	91	94
	Crop residue cover (CR)	Poor	76	85	90	93
		Good	74	83	88	90
Woods -	grass combination (orchard	lor Poor	57	73	82	86
tree farm		Fair	43	65	76	82
tiee laii	ιι)	Good	32	58	72	79
		Good	32	50	12	73
Woods		Poor	45	66	77	83
		Fair	36	60	73	79
		Good	30	55	70	77
Commercia	al	(85% Imperv	ious) 89	92	94	95

LAND USE DESCRIPTION		HYDRO	OLOGIC	SOIL	GROUP
	Hydrologic Condition	A	В	С	D
Industrial	(72% Impervious)	81	88	91	93
Institutional	(50% impervious)	71	82	88	90
Residential districts by average	lot size:				
	% Impervious				
1/8 acre or less (town house	es) 65	77	85	90	92
1/4 acre	38	61	75	83	87
1/3 acre	30	57	72	81	86
1/2 acre	25	54	70	80	85
1 acre	20	51	68	79	84
2 acres	12	46	65	77	82
Farmstead		59	74	82	86
Smooth Surfaces (Concrete, Aspha Gravel or Bare Compacted Soil)	lt,	98	98	98	98
Water		98	98	98	98
Mining/Newly Graded Areas (Pervi	ous	77	86	91	94

<sup>\*</sup> Includes Multi-Family Housing unless justified lower density can be provided.

Existing site conditions of bare earth or fallow ground shall be Note: considered as meadow when choosing a CN value.

TABLE B-3 RATIONAL RUNOFF COEFFICIENTS

_					GROUP
LAND USE DESCRIPTION		А	В	С	D
Cultivated Land : without	conservation treatment	.49	.67	.81	.88
: with con	servation treatment	.27	.43	.61	.67
Pasture or range land : po	or condition	.38	.63	.78	.84
: gc	ood condition	*	.25	.51	.65
Meadow : good condition		*	*	. 44	.61
Wood or Forest Land : thin mulch	stand, poor cover, no	*	.34	.59	.70
: good	d cover	*	*	.45	.59
Open Spaces, lawns, parks, ies	golf courses, cemeter-				
Good condition grass cover on 75% or more of the area		*	.25	.51	.65
Fair condition : grass cover on 50% to 75% of the area		*	.45	.63	.74
Commercial and business ar	eas (85% impervious)	.84	.90	.93	.96
Industrial districts (72%	impervious)	.67	.81	.88	.92
Residential :					
Average lot size	Average % Impervious				
1/8 acre or less	65	.59	.76	.86	.90
1/4 acre	38	.25	.49	.67	.78
1/3 acre	30	*	.49	.67	.78
1/2 acre	25	*	.45	.65	.76
1 acre	20	*	.41	.63	.74
Paved parking lots, roofs, driveways, etc.		.99	.99	.99	.99
Streets and roads :					
Paved with curbs and	storm sewers	.99	.99	.99	.99
Gravel		.57	.76	.84	.88
Dirt		.49	.69	.80	.84

Notes: Values are based on S.C.S. definitions and are average values. Values indicated by "---" should be determined by the design engineer based on site characteristics.

Source: New Jersey Department of Transportation, Technical Manual for Stream Encroachment, August, 1984

TABLE B-4 Roughness Coefficients (Manning's "n") For Overland Flow (U.S. Army Corps Of Engineers, HEC-1 Users Manual)

Surface Description			<u>n</u>	
Dense Growth		0.4	_	0.5
Pasture		0.3	_	0.4
Lawns		0.2	-	0.3
Bluegrass Sod		0.2	_	0.5
Short Grass Prairie		0.1	-	0.2
Sparse Vegetation		0.05	_	0.13
Bare Clay-Loam Soil	(eroded)	0.01	_	0.03
Concrete/Asphalt	- very shallow depths (less than 1/4 inch)	0.10	-	0.15
	- small depths (1/4 inch to several inches)	0.05	-	0.10

Roughness Coefficients (Manning's "n") For Channel Flow

Reach Description	<u>n</u>
Natural stream, clean, straight, no rifts or pools	0.03
Natural stream, clean, winding, some pools or shoals	0.04
Natural stream, winding, pools, shoals, stony with some weeds	0.05
Natural stream, sluggish deep pools and weeds	0.07
Natural stream or swale, very weedy or with timber under- brush	0.10
Concrete pipe, culvert or channel	0.012
Corrugated metal pipe	0.012-0.027(1)
High Density Polyethylene (HDPE) Pipe	
Corrugated	0.021-0.029(2)
Smooth Lined	0.012-0.020(2)

<sup>(1)</sup> Depending upon type, coating and diameter

<sup>(2)</sup> Values recommended by the American Concrete Pipe Association, check Manufacturer's recommended value.

#### 1. PROJECT INFORMATION

Project Name: Franklin Hill Manor
Date of Review: 1/24/2024 01:02:39 PM

Project Category: Development, Residential, Subdivision containing more than 2 lots and/or 2 single-family

units

Project Area: **6.38 acres** County(s): **Monroe** 

Township/Municipality(s): SMITHFIELD TOWNSHIP

ZIP Code:

Quadrangle Name(s): EAST STROUDSBURG

Watersheds HUC 8: Middle Delaware-Mongaup-Brodhead

Watersheds HUC 12: **Marshalls Creek** Decimal Degrees: **41.017505, -75.144408** 

Degrees Minutes Seconds: 41° 1' 3.166" N, 75° 8' 39.8674" W

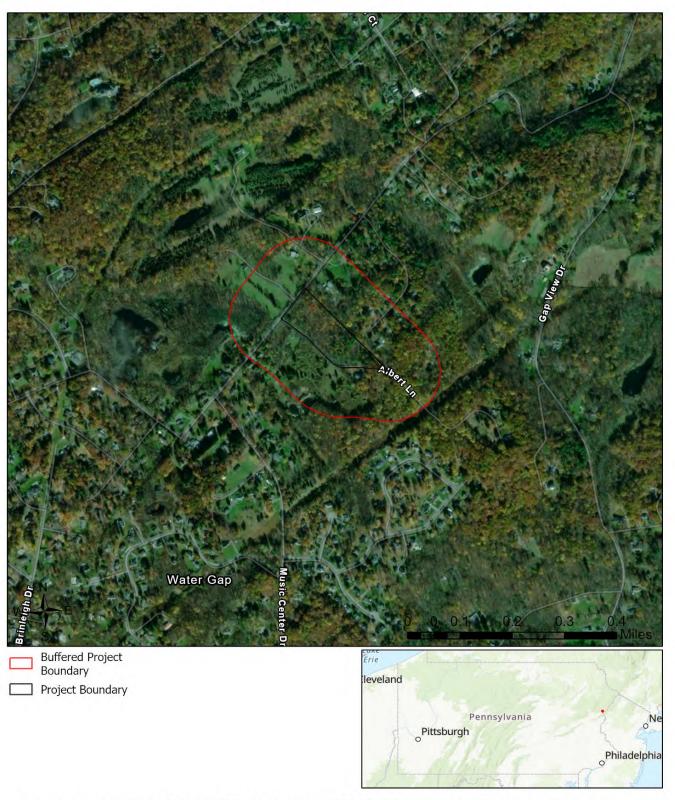
#### 2. SEARCH RESULTS

Agency	Results	Response			
PA Game Commission	Conservation Measure	No Further Review Required, See Agency Comments			
PA Department of Conservation and Natural Resources	No Known Impact	No Further Review Required			
PA Fish and Boat Commission	No Known Impact	No Further Review Required			
U.S. Fish and Wildlife Service	Potential Impact	MORE INFORMATION REQUIRED, See Agency Response			

As summarized above, Pennsylvania Natural Diversity Inventory (PNDI) records indicate there may be potential impacts to threatened and endangered and/or special concern species and resources within the project area. If the response above indicates "No Further Review Required" no additional communication with the respective agency is required. If the response is "Further Review Required" or "See Agency Response," refer to the appropriate agency comments below. Please see the DEP Information Section of this receipt if a PA Department of Environmental Protection Permit is required.

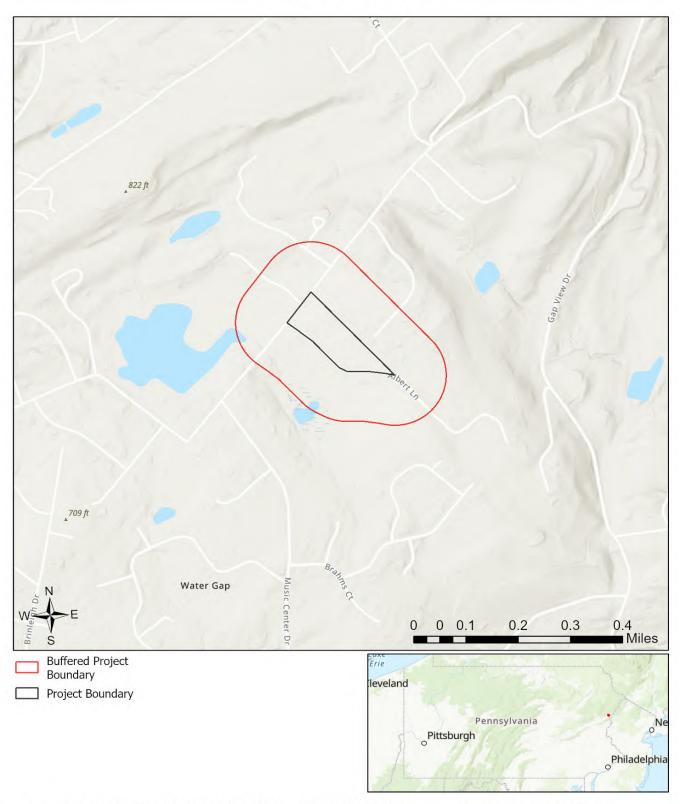
Project Search ID: PNDI-804626

#### Franklin Hill Manor



Sources: Esri, Airbus DS, USGS, NGA, NASA, CGIAR, N Robinson, NCEAS, NLS, OS, NMA, Geodatastyrelsen, Rijkswaterstaat, GSA, Geoland, FEMA, Intermap and the GIS user community

#### Franklin Hill Manor



Sources: Esri, Airbus DS, USGS, NGA, NASA, CGIAR, N Robinson, NCEAS, NLS, OS, NMA, Geodatastyrelsen, Rijkswaterstaat, GSA, Geoland, FEMA, Intermap and the GIS user community

### **RESPONSE TO QUESTION(S) ASKED**

Q1: Accurately describe what is known about wetland presence in the project area or on the land parcel by selecting ONE of the following. "Project" includes all features of the project (including buildings, roads, utility lines, outfall and intake structures, wells, stormwater retention/detention basins, parking lots, driveways, lawns, etc.), as well as all associated impacts (e.g., temporary staging areas, work areas, temporary road crossings, areas subject to grading or clearing, etc.). Include all areas that will be permanently or temporarily affected -- either directly or indirectly -- by any type of disturbance (e.g., land clearing, grading, tree removal, flooding, etc.). Land parcel = the lot(s) on which some type of project(s) or activity(s) are proposed to occur.

**Your answer is:** Someone qualified to identify and delineate wetlands (holding a natural resource degree or equivalent work experience) has investigated the site, and determined that wetlands ARE located in or within 300 feet of the project area. (A written report from the wetland specialist, and detailed project maps should document this.)

**Q2:** The proposed project is in the range of the Indiana bat. Describe how the project will affect bat habitat (forests, woodlots and trees) and indicate what measures will be taken in consideration of this. Round acreages up to the nearest acre (e.g., 0.2 acres = 1 acre).

Your answer is: The project will affect 1 to 39 acres of forests, woodlots and trees.

Q3: Is tree removal, tree cutting or forest clearing necessary to implement all aspects of this project?

Your answer is: Yes

**Q4:** Is tree removal, tree cutting or forest clearing of 40 acres or more necessary to implement all aspects of this project?

Your answer is: No

**Q5:** How many acres of woodland, forest, forested fencerows and trees will be cut, cleared, removed, disturbed or flooded (inundated) as a result of carrying out all aspects or phases of this project? [Round acreages UP to the nearest acre (e.g., 0.2 acres = 1 acre).]

Your answer is: 1 to 10 acres

#### 3. AGENCY COMMENTS

Regardless of whether a DEP permit is necessary for this proposed project, any potential impacts to threatened and endangered species and/or special concern species and resources must be resolved with the appropriate jurisdictional agency. In some cases, a permit or authorization from the jurisdictional agency may be needed if adverse impacts to these species and habitats cannot be avoided.

These agency determinations and responses are **valid for two years** (from the date of the review), and are based on the project information that was provided, including the exact project location; the project type, description, and features; and any responses to questions that were generated during this search. If any of the following change: 1) project location, 2) project size or configuration, 3) project type, or 4) responses to the questions that were asked during the online review, the results of this review are not valid, and the review must be searched again via the PNDI Environmental Review Tool and resubmitted to the jurisdictional agencies. The PNDI tool is a primary screening tool, and a desktop review may reveal more or fewer impacts than what is listed on this PNDI receipt. The jurisdictional agencies **strongly advise against** conducting surveys for the species listed on the receipt prior to consultation with the agencies.

# PA Game Commission RESPONSE:

Conservation Measure: Potential impacts to state and federally listed species which are under the jurisdiction of both the Pennsylvania Game Commission (PGC) and the U.S. Fish and Wildlife Service may occur as a result of this project. As a result, the PGC defers comments on potential impacts to federally listed species to the U.S. Fish and Wildlife Service. No further coordination with the Pennsylvania Game Commission is required at this time.

Project Search ID: PNDI-804626

# PA Department of Conservation and Natural Resources RESPONSE:

No Impact is anticipated to threatened and endangered species and/or special concern species and resources.

# PA Fish and Boat Commission RESPONSE:

No Impact is anticipated to threatened and endangered species and/or special concern species and resources.

# U.S. Fish and Wildlife Service RESPONSE:

Information Request: Conduct a Bog Turtle Habitat (Phase 1) Survey in accordance with USFWS Guidelines for Bog Turtle Surveys (April 2020). Evaluate all wetlands within 300 feet of the project area, which includes all areas that will be impacted by earth disturbance or project features (e.g., roads, structures, utility lines, lawns, detention basins, staging areas, etc.). IF THE PHASE 1 SURVEY IS DONE BY A QUALIFIED BOG TURTLE SURVEYOR (see Pennsylvania Qualified Surveyors | FWS.gov): 1) Send positive results to USFWS for concurrence, along with a project description documenting how impacts will be avoided. OR, conduct a Phase 2 survey and send Phase 1 and 2 results to USFWS for concurrence. 2) Send a courtesy copy of negative results to USFWS (label as "Negative Phase 1 Survey Results by Qualified Bog Turtle Surveyor: USFWS Courtesy Copy"). USFWS approval of negative results is not necessary when a qualified surveyor does the survey in full accordance with USFWS guidelines. IF THE PHASE 1 SURVEY IS NOT DONE BY A QUALIFIED SURVEYOR: Send ALL Phase 1 results to USFWS for concurrence, and if potential habitat is found, also send a project description documenting how impacts will be avoided. (name) certify that I conducted a Phase 1 survey of all As a qualified bog turtle surveyor, I wetlands in and within 300 feet of the project area on (date) and determined that bog turtle habitat is absent. (Signature) Avoidance Measure: The proposed project is located in the vicinity of northern long-eared bat spring staging/fall

Avoidance Measure: The proposed project is located in the vicinity of northern long-eared bat spring staging/fall swarming habitat. To ensure take is not reasonably certain to occur, do not conduct tree removal from May 15 to August 15. The U.S. Fish and Wildlife Service determined take is not reasonably certain to occur from tree removal if activities are avoided during the pup season (i.e., the range of time when females are close to giving birth (i.e., two weeks prior to birth) and have non-volant (i.e., unable to fly) young). For more information, see the Interim Voluntary Guidance for the Northern Long-Eared Bat: Forest Habitat Modification, available here: <a href="https://www.fws.gov/library/collections/interim-habitat-modification-guidance">https://www.fws.gov/library/collections/interim-habitat-modification-guidance</a>.

As the project proponent or applicant, I certify that I will implement the above Avoidance Measur	re:
(Signature)	

SPECIAL NOTE: If you agree to implement the above Avoidance Measure and if applicable, any Information Requests, no further coordination with this agency regarding threatened and endangered species and/or special concern species and resources is required. If you are not able to comply with the Avoidance Measures, you are required to coordinate with this agency - please send project information to this agency for review (see "What to Send" section).

#### WHAT TO SEND TO JURISDICTIONAL AGENCIES

If project information was requested by one or more of the agencies above, upload\* or email the following information to the agency(s) (see AGENCY CONTACT INFORMATION). Instructions for uploading project materials can be found <a href="https://example.com/here">here</a>. This option provides the applicant with the convenience of sending project materials to a single location accessible to all three state agencies (but not USFWS).

\*If information was requested by USFWS, applicants must email, or mail, project information to <a href="mailto:IR1\_ESPenn@fws.gov">IR1\_ESPenn@fws.gov</a> to initiate a review. USFWS will not accept uploaded project materials.

#### **Check-list of Minimum Materials to be submitted:**

- X Project narrative with a description of the overall project, the work to be performed, current physical characteristics of the site and acreage to be impacted.
- X A map with the project boundary and/or a basic site plan(particularly showing the relationship of the project to the physical features such as wetlands, streams, ponds, rock outcrops, etc.)

#### In addition to the materials listed above, USFWS REQUIRES the following

X **SIGNED** copy of a Final Project Environmental Review Receipt

#### The inclusion of the following information may expedite the review process.

- \_\_\_\_Color photos keyed to the basic site plan (i.e. showing on the site plan where and in what direction each photo was taken and the date of the photos)
- Information about the presence and location of wetlands in the project area, and how this was determined (e.g., by a qualified wetlands biologist), if wetlands are present in the project area, provide project plans showing the location of all project features, as well as wetlands and streams.

#### 4. DEP INFORMATION

The Pa Department of Environmental Protection (DEP) requires that a signed copy of this receipt, along with any required documentation from jurisdictional agencies concerning resolution of potential impacts, be submitted with applications for permits requiring PNDI review. Two review options are available to permit applicants for handling PNDI coordination in conjunction with DEP's permit review process involving either T&E Species or species of special concern. Under sequential review, the permit applicant performs a PNDI screening and completes all coordination with the appropriate jurisdictional agencies prior to submitting the permit application. The applicant will include with its application, both a PNDI receipt and/or a clearance letter from the jurisdictional agency if the PNDI Receipt shows a Potential Impact to a species or the applicant chooses to obtain letters directly from the jurisdictional agencies. Under concurrent review, DEP, where feasible, will allow technical review of the permit to occur concurrently with the T&E species consultation with the jurisdictional agency. The applicant must still supply a copy of the PNDI Receipt with its permit application. The PNDI Receipt should also be submitted to the appropriate agency according to directions on the PNDI Receipt. The applicant and the jurisdictional agency will work together to resolve the potential impact(s). See the DEP PNDI policy at <a href="https://conservationexplorer.dcnr.pa.gov/content/resources">https://conservationexplorer.dcnr.pa.gov/content/resources</a>.

Project Search ID: PNDI-804626

#### 5. ADDITIONAL INFORMATION

The PNDI environmental review website is a preliminary screening tool. There are often delays in updating species status classifications. Because the proposed status represents the best available information regarding the conservation status of the species, state jurisdictional agency staff give the proposed statuses at least the same consideration as the current legal status. If surveys or further information reveal that a threatened and endangered and/or special concern species and resources exist in your project area, contact the appropriate jurisdictional agency/agencies immediately to identify and resolve any impacts.

For a list of species known to occur in the county where your project is located, please see the species lists by county found on the PA Natural Heritage Program (PNHP) home page (<a href="www.naturalheritage.state.pa.us">www.naturalheritage.state.pa.us</a>). Also note that the PNDI Environmental Review Tool only contains information about species occurrences that have actually been reported to the PNHP.

#### 6. AGENCY CONTACT INFORMATION

# PA Department of Conservation and Natural Resources

Bureau of Forestry, Ecological Services Section 400 Market Street, PO Box 8552 Harrisburg, PA 17105-8552 Email: RA-HeritageReview@pa.gov

#### **PA Fish and Boat Commission**

Division of Environmental Services 595 E. Rolling Ridge Dr., Bellefonte, PA 16823 Email: RA-FBPACENOTIFY@pa.gov

#### U.S. Fish and Wildlife Service

Pennsylvania Field Office Endangered Species Section 110 Radnor Rd; Suite 101 State College, PA 16801 Email: <u>IR1\_ESPenn@fws.gov</u>

**NO Faxes Please** 

#### **PA Game Commission**

Bureau of Wildlife Management Division of Environmental Review 2001 Elmerton Avenue, Harrisburg, PA 17110-9797

Project Search ID: PNDI-804626

Email: RA-PGC PNDI@pa.gov

**NO Faxes Please** 

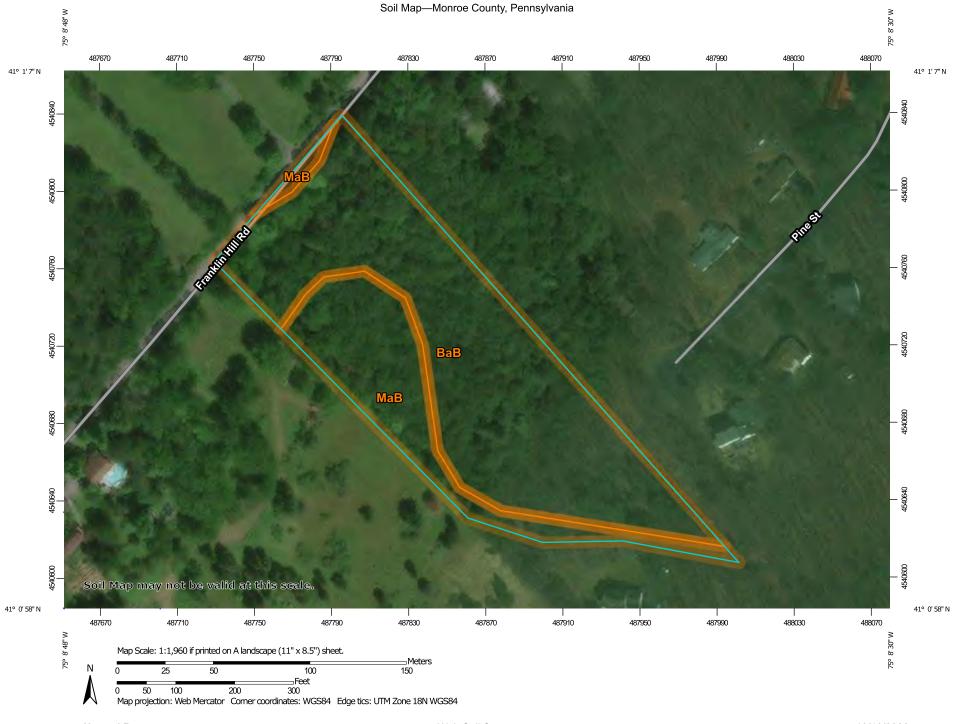
#### 7. PROJECT CONTACT INFORMATION

Name: Lighe Meckes	Alegral all all and the state of the second
Company/Business Name: Keystone Co	nsulting Engineers Inc.
Address: 863 Interchange Road, Suite	e 101, P.O. Box 639
City, State, Zip: Kresgeville, PA 18333	
Phone:(610) 681-5233	Fax:( <u>610</u> ) <u>681-5248</u>
Email: tmeckes@kceinc.com	

#### 8. CERTIFICATION

I certify that ALL of the project information contained in this receipt (including project location, project size/configuration, project type, answers to questions) is true, accurate and complete. In addition, if the project type, location, size or configuration changes, or if the answers to any questions that were asked during this online review change, I agree to re-do the online environmental review.

Lugh M. Make	1-24-2024
applicant/project proponent signature	date



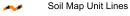
#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons



Soil Map Unit Points

#### **Special Point Features**

Blowout (0)

Borrow Pit 

× Clay Spot

Closed Depression

Gravel Pit

**Gravelly Spot** 

Landfill

Lava Flow Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot Other

Special Line Features

#### **Water Features**

0

Streams and Canals

#### Transportation

Rails ---

Interstate Highways

**US Routes** 

Major Roads

Local Roads 1

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Monroe County, Pennsylvania Survey Area Data: Version 15, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Feb 5, 2014—Oct 15. 2016

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

### **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
ВаВ	Bath channery silt loam, 3 to 8 percent slopes	4.3	73.5%
МаВ	Mardin channery silt loam, 3 to 8 percent slopes	1.5	26.5%
Totals for Area of Interest		5.8	100.0%

#### **SOIL LIMITATIONS**

			De	pth To								Soil L	imitations							
Map Symbol and Soil Description	HSG	Hydric Soil/ Inclusions	HWT (in)	Bedrock (in)	Cut Banks Cave	Corrosive to Steel/ Concrete		Easily Erodible	Flooding	High Water Table	Hydric Soils	Low Strength	Slow Percolation	Piping	Poor Source of Topsoil	Frost Action	Shrink/ Swell	Potential Sinkhole	Ponding	Wetness
BaB - Bath channery silt loam 3-8% slopes  Soil Component: Bath	С	No	24-36	26-38	Х	C/S	-	-	-	Х	Х	-	X	•	Х	х	-	-	-	-
BeB - Benson-Rock outcrop complex 0-8% slopes Soil Component: Benson	D	No	>80	12-20	х	С	Х	-	-	1	1	Х	х	Х	X	х	-	-	-	-
BeC - Benson-Rock outcrop complex 8-25% slopes  Soil Component: Benson	D	No	>80	12-20	Х	С	X	,	,	1	1	Х	Х	X	Х	х	-	-	-	-
MaB - Mardin channery silt loam 3-8% slopes Soil Component: Mardin	D	No	13-24	14-26	х	S	Х	Х	•	Х	X	Х	х	Х	-	Х	-	-	-	Х

PROJECT	NAME:	Franklin	Hill	Manor
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 CALCULATED BY:
 TMM
 DATE:
 10/16/2020

 CHECKED BY:
 JLS
 DATE:
 10/16/2020

### **Soil Limitations and Resolutions**

Soil Limitation		Soil Resolutions	
Cut Bank Cave	Consult with engineer	Over-excavate material and replace with suitable material	Construct appropriate rock slope protection or benching as directed by engineer
Corrosive to Concrete/Steel	Use corrosion resistant pipe materials	Apply corrosion resistant products to surface of constructed features	Over excavate and replace corrosive soils
Droughty Soils	Slope lining will be installed on all disturbed or proposed slopes 3H:1V or steeper	Soil amendments will be used to promote growth of vegetation	-
Easily Erodible	Install slope blankets on slopes 3:1 or steeper	Stabilize disturbed areas with seeding and soil supplements	Protect downstream areas from sediment laden sheet flow with compost filter sock or silt fence
High Water Table	Use pump water filter bag to dewater excavation, use trench boxes	Avoid seeps or wet spots	Ensure positive drainage away from excavations
Hydric Soils/Hydric Inclusions	Mark wetland areas with temporary protective fencing and avoid wetlands/wet areas	Ensure positive drainage away from potentially hydric areas	Return stormwater conveyance to sheetflow
Low Strength	Consult with engineer	Compact fill with a vibratory roller delivering 50,000 pounds total dynamic force	Over-excavate to firm material and backfill with suitable on-site excavated material
Slow Percolation	Avoid placing stormwater infiltration basins in these areas	Avoid placing on-lot septic systems in these areas	-
Piping	Install end sections or headwalls on all new pipes	Compact fill with a vibratory roller delivering 50,000 pounds total dynamic force	In lieu of extending existing feature, replace with new pipe and end section/end wall
Poor Source of Topsoil	Strip and stockpile material onsite. Remove stone and coarse fragment	Use for bulk fill and remove excess material from site.	Import suitable topsoil if existing material is inadequate.
Frost Action	Construction shall be limited when there is a risk of freezing to non-obstructive measures	Contractor shall consult project engineer for earthwork which is to occur during periods of	-
Wetness	Ensure that the site has proper drainage	Avoid seeps or wet spots	Ensure positive drainage away from excavations

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ON-LOT DISPOSAL OF SEWAGE

	Application N											
	Site Location			Franklin Hill	l Road		Subd'n Na	me .		Lot# 1 Fran	klin Hill Man	or
	√ Suitable		Soil Tvn	e Mardin Tax	Slope	8-12%	Limiting 2	Zone	24"M'	Ave. Perc.	Rate	
	Unsuitable	Mott	• •	eeps or Ponded	-	Bedro	-			= Fragments		Perc. Rate
	_	SI		Instabilized Fill			Other		_	_		
	INSTE	RUCTIC	NS FO	R COMPLE	TION OF	THIS FOR	M ARF I	OCATED (	N THE R	FVFRSF		
	SOILS DESC			COOMII EE	11011 01	111101 01		OOAILD	)	LVLINOL		
	Soils Desc	ription C	omplete	by:		VW Cor	nsultants LL	_C / JAV		_ Date:	7/17/20	
	Inches	Pit#	1			Description	n of Horizo	on			Additiona	Pits
ф	<u>0</u> TO 10	"	10YR3/4	Gravelly, Silt	Loam, Wea	ak, Fine, Gra	nular, Very F	riable			Pit #2 30"	М
4	10 TO 10		40VDE/			.l. 5: 0h		da - Establa		L		
۷1	<u>10</u> TO <u>18</u>	_	10YR5/4	Gravelly, Silt	Loam, wea	ak, Fine, Sub	angular Bloc	cky, Friable			_	
w2	<u>18</u> TO <u>24</u>	_"		Very Gravelly		eak, Medium	, Subangular	r Blocky, Frial	ble		_	
_	24 TO 36	,,		n distinct redo: Very Gravelly		ioturologo M	accivo Eirm					
•	<u> </u>	_	2.313/4	very Gravelly	, Luaiii, Sill	iciui ciess, IVI	assive, Filli	ı			_	
?	<u>36+</u> TO	_"	Bedrock								- <sub>D</sub>	taste :
	ТО										Depth to I Zone:	imiting
•		_	-								24	Inches
	TO	_"									_	_
	PERCOLATI Percolation Weather Cor Soil Condition	Test Co	mpleted Be	low 40 F	40 F or A	_	Dry	Rain, Sl	eet, Snow (la	_ Date: st 24 hours)		
	Percolation	Test Co	ompleted Be	low 40 F	Dry []	Frozen Reading	Reading	Reading	Reading	st 24 hours)	Reading	Readin No. 8:
	Percolation Weather Cor	Test Conditions	ompleted Be	low 40 F	Dry [	Frozen			, ,	st 24 hours)	Reading No. 7: Inches of drop	Reading No. 8: Inches of drop
	Percolation Weather Cor Soil Conditio	Test Conditions	empleted Bee	low 40 F et Reading	Reading No. 1: Inches	Frozen  Reading  No. 2:  Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches	No. 7: Inches	No. 8: Inches
	Percolation Weather Cor Soil Conditio	Test Conditions	empleted Bee	Reading Interval	Reading No. 1: Inches	Frozen  Reading  No. 2:  Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches	No. 7: Inches	No. 8: Inches
	Percolation Weather Cor Soil Conditio	Test Conditions	empleted Bee	Reading Interval	Reading No. 1: Inches	Frozen  Reading  No. 2:  Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches	No. 7: Inches	No. 8: Inches
	Percolation Weather Cor Soil Conditio	Test Conditions	empleted Bee	Reading Interval 10 / 30 10 / 30	Reading No. 1: Inches	Frozen  Reading  No. 2:  Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches	No. 7: Inches	No. 8: Inches
	Percolation Weather Cor Soil Conditio	Test Conditions	empleted Bee	Reading Interval 10 / 30 10 / 30 10 / 30	Reading No. 1: Inches	Frozen  Reading  No. 2:  Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches	No. 7: Inches	No. 8: Inches
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	Percolation Weather Cor Soil Conditio  Hole No	Test Conditions ins:  H20 ** Yes  Tremaining remaining ation of	mpleted Be W Left No g in the hol	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  20	Reading No. 1: Inches of drop	Reading No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches
	Percolation Weather Cor Soil Conditio  Hole No	Test Conditions ins:  H20  **  Yes	mpleted Be W Left No One of the hole  G in the hole  Average  uring	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of test	Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches
	Percolation Weather Cor Soil Conditio  Hole No  ****Wate Calcula	Test Conditions ins:  H20 ** Yes  remaining remaining ation of Drop d	mpleted Be W Left No One of the hole  G in the hole  Average  uring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  e at the end of the Percolation Ferc. Rate	Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading No. 2: Inches of drop  inute presoak  Depth	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop  0 minute interv	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches
	Percolation Weather Cor Soil Conditio  Hole No  ****Wate Calcula	Test Conditions ins:  H20 ** Yes  remaining remaining ation of Drop d	mpleted Be W Left No One of the hole  G in the hole  Average  uring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  e at the end of the Percolation Ferc. Rate	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop  inute presoak  Depth	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop  0 minute interv	Reading No. 5: Inches of drop  al; No use 1	Reading No. 6: Inches of drop  O minute intervition provided is	No. 7: Inches of drop	No. 8: Inches
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	Percolation Weather Cor Soil Conditio  Hole No  ****Wate Calcula	Test Conditions ins:  H20 ** Yes  remaining remaining ation of Drop d	mpleted Be W Left No One of the hole  G in the hole  Average  uring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  e at the end of the Percolation Ferc. Rate	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop  inute presoak  Depth	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  al; No use 1:  The informat correct result me, performe vision, or cor	Reading No. 6: Inches of drop  O minute intervition provided is ts of tests conced under my profirmed in a ma	No. 7: Inches of drop	No. 8: Inches of drop
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### COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION BUREAU OF CLEAN WATER

### SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ONLOT DISPOSAL OF SEWAGE

11/2

ALBERT

UNSUIT	ABLE	Soil Ty  Mo	ype	Slope Slope	B-IO % Ponded Wa	Depth to L	imiting Zon Bedrock	e 7 Fracture	_ Ave. F	Perc. Rate	17.32
SOILS DES Soils Descr			ed by:					D	olos		
Inche		- mpioto				Descrip	otion of Ho		ate:		
T						Dosori	otion of the	112011			
т											
T										7	
T	0	-									-1
T	0								G.		
Т	0										
Weather Co Soil Condition	onditions ons:	s: [	Below 40	940	Frozen	e Dry	☐ Rain	, Sleet, Sn	ow (last 24	hours)	
		tak	Reading	Reading No. 1:	Reading No. 2:	Reading No. 3:	Reading No. 4:	Reading No. 5:	Reading No. 6:	Reading No. 7	Reading No. 8:
Hole No.	Yes	No	Interval	Inches of drop		Inches of drop		Inches of drop	Inches of drop	Inches of drop	Inches of drop
2	¥		10 (30)	418		314"	23/4"	27/8"	27/8"	27/84	
3	Y		10 (30)	11/2"	15/8"	11/8"	11/4"	11/4"	1484	-	
4	X		10/(30)	25/8"	21/8"	21/8"	21/8"	248"			
5	Y		10 (30)	248"		17/8"	E	13/4"			
6	K		10/30)	. 17/811	11/2"	15/8"	11/2"	19/8"			
	Calcula		Average	he final 30-min Percolation erc. Rate as	Rate:	Yes, use 30	PERC	BETV	VEEN	PIT #1	-
Hole No.	fina	period		inutes/Inch	of H	lole "	IN/HF		וטוט	IN/HR =	= 3.5
2	- 10-	7/8		10.4		u	0.	610	310_910	2	
3		118		26.7	_	n	rie	Stock 8	) -)		
5	-	3/4		17.1	_	- "				s the true ar	
0		5/8	α	18.5	_	V " M	in und	er my pers	onal superv	d by me, poision, or ye	rified in a
TOTAL OF	_		_	1039	= 17	1.32	cn mai	nner appa	oved by Protection	the Depar	lment of
TOTAL NO	4000 4 4 50			6	-		(S)	Wel	le le	int Officer (SE	
	1 1 A	gency			□ Pinl	- Local DE	D Office			Yellow - /	

3800-FM-WSWM0290A Rev. 10/2003



#### 3 COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION BUREAU OF WATER SUPPLY AND WASTEWATER MANAGEMENT

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ONLOT DISPOSAL OF SEWAGE

#### INSTRUCTIONS FOR COMPLETION OF THIS FORM ARE LOCATED ON THE REVERSE SIDE

Application I				OWN ELTIO							, C OIDE	
Site Location												
		☐ Mot	tling 🗌	Slope% Depth to Limiting Zone Ave. Perc. Rate  Seeps or Ponded Water								
SOILS DES			-l l						D	-4		
Soils Descri		ompiete	a by:							ate:		<del></del>
Inche						Descrip	ition o	т но	rizon			
	0											
	0		-									
	0											
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	o o											
PERCOLAT Percolation Weather Co Soil Condition Hole No.	Test Co inditions ons:	mpleted	Below 40	°F	Reading No. 2:	Reading No. 3:	Read No.	ling 4:	Reading No. 5:	Reading No. 6:		Reading No. 8: Inches of drop
***Water remai	Calcula Drop	tion of A	Average I H <del>Pe</del> Mii	ne final 30-min Percolation C RATE rc. Rate as nutes/Inch	Rate:	pth Hole "	Do	ouble	e-ring infil /in = 2 in	trometer		
TOTAL OF I	 MIN / IN	I →			  - =	" " <u>Mi</u> " <u>Inc</u>		cor per	rect result formed un	of tests der my pe	ed is the conducted ersonal supproved by	by me, pervision,

Sewage Enforcement Officer

# E850-F. -3 DW0299A 4/2016 DEPARTMENT OF ENVIRONMENTAL PROTECTION

#### COMMONWEALTH OF PENSYLVAL A TEPARY WENT OF ENVIRONITENTAL PROTECTION BUREAU OF CLEAN WATER

## SITE INVESTIGATION AND PERCOLATION

AKIOI

10.0	ISTRUCȚIOI	TEST RE	MOKIF(	JK UNL( 1 of this	ji dispu Form ar	JSAL U E LOCAT	f devval Ed on thi	je Erevers	ESIDE G	reserve)
Application No Site Location SUITABLE UNSUITAE	Albe Soil Ty	mt lane	Slope 8	Viunicipality  Lim Hill  -10 % E  onded Wat	Rd. S Depth to Lir er Be	ubdivision niting Zon	Name <u>T</u> e <u>25" Ø</u> ] Fractures	County 1.3 CANO. Pe	erc. Rate <u>1</u>	19.0
SOILS DESCI Soils Descript	RIPTION:	ed by:	Colf to color from the description of the last				Da	ate:		
Inches		, a ~ j				tion of Ho				
		***							<del></del>	<u> </u>
TO										
TO	•						-			
TO		September 1 and 1			manage of the state of the stat				Commontant and a series	The same trading and adjust to the same
PERCOLATIO Percolation To Weather Con Soil Condition  Hole No.  1 2 3 4 5 6 ***Water remain	est Complete ditions:	Reading Interval III 10 (30) 10 (30) 10 (30) 10 (30) 10 (30) 10 (30) 10 (30) 11 (30) 1	Reading No. 1: nches of drop  3/8"  3/8"  1/2"  5/8"  a final 30-minu	For above rozen 1035 Reading No. 2: Inches of drop 1/4" 5/8" 3/8" 1/2" ute presoak?	Reading No. 3: Inches of drop I/A" I/2" I/4" I/4" I/4" I/4" I/4"	Reading No. 4: Inches of dro  1/4"  1/4"  1/4"	Reading No. 5: p Inches of drop	No. 6: Inches of drop	Reading No. 7 Inches of drop	Reading No. 8:
Hole No.  1 2 3 4 5 TOTAL OF N	Drop during final period 1/4. 1/2* 1/4 1/4 MIN / IN →	eg Perod Min	c. Rate as autes/Inch 2.0 60 2.0 120 30 24 474 6	De of L	" " " <u>N</u>	Th re l <u>lin</u> ur ch m	ne information sult of test anner appropriet appropriet approximation of the second se	n provided i s conducte sonal super roved by	d by me, vision, or ve the Depar DEP).	performed erified in a rtment of
□ White - L	_ocal Agency			☐ Pinŀ	k - Local Di	EP Office		[	] Yellow -	Applicant

# 1850-F. -3 2W0296A 4/2016 DEPARTMENT OF ENVIRONMENTAL PROTECTION

#### COWNONWEAUTH OF PERMSYLVANIA TEPARTNENTOF ENVIRONINENTAL PROTECTION BUREAU OF CLEAN WAYER

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ONLOT DISPOSAL OF SEWAGE

AKIO2 (PRVHARM)

INCEDIATIONS FOR COMPLETION OF THIS FORM ARE LOCATED ON THE REVERSE SIDE

1	NSTRU	CTIONS	FOR C	OMPLETIO	N OF THIS	FORM AR	E LOCAT	ED ON TH	e revers ^^	e side	-, ,
ا Application N Site Locatior	۱o		. 10		Municipalit	y Smithuni	eld Town	5h)p_	County <u>II</u>	Minos	
Site Location	1 Llbe	17 les	ne/I	talking b	till Rd.	S	ubdivision	Name_T	BU		20.00
ISHITARI	F	Soil I voe	€	Slope	169 % !	рерин ко пи	mung Zon	3 <u>4 J M</u>	/\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	610. Laro 7	97 44 Z
	ABLE [	☐ Mottli	ng 📙	Seeps or P	onded Wat	ter ∐B∈	edrock L	_ Fractures	S ∐ C	oarse Frag	ments
	l	Perc.	Rate	Slope	Unstabi	Ilized Fili	☐ F100d/	way ∐ ∪	ruer		
SOILS DES	CRIPTIO	N:			And the second of the second o			D			
Soils Descri	otion Cor	npleted	by:						ate:		
Inche	S				•	Descrip	tion of Ho	rizon			
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T(	O		<del></del>								<del></del>
To	o						····				
Т	o							_		·	
Т	O		· -						,		
			•								
	The second second second	Section of the second	5 y square nice and	American Completion Completion Completion Completion Completion Completion Completion Completion Completion Co	A A			Action to the second	(		
PERCOLAT Percolation	ION TES	ST: mpleted l	hu Kak	en hoorly	of Class	5) Decl	il Ho	nes D	ate: Nove	mber 7	, 2023
	****			OF 700 40	0F b	- [] Dw.	Mario Columbia	, Cloat Cn	ou (last 24	hours) (4	lawes)
Soil Condition	nalions. ons:	V V	Vet [	Dry 🔲	rozen		,~~		コピ		·0//2/0)
Weather Co Soil Condition				905	935	1005	NO35	Reading	Reading	Reading	Reading
	**	* }	Reading	No. 1:	No. 2:	No. 3:	No. 4:	No. 5:	No. 6:	No. 7	No. 8:
Hole No.	Yes	No	Interval	Inches of drop	Inches of drop	Inches of drop	Inches of drop	Inches of drop	Inches of drop	Inches of drop	Inches of drop
1	*		10 (30) 10 (30)	23/8"	21/8	13/4"		142"	11/2"		
<u>2</u> 3	16		10 (30)	13/4"	11/8"	11/8"	1118"				
4			10 / (30)	13/2"	111	168	7/8"				
5	X		10 (30)	1318" 5/8"	1/2"	1/2"	1/2"	· ·			
6	X		10/80	1/2"	115,,	3/gv	3/8"				
***Water rema	ining in the	hole at th	e end of th	ne final 30-min	ute presoak?	(es) use 30-r	minute interv	al; No, use 10	-minute inter	/al.	
. (	Calculati	ion of A	verage	Percolation	Rate:	- 1100					
		during		rc. Rate as	Dej						•
Hole No.		period	Mi	nutes/Inch	of L						
	<u>V</u>	5/B "		18.5		<u>0                                    </u>	_		_		
		12 "		20		"	$\mathcal{P}_{r}$	Soul	135-8	) <del>3</del> 5 >	
3		18 "	·	26.7	<u> </u>	"					
4		2 "		34,3	_	- "	Th	e informatio	n provided i:	s the true a	nd correct nerformed
		18 "		<u>60</u> පිට		<u></u> ₩	in un	der my pers	onal superv	ision, or ve	rified in a
6				239,5	- <del></del>	$\frac{\mathbf{v}}{\mathbf{v}}$ " inc			oved by Protection (	the Depar DEP).	tment of
TOTAL OF				_	_	1.78)			. (	,	
TOTAL NO	. OF HOI	LES→	<u> </u>	_6	-	•	(S	) Sewag	ge Enforceme	ent Officer (SE	EO)
•							<u> </u>				
☐ White ~	Local Ag	ency			☐ Pink	- Local DE	P Office	•		J Yellow -	Applicant

(1.76)(500)=880 15x60

# 2850-F -3 2WO28 (A 4/21-6 DEPARTMENT OF ENVIRONMENTAL PROTECTION

#### COMMONWEACTH OF PERMSYLVALLA IS EPARTMENT OF ENVIRONIL ENTAL PROTECTION BUREAU OF CLEAN WATER

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ONLOT DISPOSAL OF SEWAGE

AK103 (234)

INSTRUCTIONS FOR	AANDI ETIAN	AF THE FARM	ADELACATEN	ON THE DE	verse sine
INICTRICTIONS FOR	COMPLETION	OF THIS FORW	ARE LUCATED	on incre	Ackor oine

	IM21KUC !!C							County M	Sm Anda	
Application I	No n <b>Alb</b> ert	, /	la 1.12.1	Municipalit	y <u>Janvery</u>	Constitution	n Nama	County <u>"r</u>	on be	•
Site Location	n <u>IALOM</u> E Soil T	<u>Luie La</u>	Slone S	till koad	Donth to Li	mitina Zo	nna 72 ° 0	oß Ave P	erc Rate	43.67
	ABLE M	ottling $\square$	_ Soons or P	onded Wat	ter $\square$ B	edrock	Fractures	$\Box$	oarse Frag	ments
_] UNSUIT	ABLE LIM	ounny ∐ arc Rafe 「	Jeeps or i ∃Slone	⊟ Unstabi	ilized Fill	∏:Floo	dway 🔲 O	ther		,
		oro, rato L								Zin de La Company
SOILS DES	CRIPTION:	tod by					D:	ate.		
	ption Comple	tea by:								
Inche					Descrip	otion of h	ionzon			
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	0	process of the same of the same			att all and the second					Transport Marketon (Con-
Percolation Weather Co Soil Condition	Test Completonditions:	Below 40° Wet	°F 🛅 40° Drv 🗀 F	°F or above	e 📕 Dry	J R	ain, Sleet, Sn	ow (last 24	hours)	
			1020	1120	N <sup>50</sup>	12 Reading	V2 <sup>50</sup>	Reading	Reading	Reading
	***	Reading	Reading No. 1:	Reading No. 2:	Reading No. 3:	No. 4:	No. 5:	No. 6:	No. 7	No. 8:
Hole No.	Yes No		Inches of drop	Inches of drop	Inches of drop	Inches of di	rop Inches of drop	Inches of drop	Inches of drop	Inches of drop
1	¥	10/(30)	1140	1,14,,	1118"	11/8				
2	X	10 (30)	13/8"	114"	114"	11/8)		118"		
3	K	10 (30)	11/2* 5/8"	114	3/8"	3/8		7,18	1	
4_		10 (30)	1,181,	1180	7/8"		11			
5	<u> </u>	10(30)	5/8"	1/2"	1/2"	1/2"				
6	ining in the hele	ot the end of the	a final 30-min	ite prespak?	Yes use 30.	minute inte	rval: No. use 10	I I-minute inter	val.	<u></u>
***vvater rema	aining in the hole	S A		Dete:		J. (II. a.o II. a	. ( ) . ( )	.,,,,,		
•	Calculation of				. 21					
Hole No.	Drop duri final perio		c. Rate as nutes/Inch	De <sub>l</sub> of <del>L</del>						
11016 140.	148		26.7	_15						
7_	11/8	"	26.7		"	_	^	<b>1</b> 00 - 9	'n	
3	7/8	"	34.3		u	, <del>P</del>	resport 9	10-10-	<u></u>	
4	3/8	tt	80		tt		he information	n provided i	s the true a	nd correct
<u>;</u>	7/8	ıt	34.3		"	r	esult of tests	conducte	d by me,	performed
6	1/2	ıı.	60		<u>√</u> " <u>M</u>	<u>fin</u> և	ınder my pers nanner appr	onal super oved bv	/ision, or ve the Depai	ermed in a rtment of
TOTAL OF	MIN / IN →		262	= A3	.67		Environmental	Protection (	DEP).	
	, OF HOLES-		6		(1.86)	/	S)			
IOTALNO	, OF HULLO	<i></i>		-	•	1	Sewag	ge Enforceme	nt Officer (SI	EO)
						1				
☐ White -	Local Agency	1		Pink	- Local Di	EP Office			J Yellow -	Applicant

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ON-LOT DISPOSAL OF SEWAGE

			Eronklin Ui				nithfield Tow		County		nroe	
											и	
		Mottling     ☐ Seeps or Ponded Water     ☐ Bedrock     ☐ Fractures     ☐ Coarse Fragments       ☐ Slope     ☐ Unstabilized Fill     ☐ Floodplain     ☐ Other								Perc. Rate		
			OR COMPLE	ETION OF	THIS FOR	RM ARE L	OCATED (	ON THE R	EVERSE			
			to by		\/\/\ Co	naultanta l	I C / IAV		Dotos	7/47/20		
			te by						Date.		Du-	
				•						Additional Pits		
<u> </u>	-"	10YR3/4 Gravelly, Silt Loam, Weak, Fine, Granular, Very Friable							_Pit #4 25"h	{		
10 TO 18	n .	10YF	85/4 Gravelly, Sil	t Loam, We	ak, Medium,	Subangular	Blocky, Friab	_				
										_		
<u> 18</u> 10 <u>25</u>		1018	4/6 Very Gravei	iy, Siit Loam	, Structurele	ss, Massive,	Friable					
_25+_TO		Bedro	ock				····			<b>-</b>		
TO	11											
10	-		<del> </del>						<del>- , </del>	Depth to Li	miting	
TO	11									_Zone:	_	
TO	11									25	Inches	
10	_		· · · · · · · · · · · · · · · · · · ·							-		
PERCOLATIC	ON TES	ST:					÷			<del></del>		
			ed by:						Date:			
Weather Cond Soil Condition						Dry	Rain, S	leet, Snow (las	t 24 hours)			
	:o.		Wet	Dry	Frozen							
	H20	Left	Wet	Dry Reading	Frozen Reading	Reading	Reading	Reading	Reading	Reading	Reading	
		Left		Reading No. 1:	Reading No. 2:	No. 3:	No. 4:	No. 5:	No. 6:	No. 7:	No. 8:	
Hole No.	H20	Left	Wet  Reading Interval	Reading	Reading				-	1 - 1		
	H20	Left	Reading	Reading No. 1: Inches	Reading No. 2: Inches	No. 3: Inches	No. 4: Inches	No. 5: Inches	No. 6: Inches	No. 7: Inches	No. 8: Inches	
	H20	Left	Reading Interval	Reading No. 1: Inches	Reading No. 2: Inches	No. 3: Inches	No. 4: Inches	No. 5: Inches	No. 6: Inches	No. 7: Inches	No. 8: Inches	
	H20	Left	Reading Interval 10 / 30	Reading No. 1: Inches	Reading No. 2: Inches	No. 3: Inches	No. 4: Inches	No. 5: Inches	No. 6: Inches	No. 7: Inches	No. 8: Inches	
	H20	Left	Reading Interval 10 / 30 10 / 30	Reading No. 1: Inches	Reading No. 2: Inches	No. 3: Inches	No. 4: Inches	No. 5: Inches	No. 6: Inches	No. 7: Inches	No. 8: Inches	
	H20	Left	Reading Interval 10 / 30 10 / 30 10 / 30	Reading No. 1: Inches	Reading No. 2: Inches	No. 3: Inches	No. 4: Inches	No. 5: Inches	No. 6: Inches	No. 7: Inches	No. 8: Inches	
Hole No.	H20 ** Yes	Left No	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30	Reading No. 1: Inches of drop	Reading No. 2: Inches of drop	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop	No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches	
Hole No.	H20 ** Yes	No No g in the	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of	Reading No. 1: Inches of drop	Reading No. 2: Inches of drop	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop	No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches	
Hole No.	Yes  remaining tion of A	No No g in the Average	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of the Percolation Interval	Reading No. 1: Inches of drop	Reading No. 2: Inches of drop	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop	No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches	
Hole No.	H20 ** Yes	g in the	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop	No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches	
Hole No.  ***Water of Calculate	Yes Yes remaining	g in the	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of the Percolation In Perc. Rate	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop  inute presoak  Depth of Hole	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop	No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches	
Hole No.  ***Water of Calculate	Yes Yes remaining	g in the Averaguring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of the Percolation In Perc. Rate	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop  inute presoak  Depth of Hole	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop	No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches	
Hole No.  ***Water of Calculate	Yes Yes remaining	g in the Averaguring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of the Percolation In Perc. Rate	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop  inute presoak  Depth of Hole	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop  al; No use 10  The informatic correct results me, performed	No. 6: Inches of drop  minute interva	No. 7: Inches of drop  al.  the true and ucted by rsonal super-	No. 8: Inches	
Hole No.  ***Water of Calculate	Yes Yes remaining	g in the Averaguring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of the Percolation In Perc. Rate	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop  inute presoak  Depth of Hole	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop  ral; No use 10  The informatic correct results me, performer vision, or conf	No. 6: Inches of drop  minute interval on provided is of tests condid under my pe irmed in a mai	No. 7: Inches of drop  al.  the true and ucted by	No. 8: Inches	
Hole No.  ***Water of Calculate	Yes Yes remaining	g in the Averaguring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of the Percolation In Perc. Rate	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop  Inute presoak  Depth of Hole	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop  al; No use 10  The informatic correct results me, performed	No. 6: Inches of drop  minute interval on provided is of tests condid under my pe irmed in a mai	No. 7: Inches of drop  al.  the true and ucted by rsonal super-	No. 8: Inches	
+**Water of Calculate Hole No.	Yes  remaining tion of A  Drop d final pe	g in the Averaguring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of the Percolation I Perc. Rate Minutes/Ir	Reading No. 1: Inches of drop  the final 30 m Rate:	Reading No. 2: Inches of drop  Inute presoak  Depth of Hole	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop  al; No use 10  The informatic correct results me, performed vision, or conf by the Departr	No. 6: Inches of drop  minute interval on provided is of tests condid under my pe irmed in a mai	No. 7: Inches of drop  al.  the true and ucted by rsonal super-	No. 8: Inches	
Hole No.  ***Water of Calculate	Yes  remaining tion of a Drop d final pe	g in the Averaguring	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  hole at the end of the Percolation I Perc. Rate Minutes/Ir	Reading No. 1: Inches of drop  the final 30 m  Rate:	Reading No. 2: Inches of drop  Inute presoak  Depth of Hole	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop  al; No use 10  The informatic correct results me, performer vision, or conf by the Departs (S)	No. 6: Inches of drop  minute interval on provided is of tests condid under my pe irmed in a mai	No. 7: Inches of drop  al.  the true and ucted by rsonal super- nner approved	No. 8: Inches	
	Unsuitable  INSTR SOILS DESC Soils Descr Inches  0 TO 10  10 TO 18  18 TO 25  25+ TO  TO  TO  TO  PERCOLATIC Percolation Weather Con-	Suitable  □ Unsuitable □ Mott □ SI  INSTRUCTIC SOILS DESCRIPTIC SOILS DESCRIPTIC SOILS DESCRIPTIC SOILS DESCRIPTIC TO T	Suitable Soil T  Unsuitable	Soil Type Lordstown  □ Unsuitable □ Mottling □ Seeps or Ponded □ Slope □ Unstabilized Fill  INSTRUCTIONS FOR COMPLE  SOILS DESCRIPTION: Soils Description Complete by: Inches Pit# 5  0 TO 10 " 10YR3/4 Gravelly, Sil  10 TO 18 " 10YR5/4 Gravelly, Sil  18 TO 25 " 10YR4/6 Very Gravel  25+ TO " Bedrock  TO "  TO "  PERCOLATION TEST: Percolation Test Completed by: Weather Conditions : □ Below 40 F	Soil Type Lordstown Slope  Unsuitable	Soil Type Lordstown? Slope 8-12%  Unsuitable	Soil Type Lordstown 1 Slope 8-12% Limiting  Unsuitable	Suitable	Suitable	Soil Type Lordstown   Slope	Soil Type Lordstown   Slope	

☐ White - Local Agency

# COMMONWEALTH OF PENNSYLVANIA

DEPARTMENT OF ENVIRONMENTAL PROTECTION **BUREAU OF CLEAN WATER** 

14

☐ Yellow - Applicant

FRANKLIN MILL

### pennsylvania DEPARTMENT OF ENVIRONMENTAL PROTECTION SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ONLOT DISPOSAL OF SEWAGE

A 1-12 TINSTRUCTIONS F	OR COMPLETION OF THIS FORM ARE I	OCATED ON THE REVERSE SIDE
Application No.	Municipality Ani Hufiel	d Twop. County Monroe  division Name Fondon Hill Manor (TBD)
Site Location PAACEL#	6/7 <i>F</i> /1/11 Subo	division Name Fookly Hill Manor (TBD)
SUITABLE Soil Type _	Slope <u> </u> %    Depth to Limitiı	ng Zone <u>25"</u> Ave. Perc. Rate <u>21.18</u>
		ock
☐ Perc. R	ate 🗌 Slope 🔲 Unstabilized Fill 📗	Floodway    Other
SOILS DESCRIPTION:	. Доминать в город в Абристичной в Май (1955) дом в применения в применения большей в Май (1965), до применения в применен	
Soils Description Completed by	ː	Date:
Inches	Description	n of Horizon
TO		
TO		
Weather Conditions: Belo	ow 40°F 40°F or above Dry [  The Dry Frozen  1000 1000 1000 1000 1000 1000 1000 10	Rain, Sleet, Snow (last 24 hours)
***	Reading Reading Reading Re	ading Reading Reading Reading
		c. 4: No. 5: No. 6: No. 7 No. 8: es of drop Inches
	160   27/8"   23/8"   21/4"   2	21/8"   21/8"
2 x 10.		3/8" 13/8" 11/8"
		1/4" 1/18"
		5/8" 13/8" 13/8"
	(30) 2"  3/4"  3/8"	1/2" 13/8" 13/8"
	(30) 25/8" 25/8" 21/4"	7/8"  3/4"  7/8"  7/8"
	nd of the final 30-minute presoak? Yes, use 30-minut	e interval; No, use 10-minute interval.
Calculation of Ave	rage Percolation Rate:	
Drop during Hole No. final period 218 "	Perc. Rate as Depth Minutes/Inch of Hole	
2 11/8 "	26.7	Pre Soul 810_910
3 1118 "	26.7	1 Reviews - J
4 13/8 "	21.8	The information provided is the true and correct
5 13/8 "	21.8 " Min	result of tests conducted by me, performed under my personal supervision, or verified in a
6 1718 "	16 " <u>Inch</u>	manner approved by the Department of
TOTAL OF MIN / IN →	127.1 = 21.18	Environmental Protection (DEP).
TOTAL NO. OF HOLES→	<u>      6                              </u>	(S)Sewage Enforcement Officer (SEO)

☐ Pink - Local DEP Office

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ON-LOT DISPOSAL OF SEWAGE

Ar	Application No.  Site Location			_	Municip	oality <sub>.</sub>	Smi	thfield Tow		County Monroe  Lot# 2 Franklin Hill Manor					
Si	ite Locatio	n _			Franklin Hill	Road		Subd'n Nai	me	L	ot# 2 Frank	lin Hill Mand	or		
	] Suitable				pe Lordstown 1					25"M'	Ave. Perc. I	Rate			
	Unsuitable				Seeps or Ponded					Coarse	e Fragments		Perc. Rate		
			Slo	ре 🗌	Unstabilized Fill	Floo	odplain [	Other							
					R COMPLE	TION OF	THIS FOR	M ARE LO	OCATED (	ON THE RI	EVERSE				
S	OILS DES Soils Des	CR crip	IPTIO	N: omplete	by:		VW Cor	sultants LL	.C / JAV		Date:	7/17/20			
	Inches	•	Pit#				Descriptio					Additional	Pits		
γp	0 TO 1	0_'		10YR3/	/4 Gravelly, Silt	Loam, Wea	ak, Fine, Grar	nular, Very F	riable			_Pit #5 25"I	₹		
	10 TO 1			10YR5/4 Gravelly, Silt Loam, Weak, Fine, Subangular Blocky, Friable								_			
					0YR5/4 Very Gravelly, Loam, Weak, Medium, Subangular Blocky, Friable										
W2	<u>18</u> TO <u>2</u>	<u> </u>		Common distinct redox features 2.5Y5/4 Very Gravelly, Loam, Structureless, Massive, Firm								-			
ء _	25_TO_3	0_'	it .	2.5Y5/4	4 Very Gravelly,	Loam, Stru	ictureless, M	assive, Firm				-			
R _3	30+_TO	'	n .	Bedroc	k							Denth to L	imiting		
	TO	-										Depth to Limiting Zone:			
												25	Inches		
_	то	'				1,100						-			
	ERCOLAT		N TES	т.											
D															
	Percolation				l by:						Date:				
V	Percolation Veather Co	n Te ondi	est Co tions :	mpleted	Below 40 F	40 F or A	_	Dry	Rain, S	leet, Snow (las	•				
V.	Percolation	n Te ondi	est Co tions : :	mpleted B V	Below 40 F	Dry 🔲 I	Frozen			leet, Snow (las	•	Reading	Reading		
V	Percolation Veather Co	n Te ondi	est Co tions :	mpleted  B  V eft	Below 40 F Wet	Dry [] I Reading No. 1:	Frozen Reading No. 2:	Reading No. 3:	Reading No. 4:	Reading No. 5:	Reading	No. 7:	No. 8:		
V	Percolation Veather Co	n Te ondi ons	est Contions : H20 L	mpleted  B  V eft	Below 40 F	Dry [] I	Frozen Reading	Reading	Reading	Reading	st 24 hours)	_			
V	Percolation Veather Co Soil Conditi	n Te ondi ons	est Continue : H20 L	mpleted   B   B   V   P   V   P   P   P   P   P   P   P	Reading	Dry I Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5; Inches	Reading No. 6: Inches	No. 7: Inches	No, 8: Inches		
V	Percolation Veather Co Soil Conditi	n Te ondi ons	est Continue : H20 L	mpleted   B   B   V   P   V   P   P   P   P   P   P   P	Reading Interval	Dry I Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5; Inches	Reading No. 6: Inches	No. 7: Inches	No, 8: Inches		
V	Percolation Veather Co Soil Conditi	n Te ondi ons	est Continue : H20 L	mpleted   B   B   V   P   V   P   P   P   P   P   P   P	Reading Interval	Dry I Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5; Inches	Reading No. 6: Inches	No. 7: Inches	No, 8: Inches		
V	Percolation Veather Co Soil Conditi	n Te ondi ons	est Continue : H20 L	mpleted   B   B   V   P   V   P   P   P   P   P   P   P	Reading Interval	Dry I Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5; Inches	Reading No. 6: Inches	No. 7: Inches	No, 8: Inches		
V	Percolation Veather Co Soil Conditi	n Te ondi ons	est Continue : H20 L	mpleted   B   B   V   P   V   P   P   P   P   P   P   P	Reading Interval 10 / 30 10 / 30 10 / 30	Dry I Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5; Inches	Reading No. 6: Inches	No. 7: Inches	No, 8: Inches		
V	Percolation Veather Co Soil Conditi	n Te	est Coltions: H20 L ***	mpleted   B   V	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30	Dry [] I Reading No. 1: Inches of drop	Frozen  Reading  No. 2: Inches  of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No, 8: Inches		
V	Percolation Veather Co Soil Conditi  Hole N	n Te	est Contions:  H20 L  ***  Yes	npleted   E	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 ole at the end of the	Pry I Reading No. 1: Inches of drop	Frozen  Reading  No. 2: Inches  of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No, 8: Inches		
V	Percolation Veather Co Soil Conditi  Hole N	n Teondi ons do.	est Contions:  H20 L  Yes  Yes	npleted  B V eft  No  in the heaverage	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 ea Percolation F	Reading No. 1: Inches of drop	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No, 8: Inches		
W S	Percolation Veather Co Soil Conditi  Hole N  ***Wat Calculation	n Te	est Contions:  H20 L  ***  Yes	npleted  B V eft  No  y in the ho	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 ole at the end of the	Reading No. 1: Inches of drop  he final 30 m Rate:	Frozen  Reading  No. 2: Inches  of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No, 8: Inches		
W S	Percolation Veather Co Soil Conditi  Hole N	n Te	est Contions:  H20 L  ***  Yes  emaining on of A	npleted  B V eft  No  y in the ho	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 eat the end of the Perc, Rate	Reading No. 1: Inches of drop  he final 30 m Rate:	Reading No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5; Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No, 8: Inches		
W S	Percolation Veather Co Soil Conditi  Hole N  ***Wat Calculation	n Te	est Contions:  H20 L  ***  Yes  emaining on of A	npleted No No In the howaring riod	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 eat the end of the Perc, Rate	Reading No. 1: Inches of drop  he final 30 m Rate:	Reading No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  /al; No use 10	Reading No. 6: Inches of drop  D minute intervi	No. 7: Inches of drop	No, 8: Inches		
W S	Percolation Veather Co Soil Conditi  Hole N  ***Wat Calculation	n Te	est Contions:  H20 L  ***  Yes  emaining on of A	npleted No  In the heaverage uring riod "	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 eat the end of the Perc, Rate	Reading No. 1: Inches of drop  he final 30 m Rate:	Reading No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  Al; No use 10  The informati correct result me, performe	Reading No. 6: Inches of drop  O minute intervention provided is sof tests conded under my pe	No. 7: Inches of drop  al	No. 8: Inches of drop		
W S	Percolation Veather Co Soil Conditi  Hole N  ***Wat Calculation	n Te	est Contions:  H20 L  ***  Yes  emaining on of A	npleted No  In the heaverage uring riod "	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 eat the end of the Perc, Rate	Reading No. 1: Inches of drop  he final 30 m Rate:	Reading No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  Zal; No use 10  The informati correct result me, performe vision, or con	Reading No. 6: Inches of drop  O minute intervi	No. 7: Inches of drop  al	No. 8: Inches of drop		
W S	Percolation Veather Co Soil Conditi  Hole N  ***Wat Calculation	n Te	est Contions:  H20 L  ***  Yes  emaining on of A	npleted No  In the heaverage uring riod "	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 eat the end of the Perc, Rate	Reading No. 1: Inches of drop  he final 30 m Rate:	Reading No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  Al; No use 10  The informati correct result me, performe	Reading No. 6: Inches of drop  O minute intervi	No. 7: Inches of drop  al	No. 8: Inches of drop		
H — — —	Percolation Veather Co Soil Conditi  Hole N  ***Wat Calcu Hole No.	n Tondions	est Contions:  H20 L  ***  Yes  Prop definal pe	npleted No  In the heaverage uring riod "	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  Ole at the end of the Percolation Ferc. Rate Minutes/In	Reading No. 1: Inches of drop  he final 30 m Rate: as	Reading No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  // Al; No use 10  The informati correct result me, performe vision, or con by the Depar	Reading No. 6: Inches of drop  D minute interval on provided is s of tests cond ad under my pe	No. 7: Inches of drop  the true and ucted by resonal super-	No. 8: Inches of drop		
H — — — — — — — — — — — — — — — — — — —	Percolation Veather Co Soil Conditi  Hole N  ***Wat Calculation	n Tenndions	est Contions:  H20 L  ***  Yes  Prop definal pee	npleted  No  If the he  Average  Jring  If the he  If the  If the he  If the	Reading Interval  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  10 / 30  Ole at the end of the Percolation Ferc. Rate Minutes/In	Reading No. 1: Inches of drop  he final 30 m Rate:	Reading No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  // Al; No use 10  The informati correct result me, performe vision, or con by the Depar	Reading No. 6: Inches of drop  O minute intervi	No. 7: Inches of drop  the true and ucted by resonal super-	No. 8: Inches of drop		

#### COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION

**BUREAU OF CLEAN WATER** 

pennsylvania

DEPARTMENT OF ENVIRONMENTAL PROTECTION ALANKLIN HILL

#### SITE INVESTIGATION AND PERCOLATION **TEST REPORT FOR ONLOT DISPOSAL OF SEWAGE**

ALLOSI	INSTRUCTION	S FOR C	OMPLETIO	N OF THIS	S FORM AI	RE LOCAT	ED ON TH	E REVERS	SE SIDE	
Application i	No n_ <i>PARCELH</i>			Municipal	ty Smith	Field 1	WSP.	County <u>M</u>	Imroe	
Site Location	n PARCELH	16 7F	11/11			Subdivision	n Name 🕣	anklin H	all Marc	su(IDD)
☐ SUITABL	_E Soil Ty	ре	Slope _	<u>/-と</u> %	Depth to Li	imiting Zor	ne <u>25°</u>	Ave. P	erc.Rate _	1802
UNSUIT	ABLE Mot									
	∐ Per	c. Rate	Slope	∐ Unstak	oilized Fill	∐ Flood	way 📙 O	ther	ar in common signa a traca	
SOILS DESC Soils Descri	CRIPTION: ption Complete	d by:					D	ate:		
Inche	s				Descrip	otion of H	orizon			
TO	0	****								
то	ο									decentification of the state of
TO	o		***						<u> </u>	
TO	o									
	o									<del></del>
то	o									
	ION TEST	1/		eranistran manatukan		managama, nangalawa, Aliote	<u>eu pape escribe en discretió de disc</u>	anggar wendi, man auto nelikisisika	Lik Tak Austra (E. 1900) Crist Turk S	27 or IAURSIG = 105/25/8 74/8/29/8/70
PERCOLAT Percolation	Test Completed	i by: <u>Ka</u> l	perheec	en clo	Justic (	Realit	<u>4</u> D	ate: 50	2mloss :	2,2020
Weather Co	nditione:	Relow 10	ν <b>Ε Μ</b> ΙΔΩ	°F or above						,
Soil Condition	ons:	Wet [	Dry [ ]	Frozen	1045	เบเซ	1145	1015	1245	115
	***		Reading	Reading	Reading	Reading	Reading	Reading	Reading	Reading
Hole No.	Yes No	Reading Interval	No. 1: Inches of drop	No. 2: Inches of drop	No. 3: Inches of drop	No. 4: Inches of drop	No. 5: Inches of drop	No. 6: Inches of drop	No. 7 Inches of drop	No. 8: Inches of drop
(	¥	10 (30)	23/4"			2"	13/4"	13/4"	1	and the same of th
2	<u> </u>	10 (30)	3"	25/8"		2"	13/4"		17/9"	The state of the s
	\ \	10 (30)	25/8"	21/4"	21/8"	2"	17/8"	17/8"		
4	¥	10 (30)	2'4"	13/2"	<del></del>	13/8	13/2,"	13/01	( 3a/a u	2604
5	X.	10 (30)	21/4-	23/8"	21/3"	13/4	172"	13/8"	13/8"	√318"
6	<u> </u>	10 (30)	11/2"	11/2"	15%"	13/4"	- l. No. 100 40	uning de intem	i d	
	ning in the hole at				Yes, use 30	minute interv	ai; ivo, use to	-minute interv	rai.	
(	Calculation of	_								
Hole No.	Drop during final period		rc. Rate as nutes/Inch		pth łole					
110,6110.	13/4.	(	17.1	2	Ö "					
2	17/8	•	16	•	<u> </u>	$\circ$				
3	17/8		16		"	y oc	Sout 8	315,95		
4	13/8		21.8		"	76	- !faunatia	n navidad i	a tha tuua ar	ad correct
5	13/8		21.8		"		e information of tests			
<u> </u>	13/4		17.1		" <u>M</u>	<u>in</u> un	der my pers	onal superv	ision, or vei	rified in a
TOTAL OF I	<del></del>		109.8	= 18	5.3		nner approvironmental			ment of
	OF HOLES→	· · · · · · · · · · · · · · · · · · ·	6		· · · ·	(S				
IOIAL NO.	OI HOLLO	-	<u> </u>	-		(5)	Sewag	je Enforcemei	nt Officer (SE	0)
☐ White - I	Local Agency			☐ Pink	- Local DE	P Office			Yellow - A	∖pplicant

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ON-LOT DISPOSAL OF SEWAGE

	Application No. Site Location		).			Municip			thfield Tow			Monroe lin Hill Manor			
ĺ	✓ Suita	able		Soil Typ	Franklin Hill  Mardin Tax eeps or Ponded	Slope	3-8%	Subd'n Nar Limiting 2 ock	Zone	21"M	Ave. Perc. I	Rate	Perc. Rate		
			Slo	ре 🔲 U	nstabilized Fill	☐ Floo	odplain [	Other							
	0011.0	DECO	DITTIC	NI.	COMPLE										
	Soils	s Descri	ption C	omplete b	oy:	·	VW Co	nsultants LL	.C / JAV		Date:	7/17/20			
		ches	Pit#					on of Horizo				Additional			
۱p.	0	TO 10	· 11	10YR3/4	Gravelly, Silt	Loam, Wea	ık, Fine, Gra	nular, Very F	riable			Pit #8 21"N	Л		
w1 <sub>.</sub>	10	TO <u>18</u>	···	10YR4/4	Gravelly, Silt	Loam, Wea	ık, Fine, Sub	angular Bloc	ky, Friable			-			
w2	18	TO 21	19	10YR5/4	Very Gravelly	y, Loam, We	eak, Medium	, Subangular	· Blocky, Fria	ble					
•				Commor	distinct redo: Very Gravelly,	x features									
		TO <u>27</u>	-			, LOGIII, OHU	oral ologo, IV	1230140, 1 11111				-			
R .	27+	то	-"	Bedrock					·			Depth to L	imiting		
		TO										Zone: <b>21</b>	Inches		
		TO	11					•							
			•												
•		COLATIO			ην.				. 4		Date:				
	Perc		「est Co	mpleted l		40 F or A	bove	Dry	Rain, S	leet, Snow (la	•				
	Perc Weath	olation 7	Fest Co ditions : s:	mpleted I Be We	low 40 F	Dry 🔲	Frozen				st 24 hours)	Reading	I Reading		
	Perc Weath	olation T her Cond	「est Co ditions∶	mpleted I Be We	low 40 F	Dry [] Reading No. 1:	Frozen Reading No. 2:	Reading No. 3:	Reading No. 4:	Reading No. 5:	Reading	Reading No. 7:	Reading No. 8:		
	Perc Weath	olation T her Cond	Test Co ditions : s:	mpleted I Be We	low 40 F	Dry [] Reading	Frozen Reading	Reading	Reading	Reading	st 24 hours)				
	Perc Weath	olation Ther Condition	Test Co ditions : s:	mpleted I Be We	low 40 F	Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches	No. 7: Inches	No. 8: Inches		
	Perc Weath	olation Ther Condition	Test Co ditions : s:	mpleted I Be We	low 40 F et  Reading Interval	Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches of drop	No. 7: Inches	No. 8: Inches of drop		
	Perc Weath	olation Ther Condition	Test Co ditions : s:	mpleted I Be We	Reading Interval	Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches of drop	No. 7: Inches	No. 8: Inches of drop		
	Perc Weath	olation Ther Condition	Test Co ditions : s:	mpleted I Be We	Reading Interval 10 / 30 10 / 30	Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches of drop	No. 7: Inches	No. 8: Inches of drop		
	Perc Weath	olation Ther Condition	Test Co ditions : s:	mpleted I Be We	Reading Interval 10 / 30 10 / 30 10 / 30	Reading No. 1: Inches	Frozen Reading No. 2: Inches	Reading No. 3: Inches	Reading No. 4: Inches	Reading No. 5: Inches	Reading No. 6: Inches of drop	No. 7: Inches	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition	Fest Coditions:	mpleted I	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30	Dry Freeding No. 1: Inches of drop	Frozen  Reading  No. 2: Inches  of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.	Fest Coditions: s: H201 *** Yes	mpleted I Be We	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the extension of the extens	Dry   Reading   No. 1: Inches   Inches	Frozen  Reading  No. 2: Inches  of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.	remaining	mpleted I Be We eft No  in the hole Average	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the Percolation Fercent 10 / 10 / 10 / 10 / 10 / 10 / 10 / 10	Dry Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.  ***Water Calcula	Fest Coditions: s: H201 *** Yes	mpleted I Be Weeft No In the hole Average I	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the extension of the extens	Dry Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches  of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.  ***Water Calcula	remaining tion of A	mpleted I Be Weeft No In the hole Average I	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the Percolation Ferco. Rate	Dry Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop	Reading No. 6: Inches of drop	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.  ***Water Calcula	remaining tion of A	mpleted I Be Weeft No In the hole Average uring	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the Percolation Ferco. Rate	Dry Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  val; No use 10	Reading No. 6: Inches of drop  D minute intervi	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.  ***Water Calcula	remaining tion of A	mpleted I Be Weeft No In the hole Average uring	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the Percolation Ferco. Rate	Dry Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  val; No use 10  The informati correct result me, performe	Reading No. 6: Inches of drop  D minute intervention provided is as of tests conded under my pe	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.  ***Water Calcula	remaining tion of A	mpleted I Be Weeft No In the hole Average uring	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the Percolation Ferco. Rate	Dry Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  val; No use 10  The informati correct result me, performe vision, or cor	Reading No. 6: Inches of drop  D minute interval ion provided is s of tests cond ad under my pe	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.  ***Water Calcula	remaining tion of A	mpleted I Be Weeft No In the hole Average uring	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the Percolation Ferco. Rate	Dry Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  val; No use 10  The informati correct result me, performe	Reading No. 6: Inches of drop  D minute interval ion provided is s of tests cond ad under my pe	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	***Water Calcula	remaining tion of A	mpleted I Be Weeft No In the hole Average uring	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the Percolation Fercolation Ferco	Dry Reading No. 1: Inches of drop  the final 30 m Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  Val; No use 10  The informati correct result me, performe vision, or cor by the Depar	Reading No. 6: Inches of drop  D minute interval ion provided is s of tests cond ad under my pe	No. 7: Inches of drop	No. 8: Inches of drop		
	Perc Weath Soil C	her Condition Hole No.  ***Water Calcula	remaining tion of / Drop d final pe	mpleted I Be Weeft No No I I I I I I I I I I I I I I I I I	Reading Interval 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 10 / 30 e at the end of the Percolation Fercolation Ferco	Dry Reading No. 1: Inches of drop  the final 30 m  Rate:	Frozen  Reading  No. 2: Inches of drop	Reading No. 3: Inches of drop	Reading No. 4: Inches of drop	Reading No. 5: Inches of drop  val; No use 10  The informati correct result me, performe vision, or cor by the Depar	Reading No. 6: Inches of drop  D minute interval ion provided is s of tests cond ad under my pe	No. 7: Inches of drop  al. the true and ucted by rsonal super-nner approved	No. 8: Inches of drop		



# COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION BUREAU OF CLEAN WATER

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ONLOT DISPOSAL OF SEWA

A7€8

FRANKLIN HILL! TEST REPORT	FOR ONLOT DISPOSAL OF SEWAGE
INSTRUCTIONS FOR COMPLETI Application No. Site Location Acces to 16 17 1 11  SUITABLE Soil Type Slope UNSUITABLE Mottling Seeps or	Municipality   Muni
SOILS DESCRIPTION:	Date;
TO	Description of Horizon
ТО	
TO	
то	
то	
Weather Conditions:         □ Below 40°F         ■ 40°F           Soil Conditions:         ■ Wet         □ Dry         □ 40°F           Wet         □ Dry         □ 40°F         ■ 40°F           Wet         □ Dry         □ Reading         No. 1:           No. 1:         Interval         Inchés of drop         No. 1:           1         10(30)         2'/8"         □ 2'/8"           2         10(30)         2'/8"         □ 2'/8"           3         10(30)         2'/8"         □ 2'/8"           5         10(30)         10/8"         □ 2'/8"           6         10(30)         5'/8"	Reading   Reading   Reading   Reading   Reading   Reading   No. 2;   No. 3;   No. 4;   No. 5;   No. 6;   No. 7   No. 8;   Inches of drop   I
Hole No.   Drop during   Perc. Rate as   Minutes/Inch   21.8     2	Depth of Hole  2D  " " " " " " " " " " " " " " " " "
☐ White - Local Agency	☐ Pink - Local DEP Office ☐ Vallow - Applicant

3800-FM-WSWM0290A Rev. 10/2003



#### 3 COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION BUREAU OF WATER SUPPLY AND WASTEWATER MANAGEMENT

# SITE INVESTIGATION AND PERCOLATION TEST REPORT FOR ONLOT DISPOSAL OF SEWAGE

#### INSTRUCTIONS FOR COMPLETION OF THIS FORM ARE LOCATED ON THE REVERSE SIDE

Application I				OWII ELIIO							)L OIDL	
Site Location												
		☐ Mot	Soil Type Slope% Depth to Limiting Zone Ave. Perc. Rate Mottling Seeps or Ponded Water Bedrock Fractures Coarse Fragr Perc. Rate Slope Unstabilized Fill Floodplain Other									gments
SOILS DES			al la							-1		
Soils Descri		omplete	a by:							ate:		<del></del>
Inche						Descrip	ition c	от но	orizon			
	0											
	0		-									
	0											
	0											
	0											
	0		-									
Percolation Weather Co Soil Condition Hole No.	onditions ons:	: 🔲	Below 40	°F	Reading No. 2:	Reading No. 3:	Read No.	ding 4:	Reading No. 5:	Reading No. 6:		Reading No. 8: Inches of drop
			10/30									
***Water remai	Calculat Drop		Average I H Pe Mi	e final 30-min Percolation C RATE rc. Rate as nutes/Inch		pth	Do 30	ouble min	e-ring infi n/in = 5 in e informati	Itrometer /hr on provide of tests		by me,
TOTAL OF	MIN / IN	I →			=						pproved by	

Sewage Enforcement Officer

